

# What does "normal-normal transmittance" mean for light-scattering materials?



Helen Rose Wilson<sup>1</sup>, Bruno Bueno<sup>1</sup>,  
Johannes Hanek<sup>1</sup>,  
Christoph Riethmüller<sup>2</sup>, Holger Illg<sup>2</sup>,  
Bertrand Deroisy<sup>3</sup>, Tilmann E. Kuhn<sup>1</sup>

1: Fraunhofer Institute for  
Solar Energy Systems ISE

2: Deutsche Institute für Textil-  
und Faserforschung

3: Belgian Building Research Institute

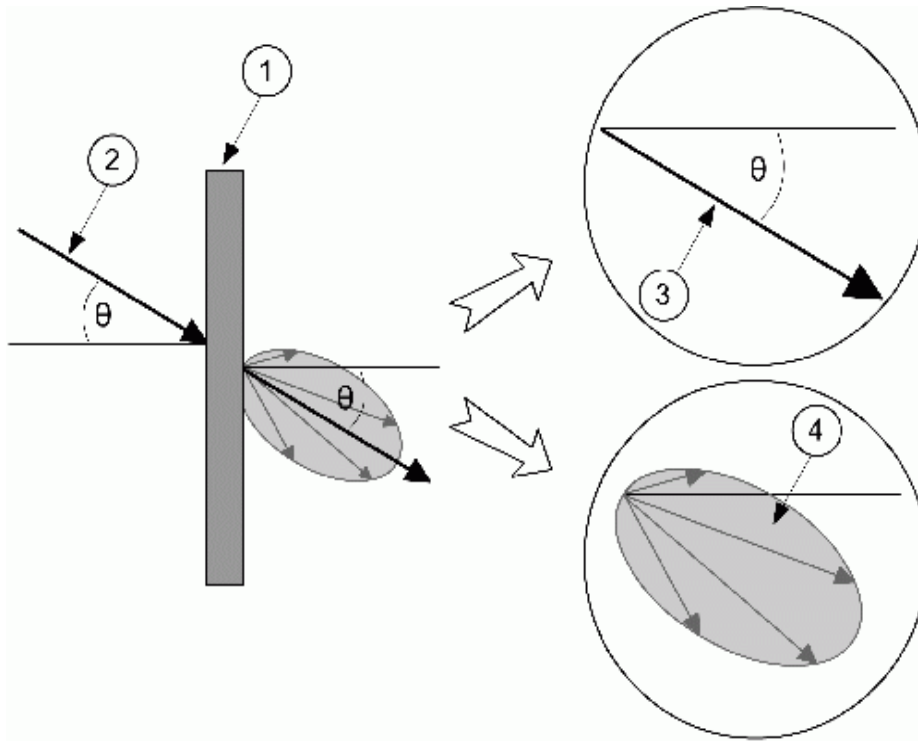
# Contents

- Motivation
- Definitions
- Determining  $\tau_{v,n-n}$  by measurement, concentrating on integrating spheres
- Characteristics of investigated solar-shading textiles
- Results for “critical” textile samples with regard to  $\tau_{v,n-n}$
- Pullback method for improved agreement in  $\tau_{v,n-n}$
- Outlook – further applications

