

Selective laser melting of Cu-based shape memory alloys

T. Gustmann, U. Kühn,
C. Bolfarini, C.S. Kiminami, P. Gargarella,
Simon Pauly

Acknowledgements

2

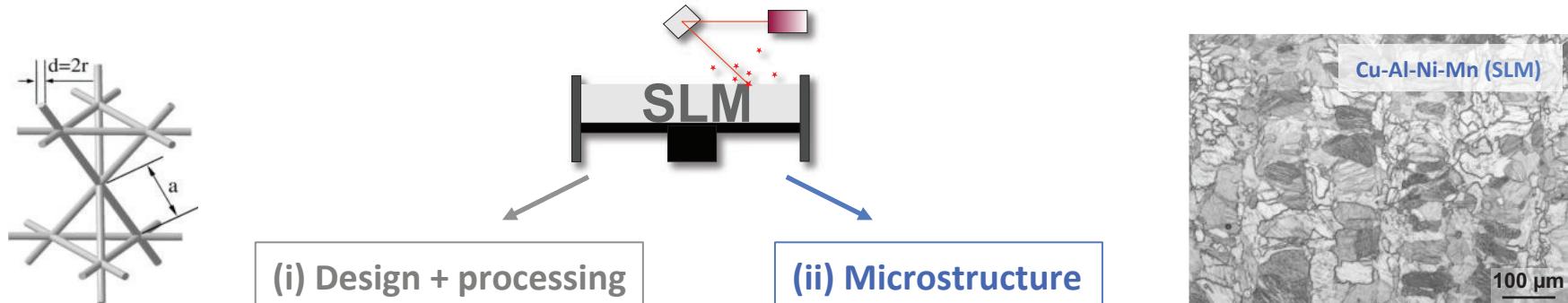


Dr. Uta Kühn,



Dr. Tobias Gustmann

Konrad Kosiba, Benjamin Escher, Pei Wang, David Geißler, Holger Schwab, Jan Sander, Frank Silze, Christian Schricker, Birgit Bartusch, Nicole Geißler, Romy Petters, Harald Merker, Brit Präßler-Wüstling, Sven Donath, Micha Frey, Kai-Uwe Baumgart, Alex Schultze, André Neves, Jonadabe Martins dos Santos, Witor Wolf, Leonardo A. Basilio, R.L. Batalha, ...



(i) Design + processing

- “Unlimited” design freedom, optimized topologies
- No need for dedicated tools/moulds
- manufacturing of prototypes, ...

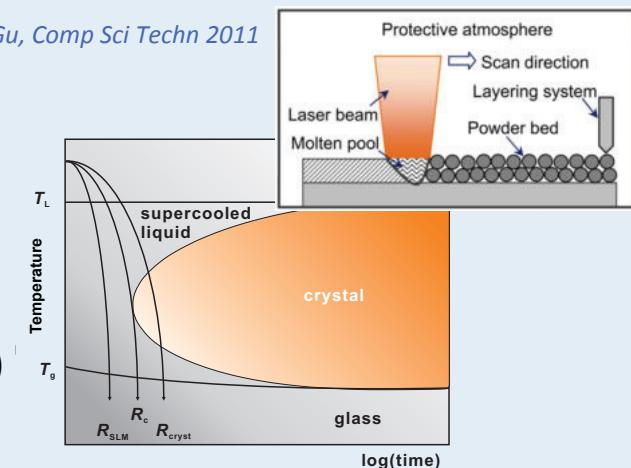


J.H. Zhu, Arch Computat Methods Eng 2015

(ii) Microstructure

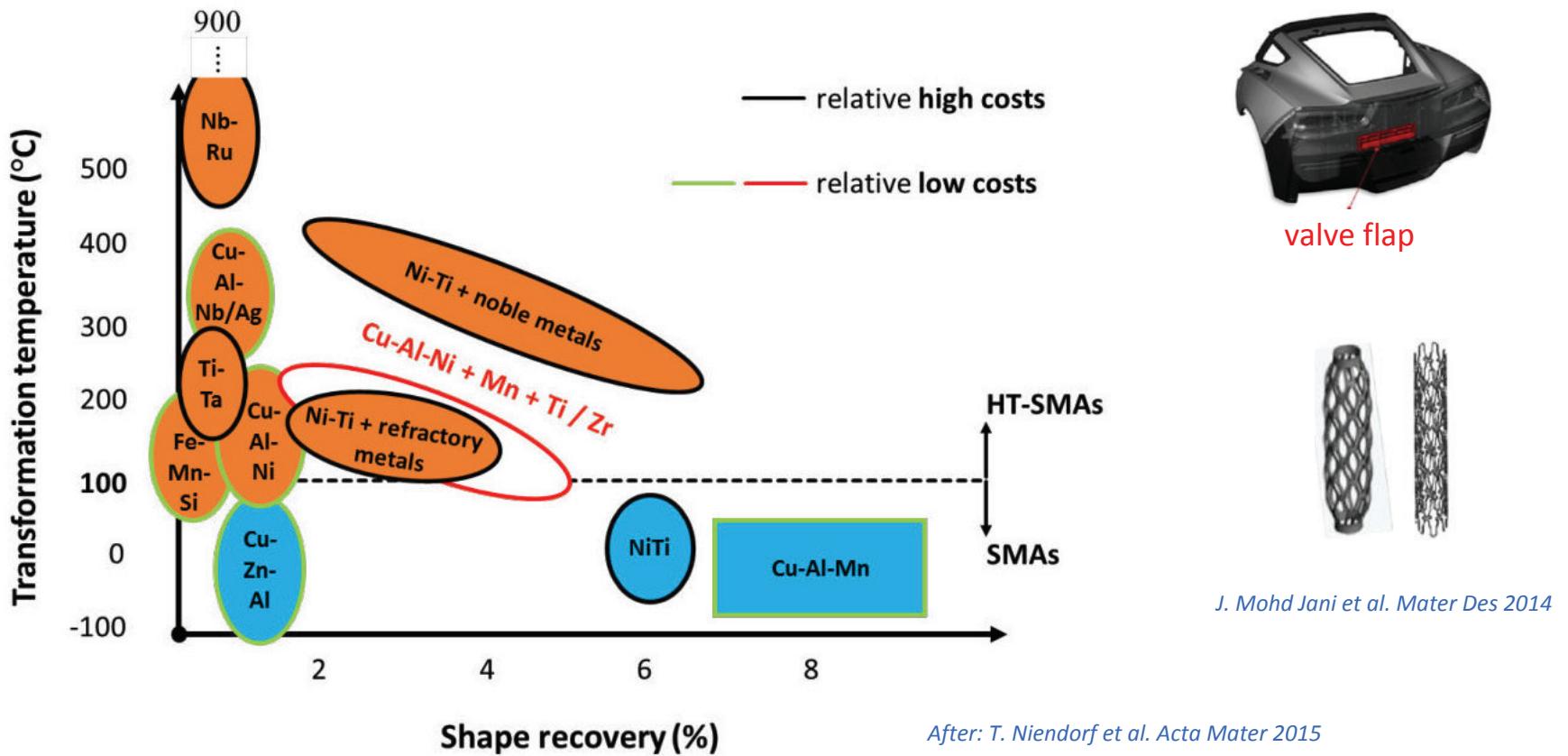
- Fabrication split into multiple “casting steps”
- Small melt pool → high intrinsic cooling rates
- Supersaturation, grain refinement, metastable phases
 - metastable microstructures
 - adjust microstructure locally (energy input, scan strategy, heating...)
 - metastable microstructures at large scales

D. Gu, Comp Sci Techn 2011



Shape-memory alloys (SMAs)