# Motivation

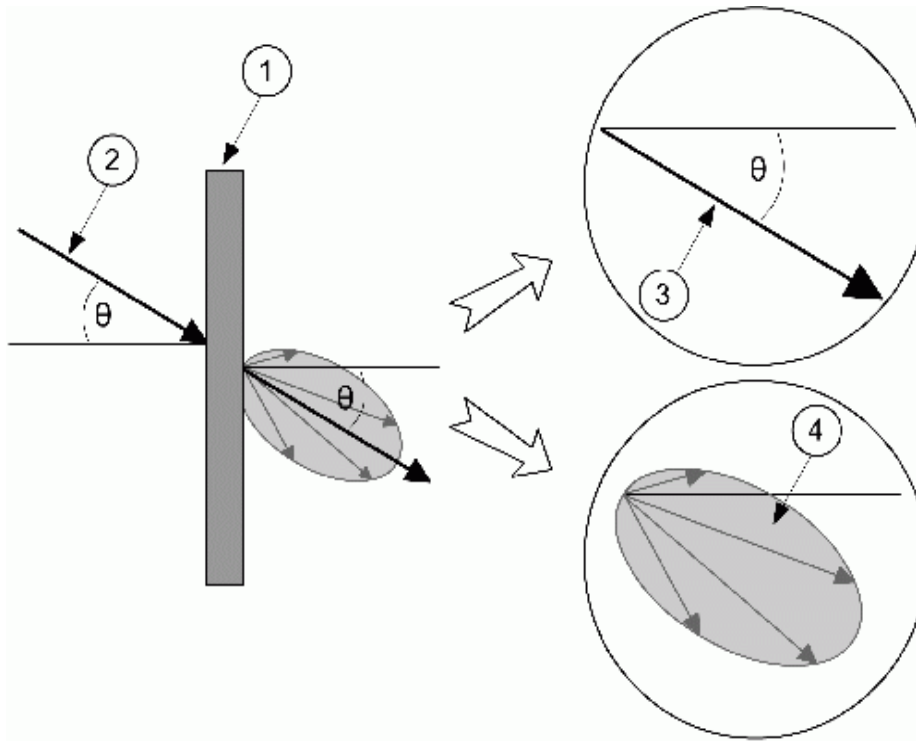
- Question: What does "normal-normal transmittance" mean for light-scattering materials?
- Answer (from EN 14500:2008):  
Fraction of normally incident radiation flux that is transmitted in accordance with the laws of geometrical optics, without diffusion or redirection
- Normal-normal transmittance is an input for performance metrics characterising solar-shading materials and glazing with respect to
  - Glare control
  - Protection against direct solar radiation
  - Night privacy
  - Visual contact with the outdoor environment

# Nomenclature referring to transmittance from EN 14500



1. Solar-shading material
2. Incident directional radiation
3. Transmitted direct component radiation
4. Transmitted diffuse component radiation

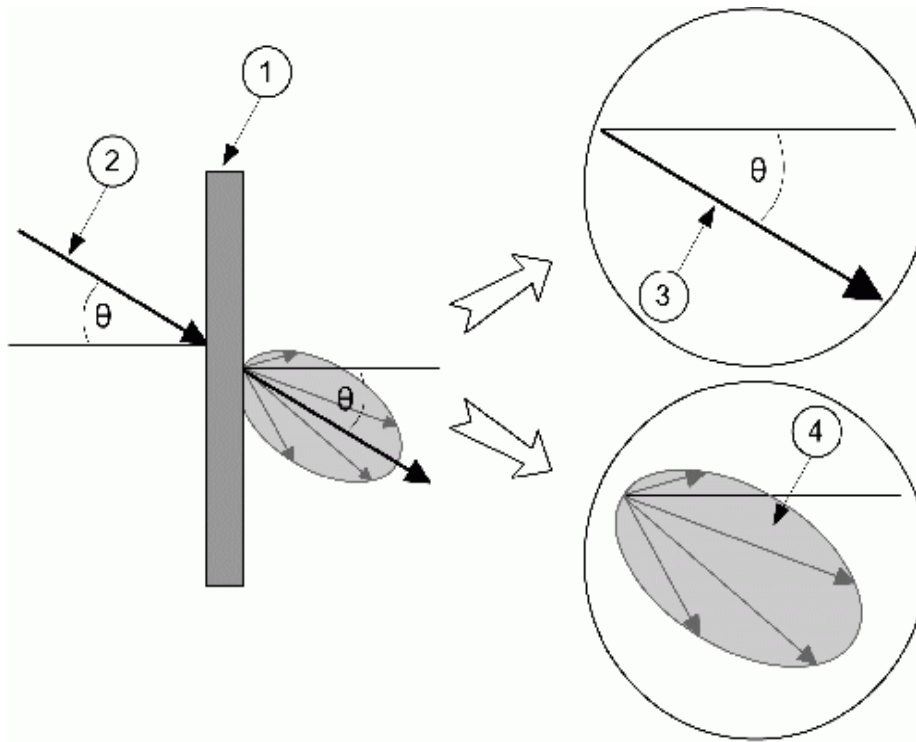
# Nomenclature referring to transmittance from EN 14500



- «  $\tau$  » transmittance
- «  $e$  » solar (energy)
- «  $v$  » visible (light)
- «  $n$  » for normal  $\theta = 0^\circ$
- «  $h$  » for hemispherical (collected in the hemisphere behind the sample plane),
- «  $dif$  » for diffuse radiation

$$\tau_{v, n-n} = \tau_{v, n-h} - \tau_{v, n-dif}$$

# Measurement methods to determine $\tau_{v, n-n}$



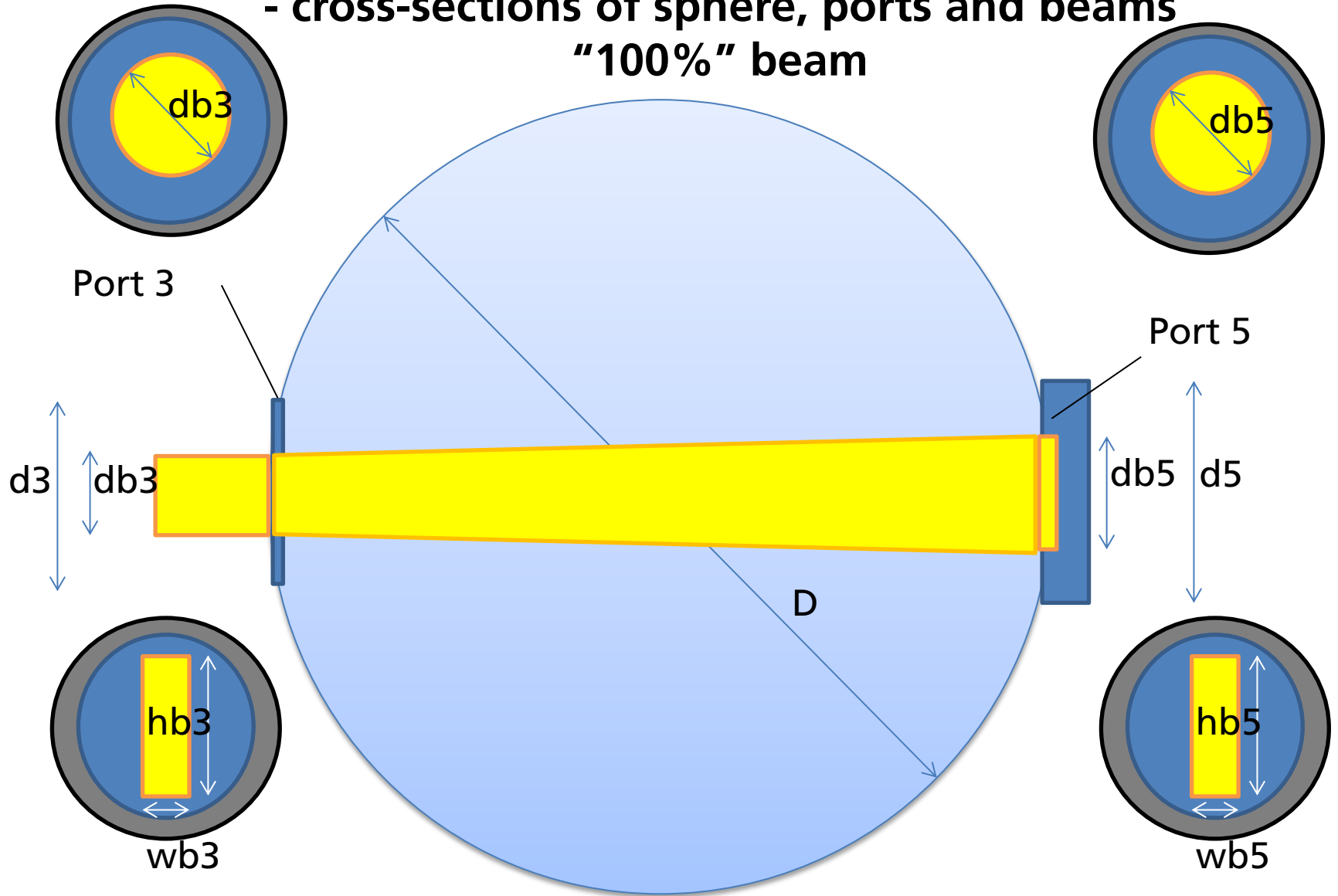
- «  $\tau$  » transmittance
- «  $e$  » solar (energy)
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- «  $h$  » for hemispherical (collected in the hemisphere behind the sample plane),
- «  $dif$  » for diffuse radiation