4



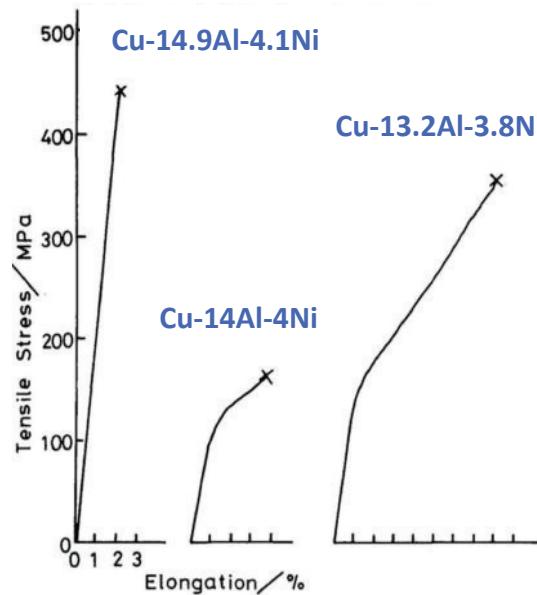
Cu-based SMAs:

- Cu-Zn-Al, Cu-Ni-Al
- Cost-efficient

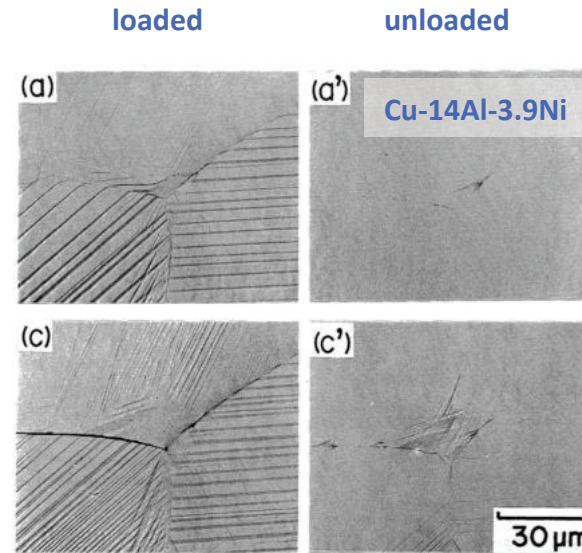
- Good processability
- Good shape memory properties
- Transformation temperatures relatively high

Cu-based shape memory alloys

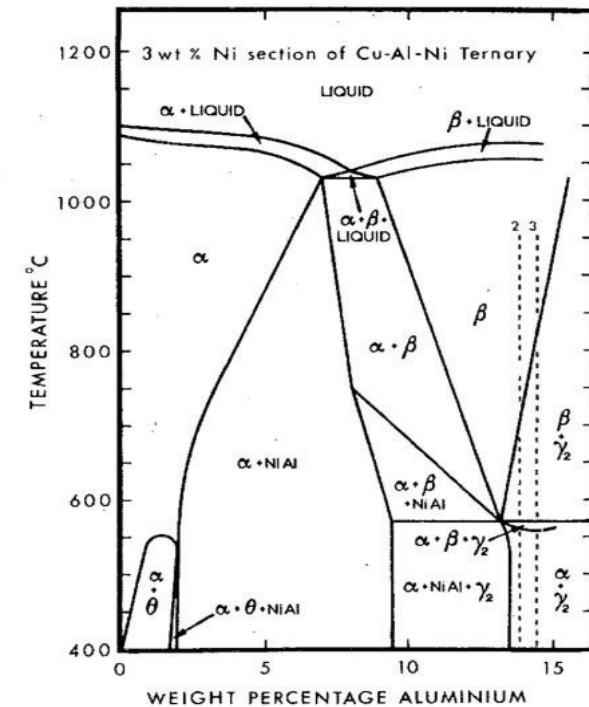
5



H. Sakamoto et al. Trans JIM 1982



S. Miyazaki et al. Trans JIM 1981



D.P. Dunne et al. Metals Forum 1981

- Coarse-grained Cu-based SMAs are intrinsically brittle
- Elastic anisotropy → transgranular fracture
- Grain refiners (e.g. Ti, Zr, B, ...), thermo-mechanical treatment, cooling rate ↑
- Avoid formation of eq. phases: α , γ_2 and NiAl

Outline

6

- Two compositions: Cu-**11.85Al-3.2Ni-3Mn**
Cu-**11.35Al-3.2Ni-3Mn-0.5Zr**
- Effect of SLM parameters and SLM on SME → tune properties
 - for comparison: spray forming and Cu-mould casting (+ annealing)
 - phase formation, grain size and ordering on SME



spray forming (SF)



Ø: 70 mm
h: 120 mm



induction casting (IC)



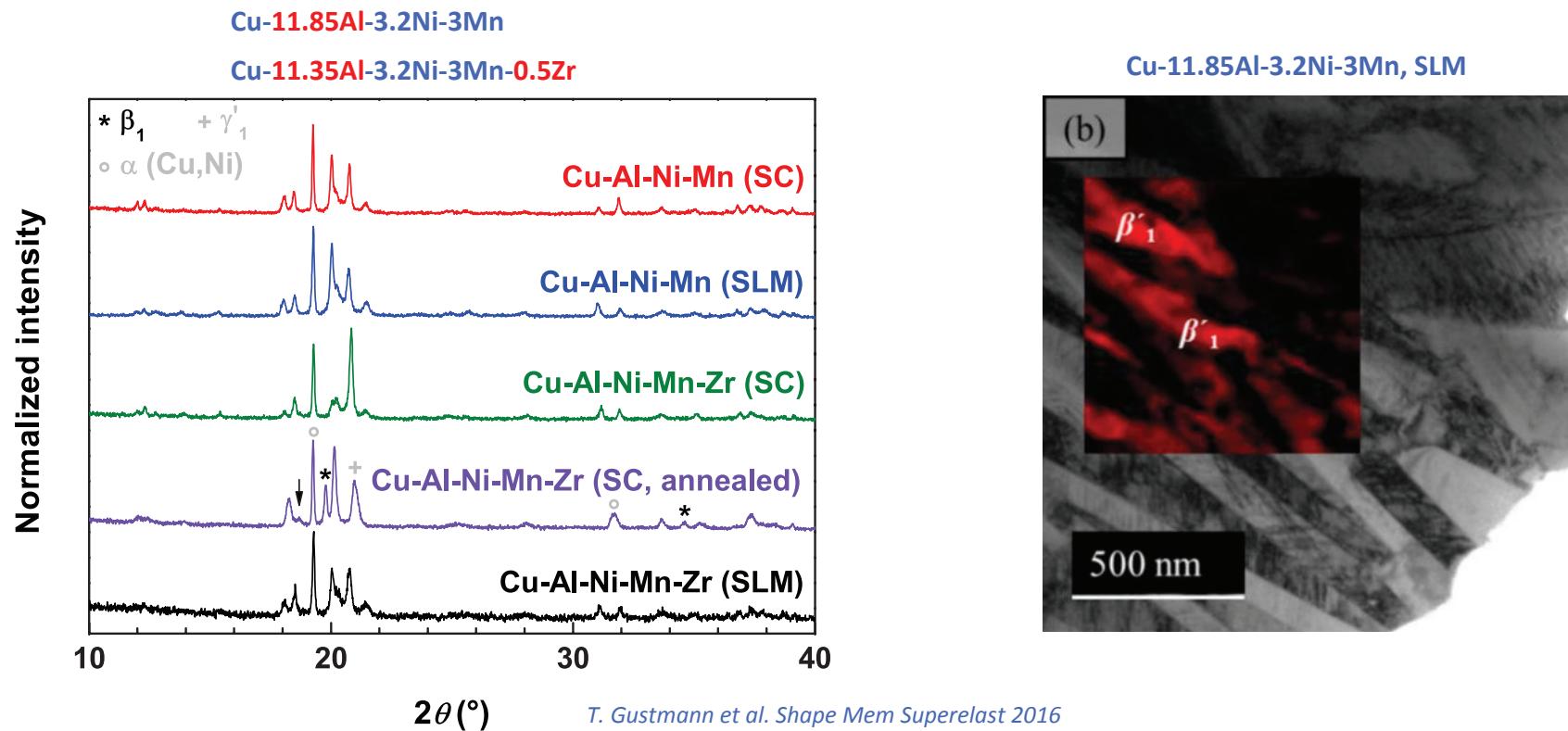
Ø: 3 mm
h: 80 mm



suction casting (SC)