1. Integrating Sphere:  $\tau_{v, n-n} = \tau_{v, n-h} - \tau_{v, n-dif}$
2. Direct measurement of  $\tau_{v, n-n}$ : (see EN 14500:2018)

# Definition of geometrical parameters for integrating spheres

- cross-sections of sphere, ports and beams

"100%" beam



area of Port 3:  $a3$   
transmittance sample port

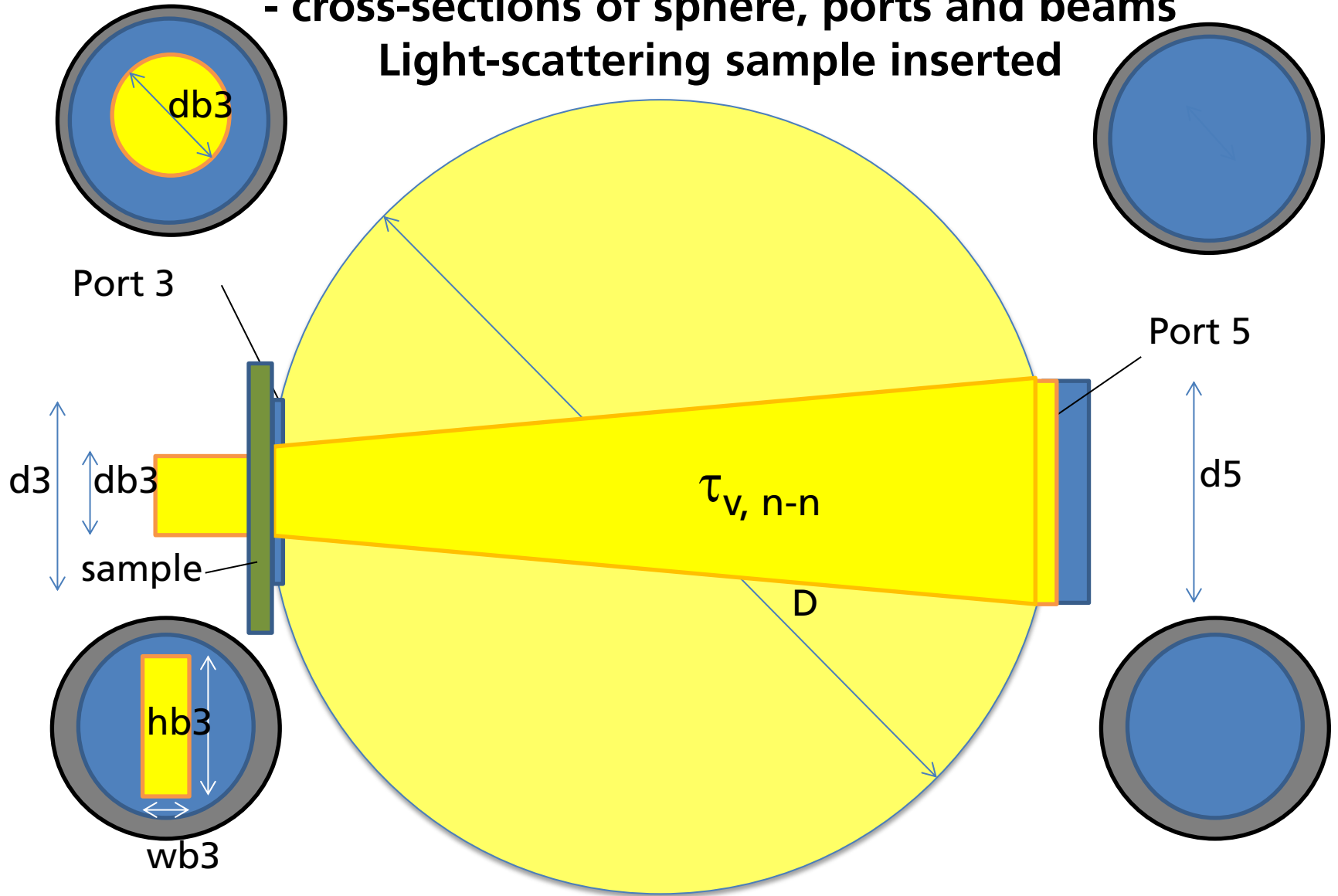
internal sphere area:  $A$

area of Port 5:  $a5$   
normal-normal transmittance exit port

# Definition of geometrical parameters for integrating spheres

- cross-sections of sphere, ports and beams

## Light-scattering sample inserted



area of Port 3:  $a3$   
transmittance sample port

internal sphere area:  $A$

area of Port 5:  $a5$   