Phase formation

7

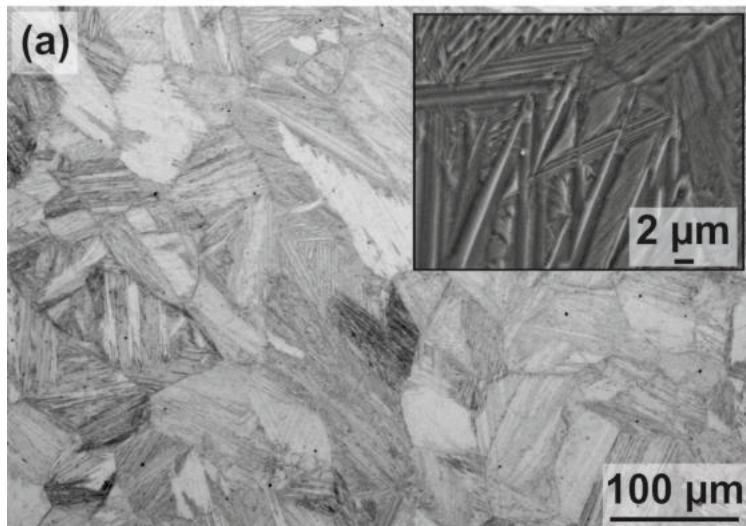


- β_1' martensite
 - Phase identification difficult: broad peaks, multitude of phases
 - Annealing: 10 mins @ 850 °C + water quenching + 60 mins @ 300 °C + slow cooling
 - After annealing: β_1 , α (?) and γ_1 (?) and additional phase (\downarrow)
- EDX + EBSD

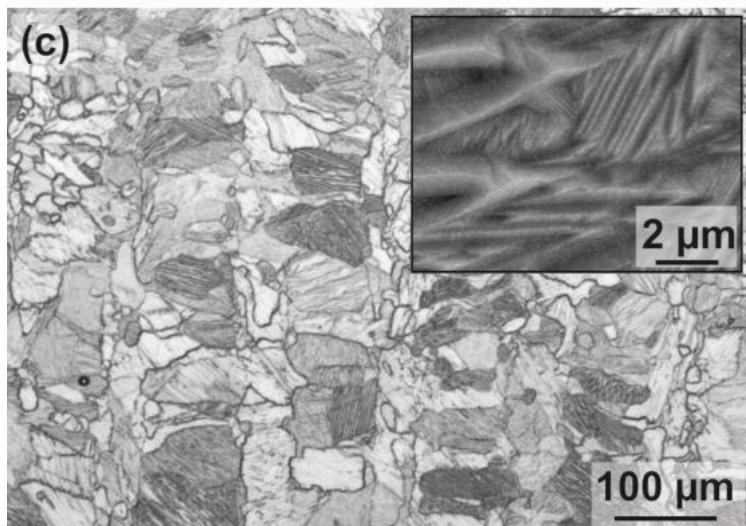
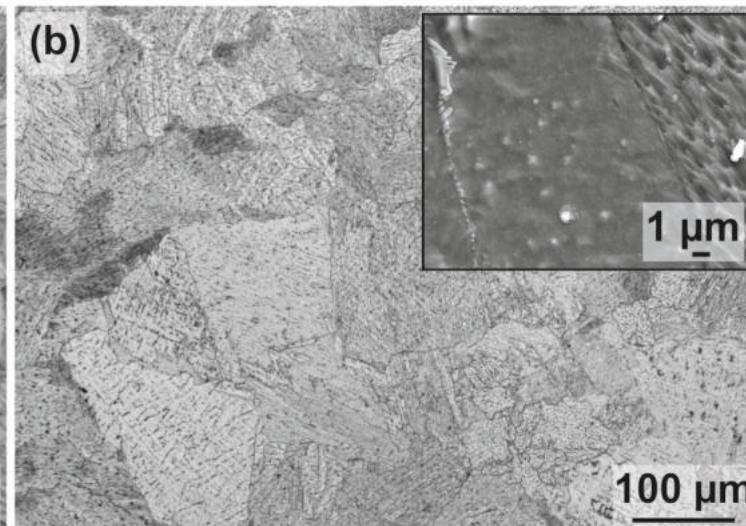
Phase formation and microstructure

8

Cu-11.85Al-3.2Ni-3Mn (cast, centre)

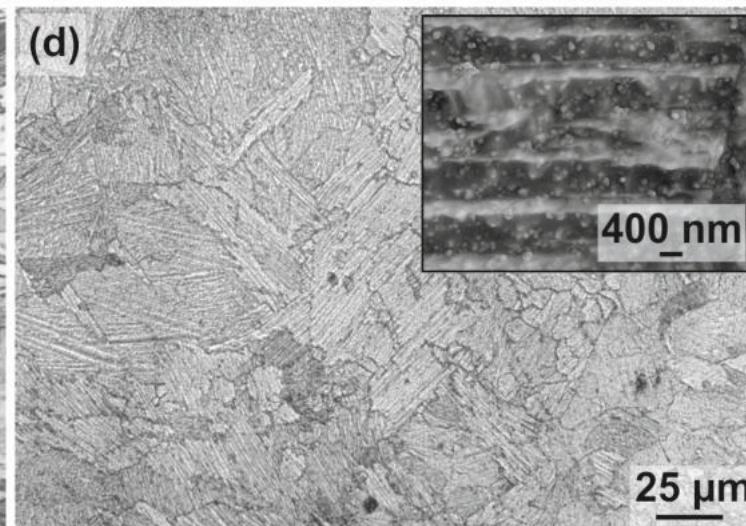


Cu-11.35Al-3.2Ni-3Mn-0.5Zr (cast, centre)



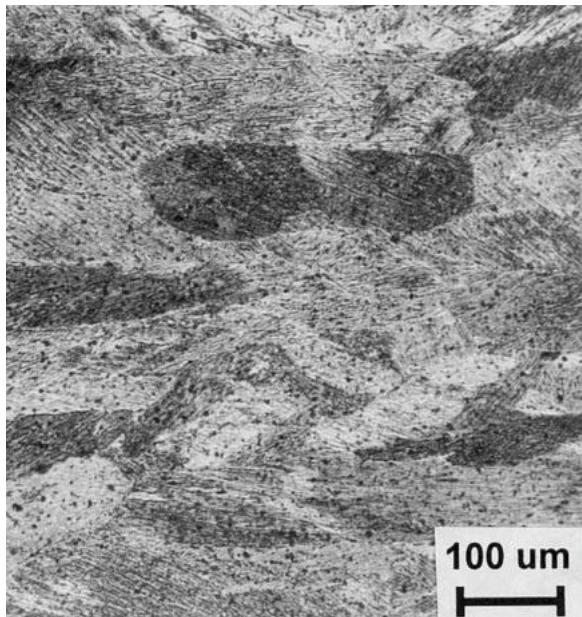
◎
BD

Cu-11.85Al-3.2Ni-3Mn (SLM)