normal-normal transmittance exit port



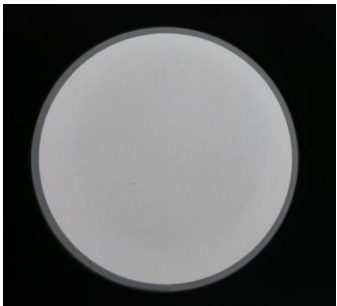
# Investigated solar-shading textiles

## - Transmitted images of light source

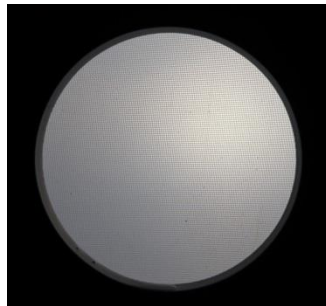
Light source



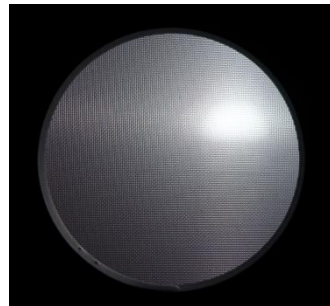
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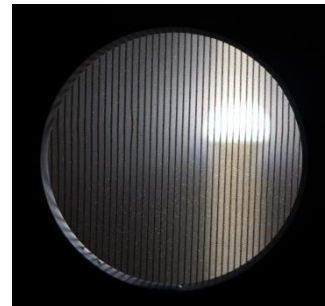
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No3



No5



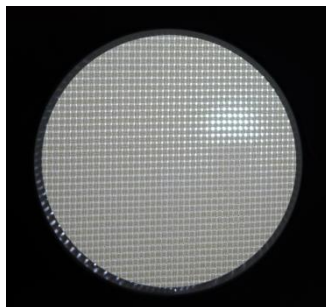
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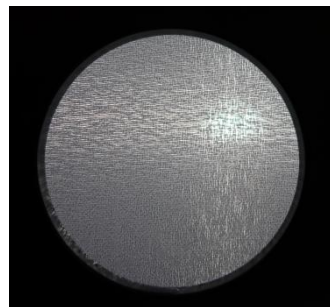
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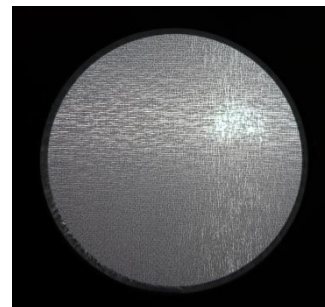
No12



No13-1



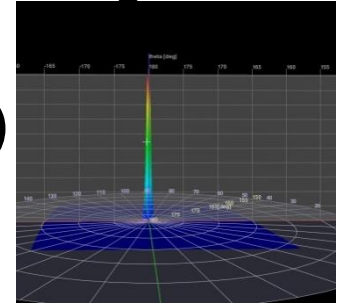
No13-2 (metallic)



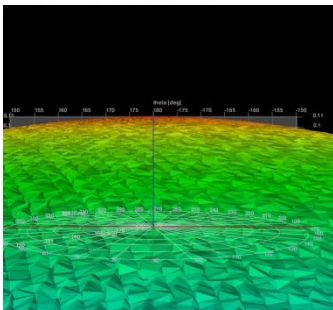
# Investigated solar-shading textiles

## - Photogoniometric transmittance images (BTDF)

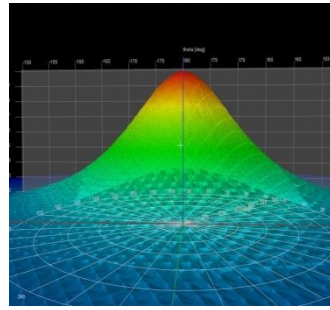
Light source



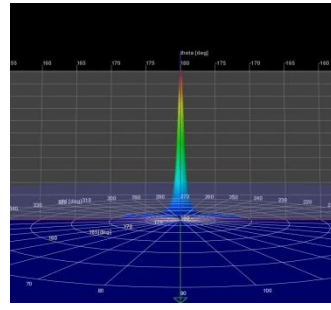
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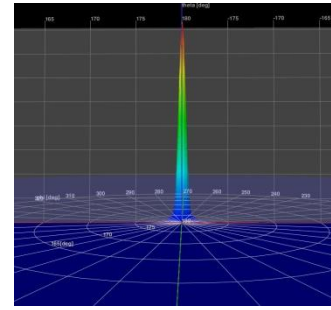
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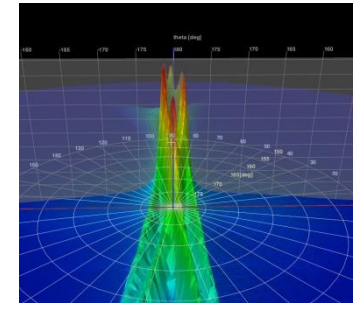
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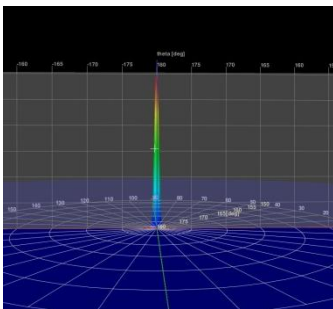