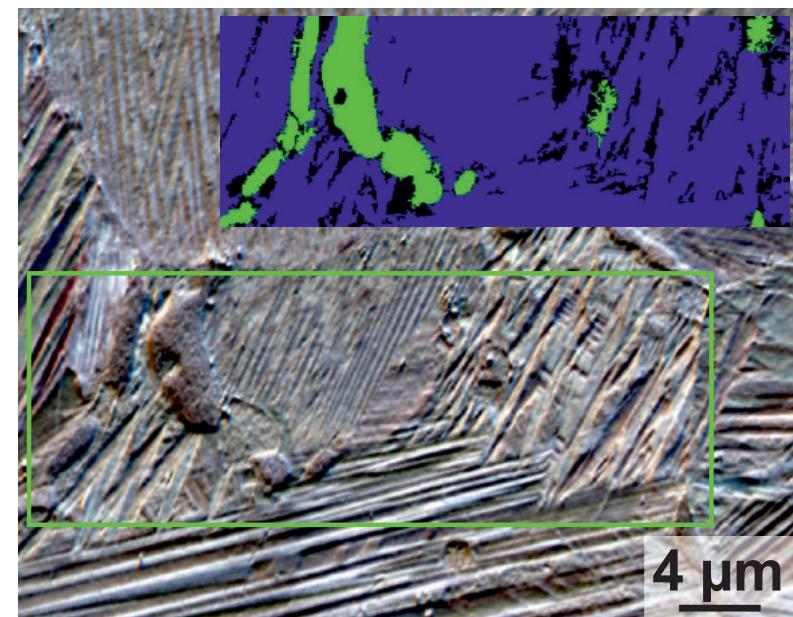
Cu-11.35Al-3.2Ni-3Mn-0.5Zr (SLM)

Cu-11.4Al-2.5Ni-5Mn-0.4Ti



Cu_2AlZr
 β_1'

cast Cu-11.35Al-3.2Ni-3Mn-**0.5Zr**, annealed



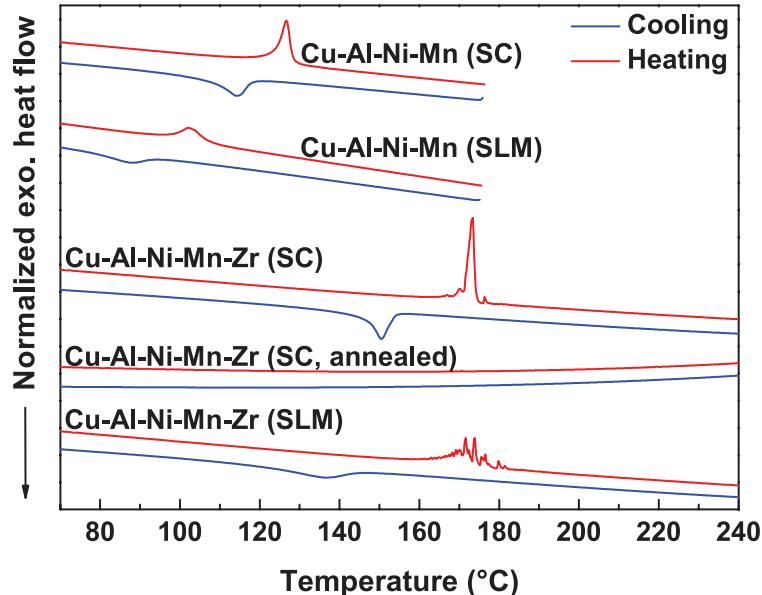
J. Dutkiewicz et al. MSEA 1999

T. Gustmann et al. Shape Mem Superelast 2016

- Cu_2AlTi (X phase) in Cu-Al-Ni-Mn-Ti
- Cu_2AlZr (Y phase, isomorphous to the X phase)
- Y phase very fine in as-prepared state
- No hints of α , γ_2 or NiAl

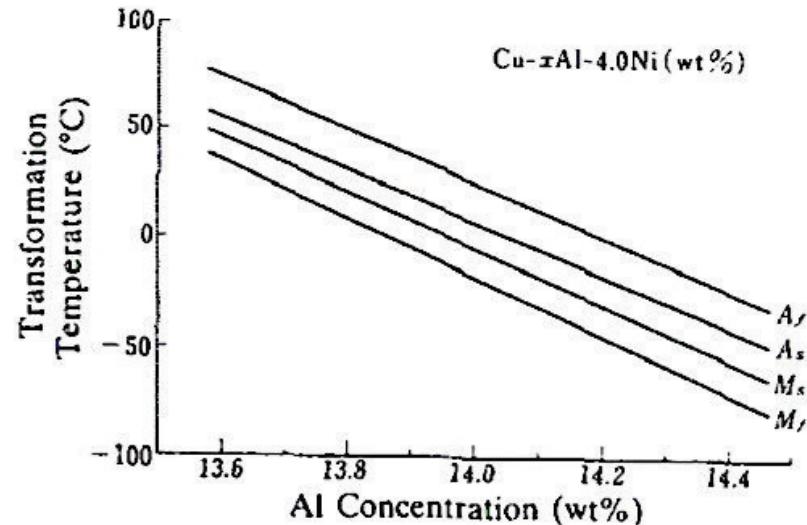
Martensitic transformation

10



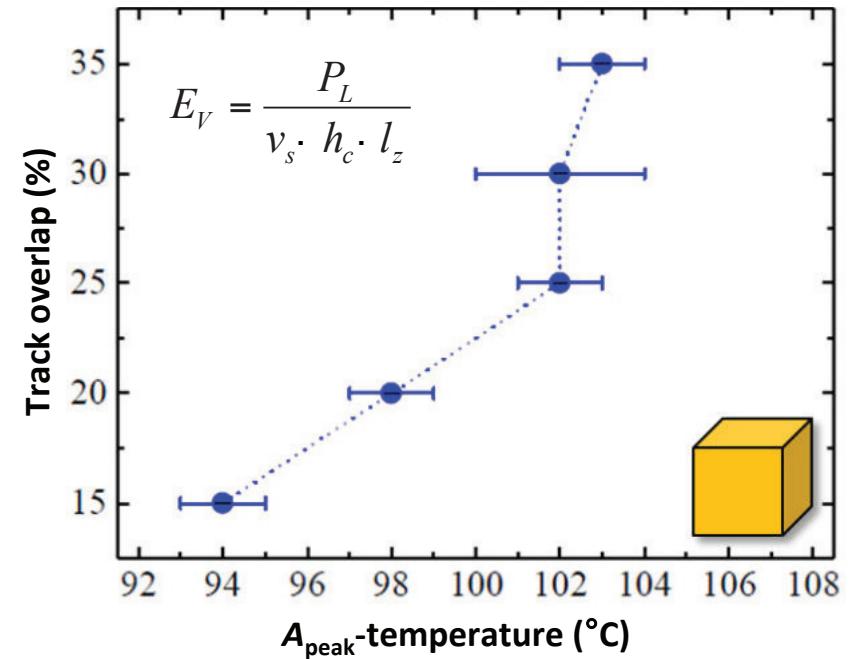
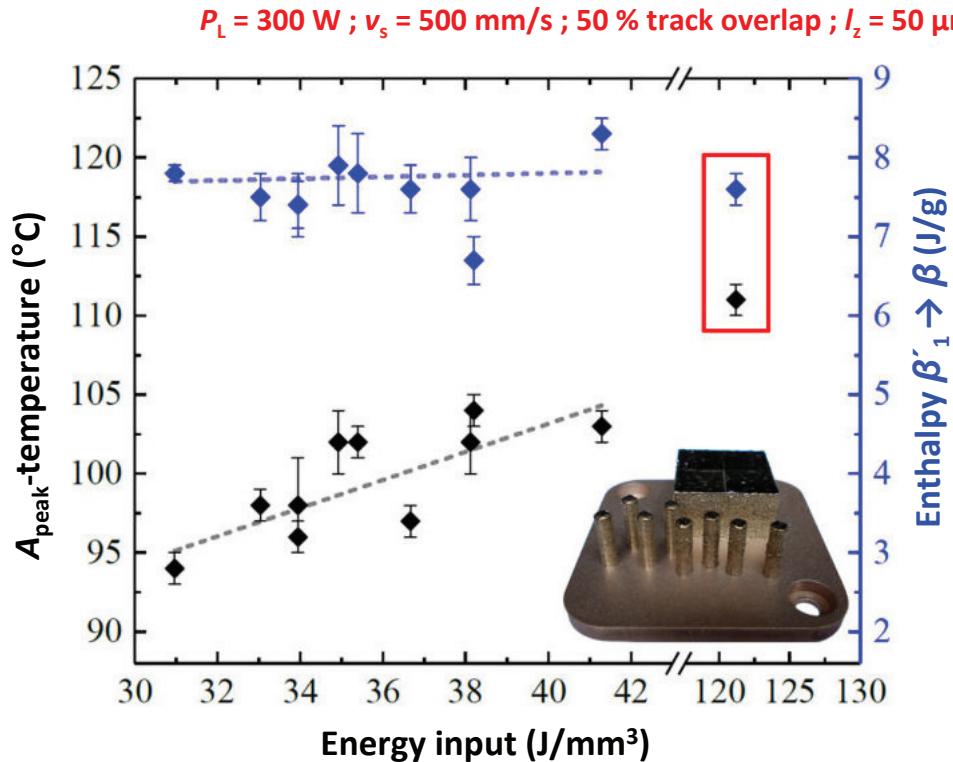
T. Gustmann et al. *Shap Mem Superelast* 2016

Cu-11.85Al-3.2Ni-3Mn
Cu-11.35Al-3.2Ni-3Mn-0.5Zr



T. Tadaki in *Shape memory materials*, 1998

- Transformation temperatures ↑ with Zr additions
- Fine Y phase: jerky transformation
- Fine Y phase: increase in MT temperatures
- Annealing: coarse Y phase at grain boundaries → no more MT
- “switch off” SME locally in sample

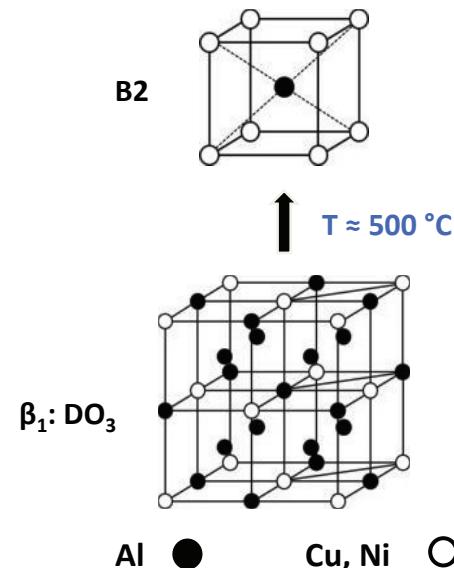
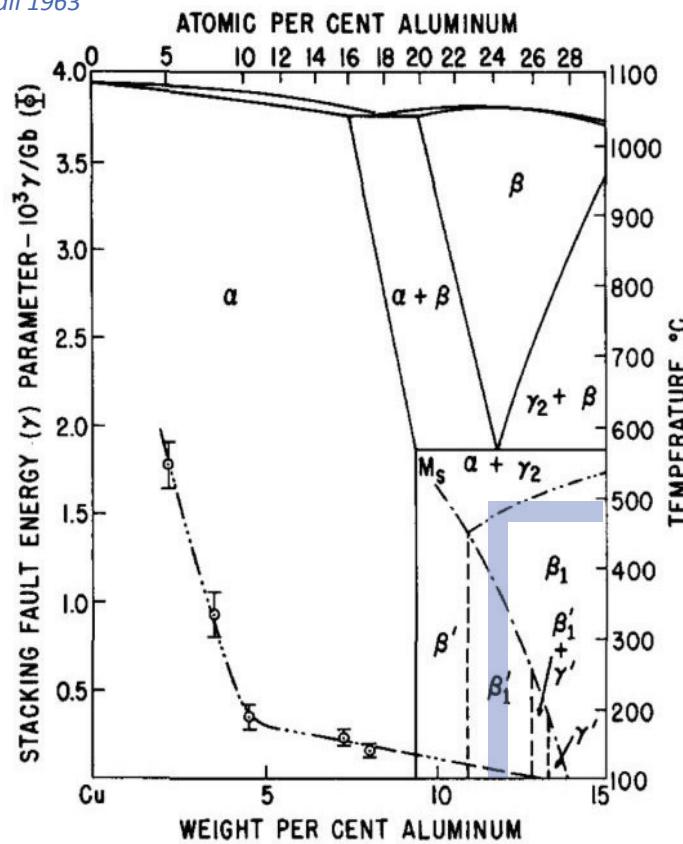


- Transformation temperatures ↑ when energy input ↑ (no oxygen uptake)
- Temperature window: about 10 °C
- Local modification by changing the process parameters
→ graded transformation
- Ordering and grain size

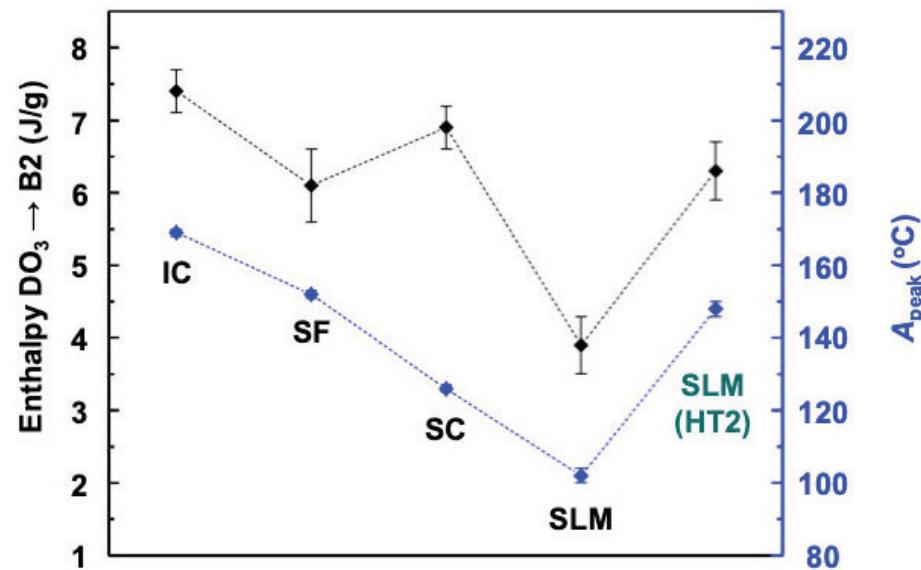
Effect of ordering in Cu-Al(-Ni)

12

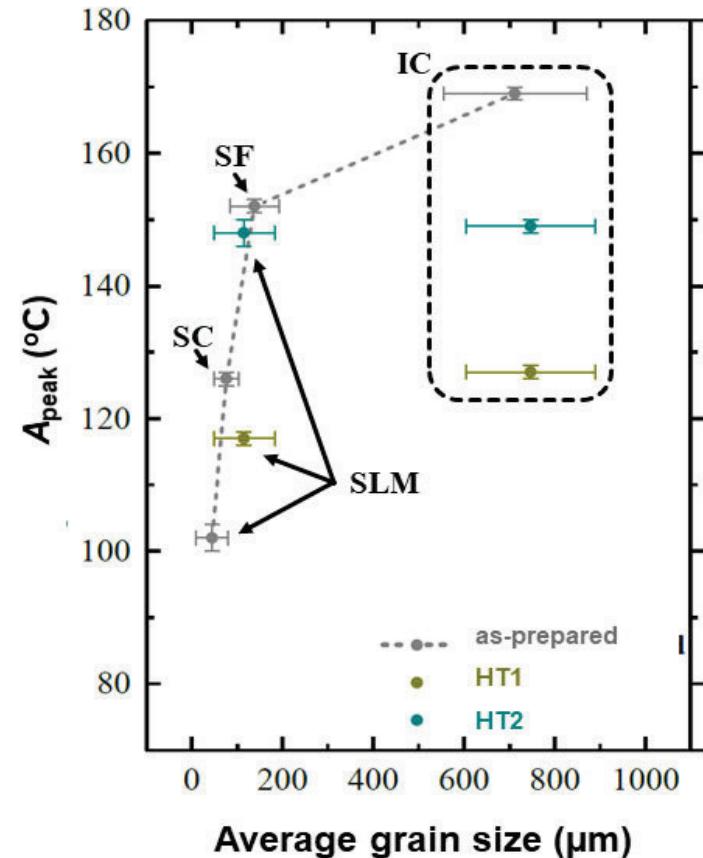
P.R. Swann et al. Acta Metall 1963



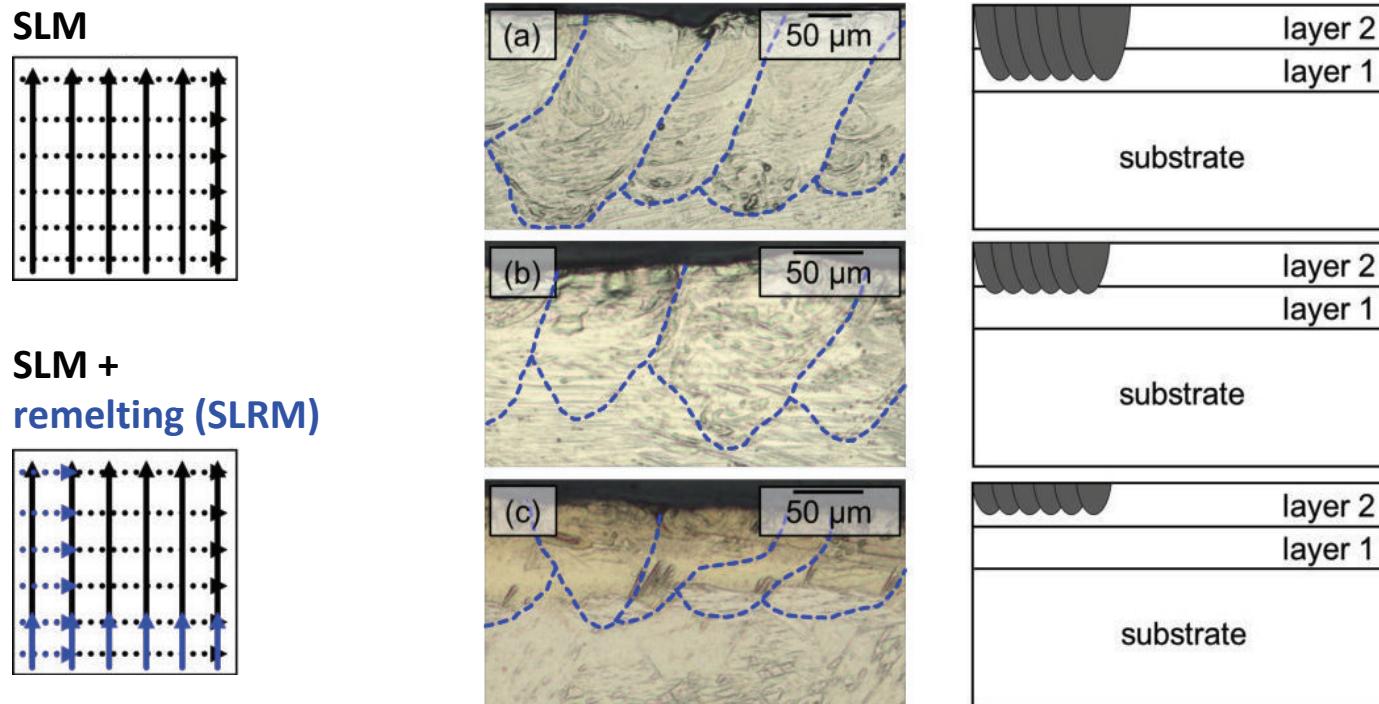
- β_1 : DO_3 ordering, B2: ordered bcc (simple cubic)
- Variation of cooling rates
- Two heat treatments



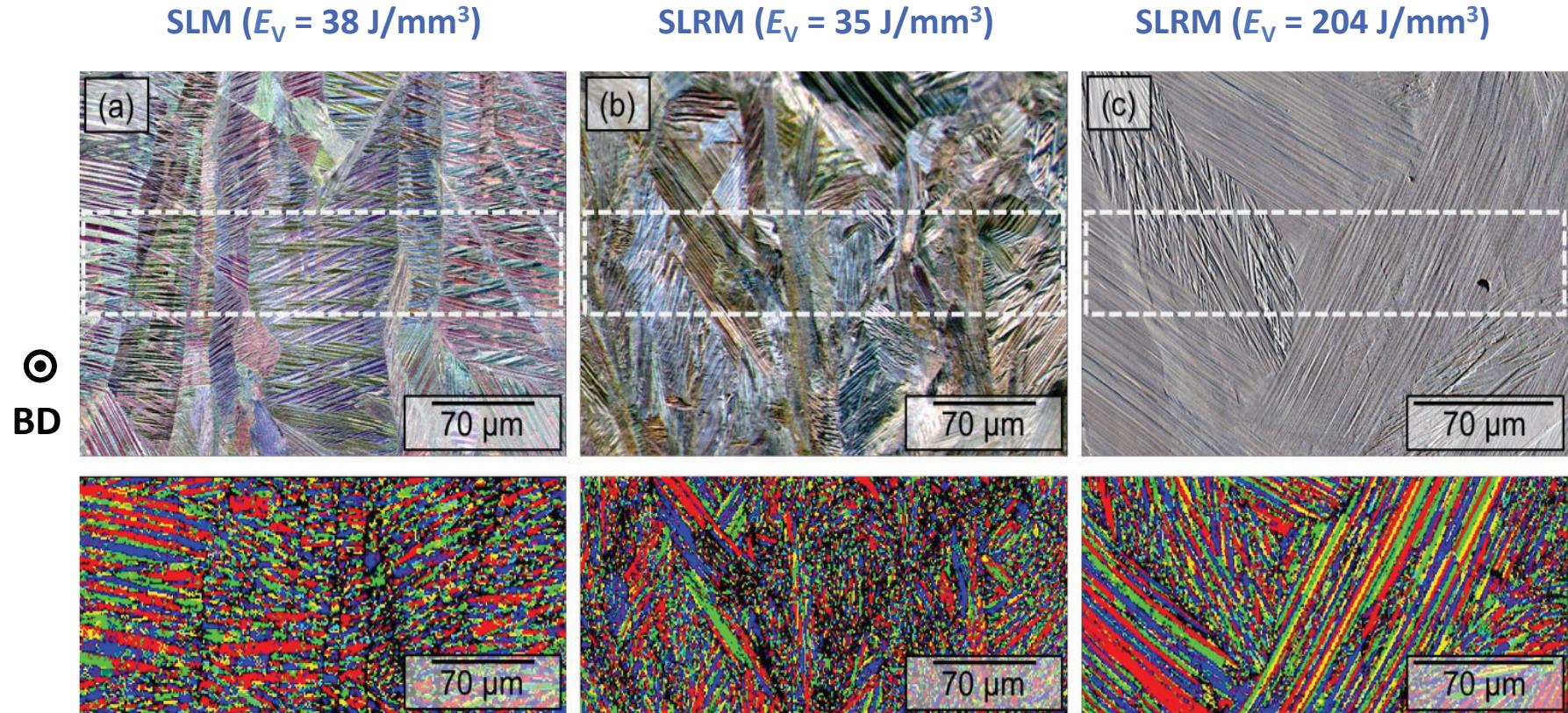
T. Gustmann et al. unpublished



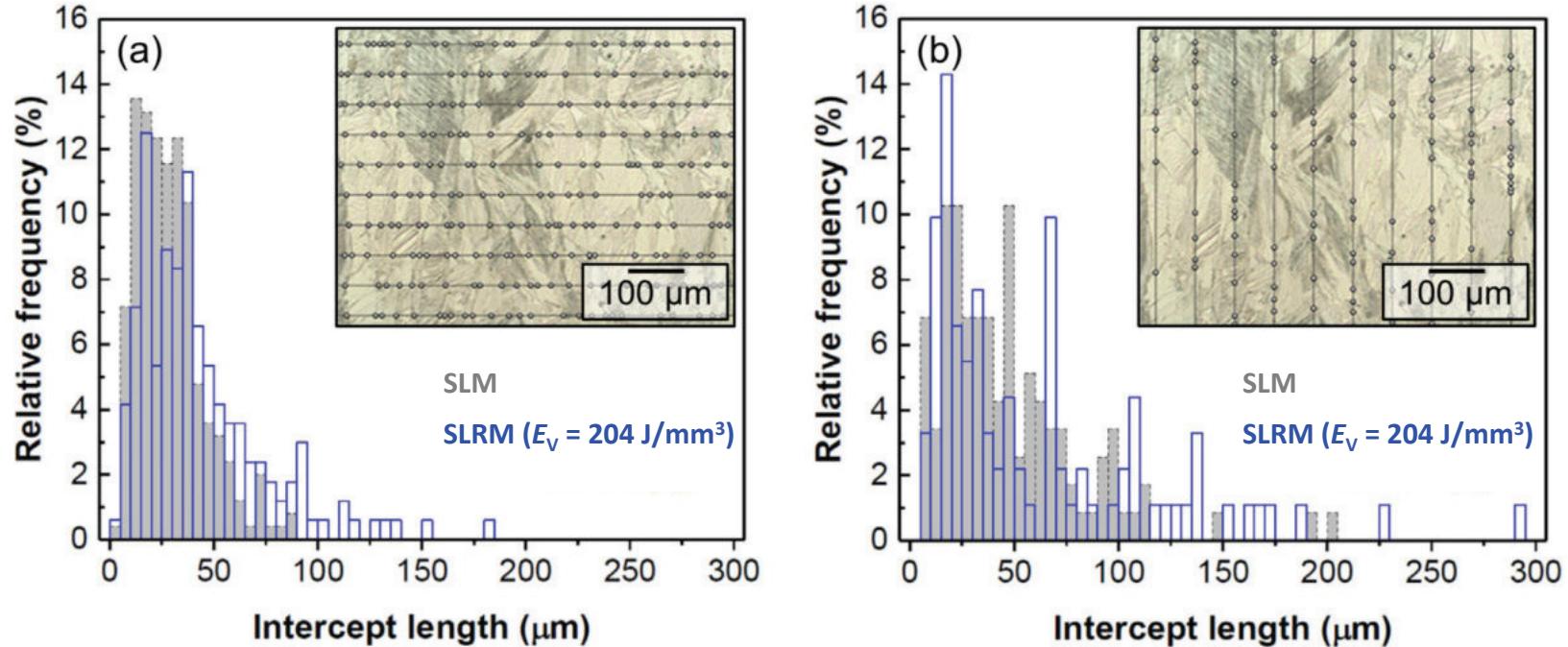
- HT1: 10 mins @ 850 °C + water quenching
- HT2: 10 mins @ 850 °C + water quenching + 60 mins @ 300 °C + slow cooling
- Suppression of DO_3 -ordering → austenite stabilization
- Different processing: large transformation temperature window



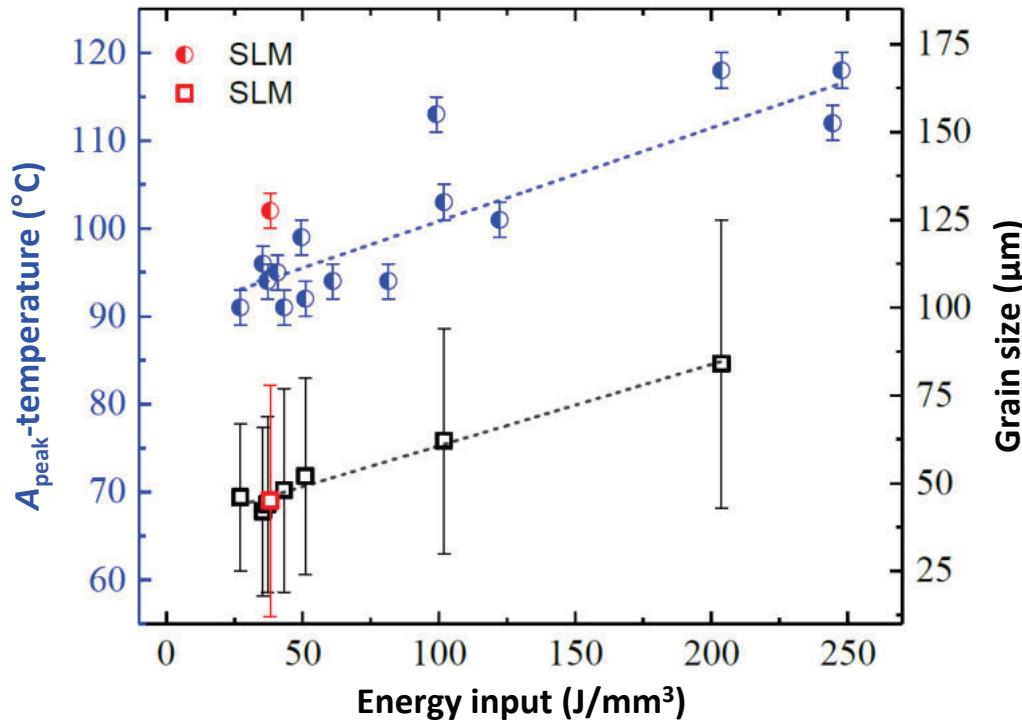
- Increase in relative density (up to 99.5%)
- Systematic variation of energy input during remelting ($30 - 250 \text{ J/mm}^3$)
- Effect on microstructure?
- Influence on transformation properties?



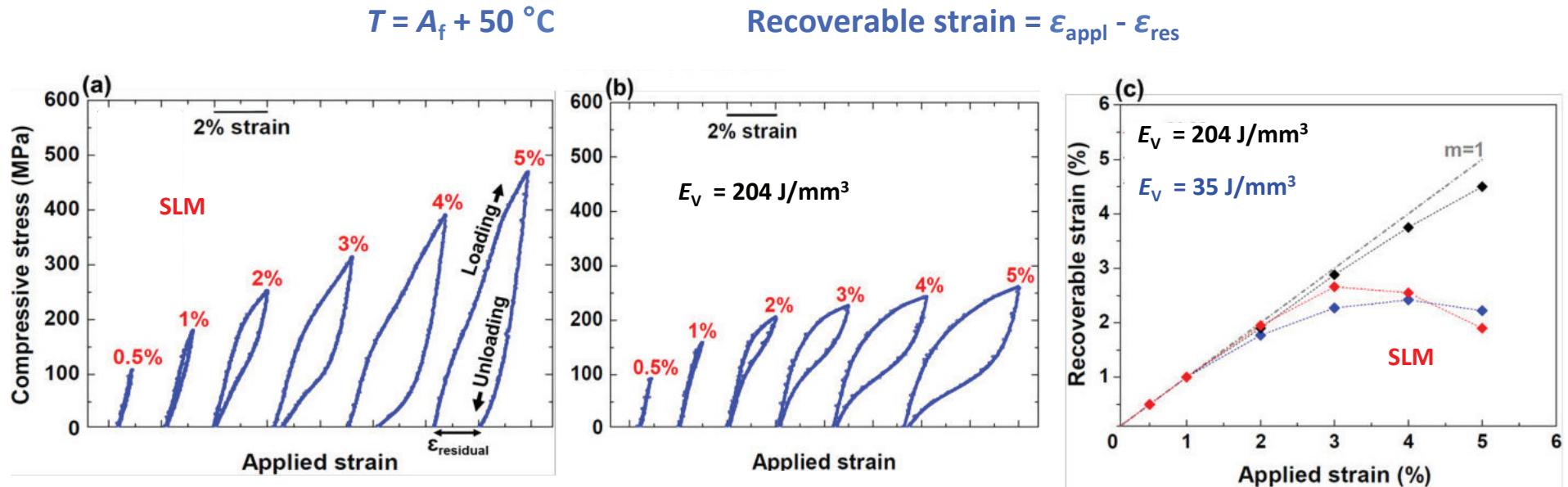
- Martensite variants become larger after remelting
- Reorientation of the variants



- Grain size determined via intercepts
- Microstructure: difficult to quantify
- Energy input ↑ (remelting), grain size ↑

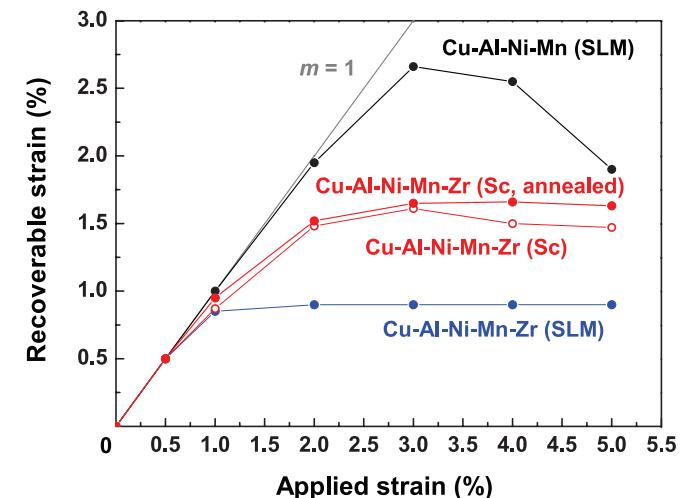


- Transformation temperature increases with grain size
- Transformation temperature window about 30 °C
- Adjust transformation temperature through parameters
- SLM: route to modify transformation temperatures even more



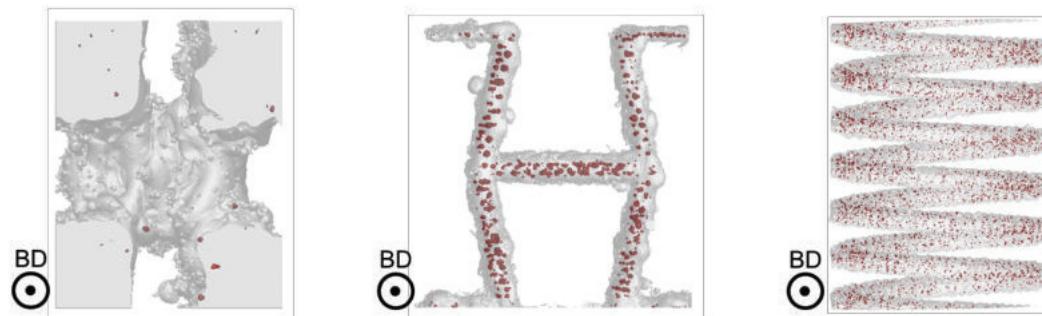
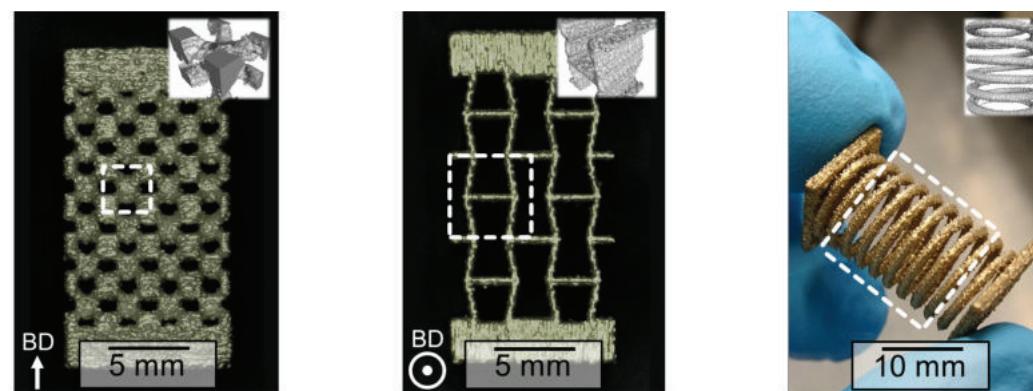
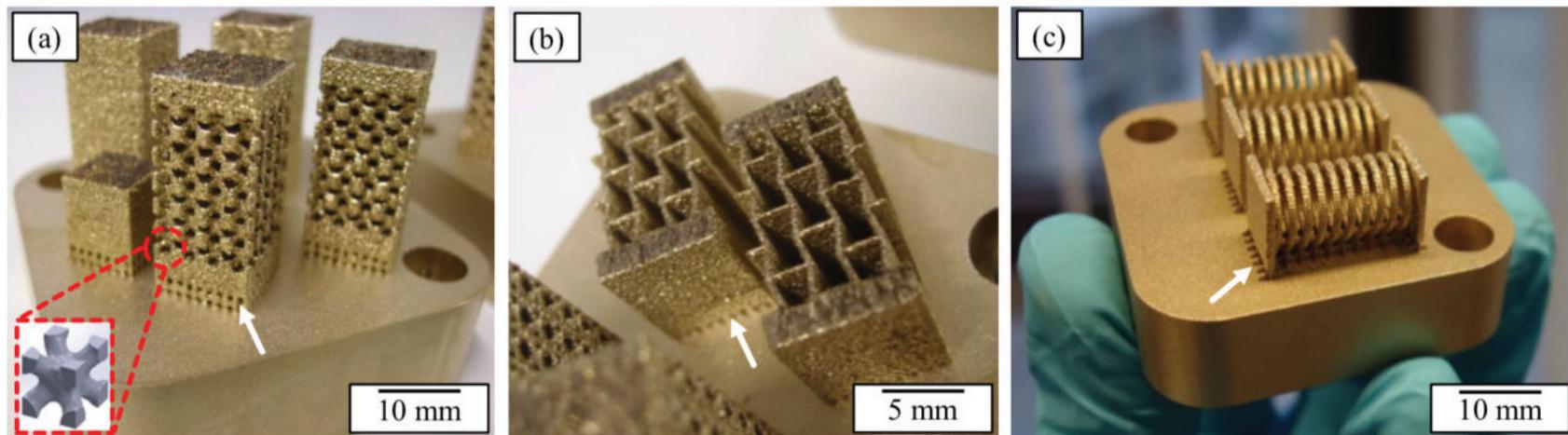
T. Gustmann et al. unpublished

- About 2% strain recovery for Cu-11.85Al-3.2Ni-3Mn (SLM)
- Remelting: strain recovery can be modified
- Almost 5% recoverable strain ($E_V = 204 \text{ J/mm}^3$)
→ exceptionally high
- Cu-Al-Ni-Mn-Zr: recoverable strain < 1%
- Cu_2AlZr might be responsible



Cu-based SMAs and SLM

19



T. Gustmann et al. unpublished

SLM of Cu-based SMAs allows:

- production of complex parts
- adjusting transformation temperatures
- optimizing shape memory properties
- local disabling of SME
- formation of graded material

→ Promising route to 4D printing