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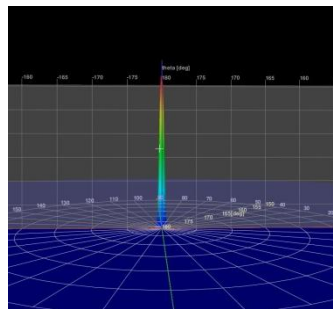
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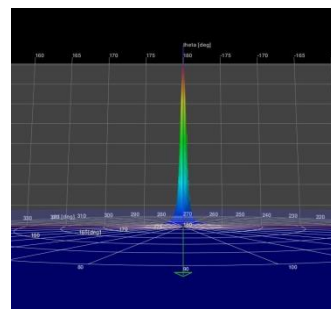
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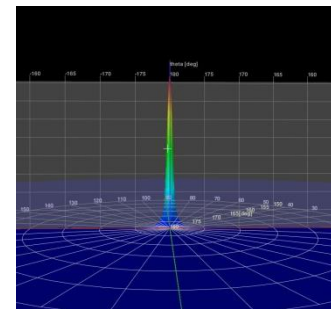
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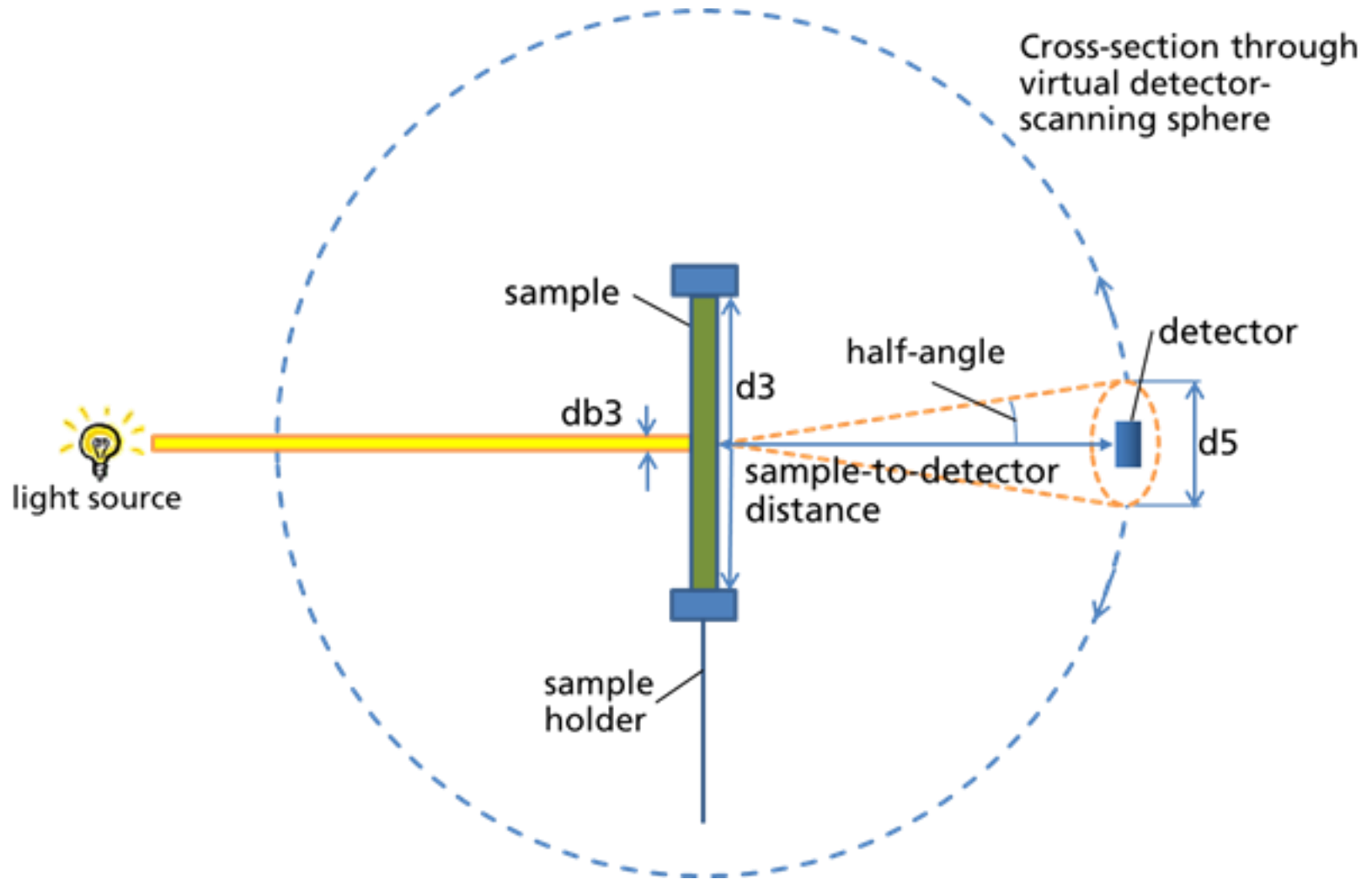
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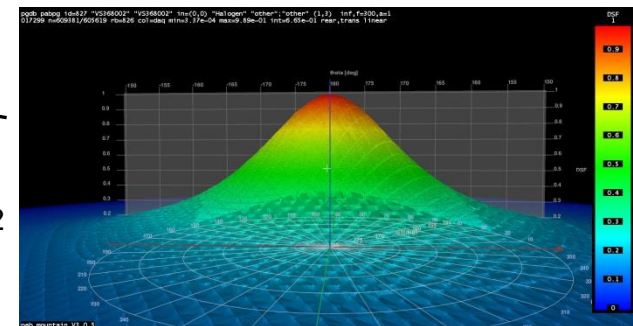
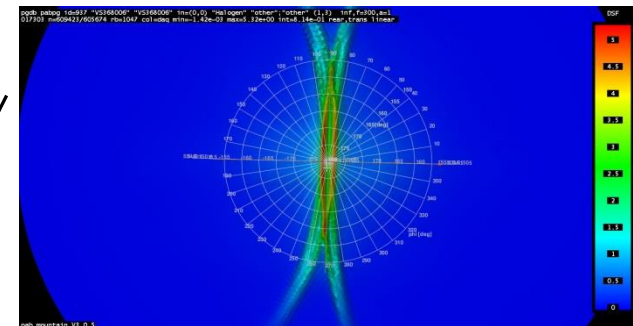
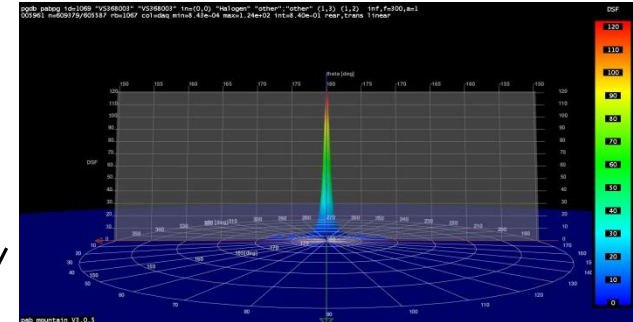
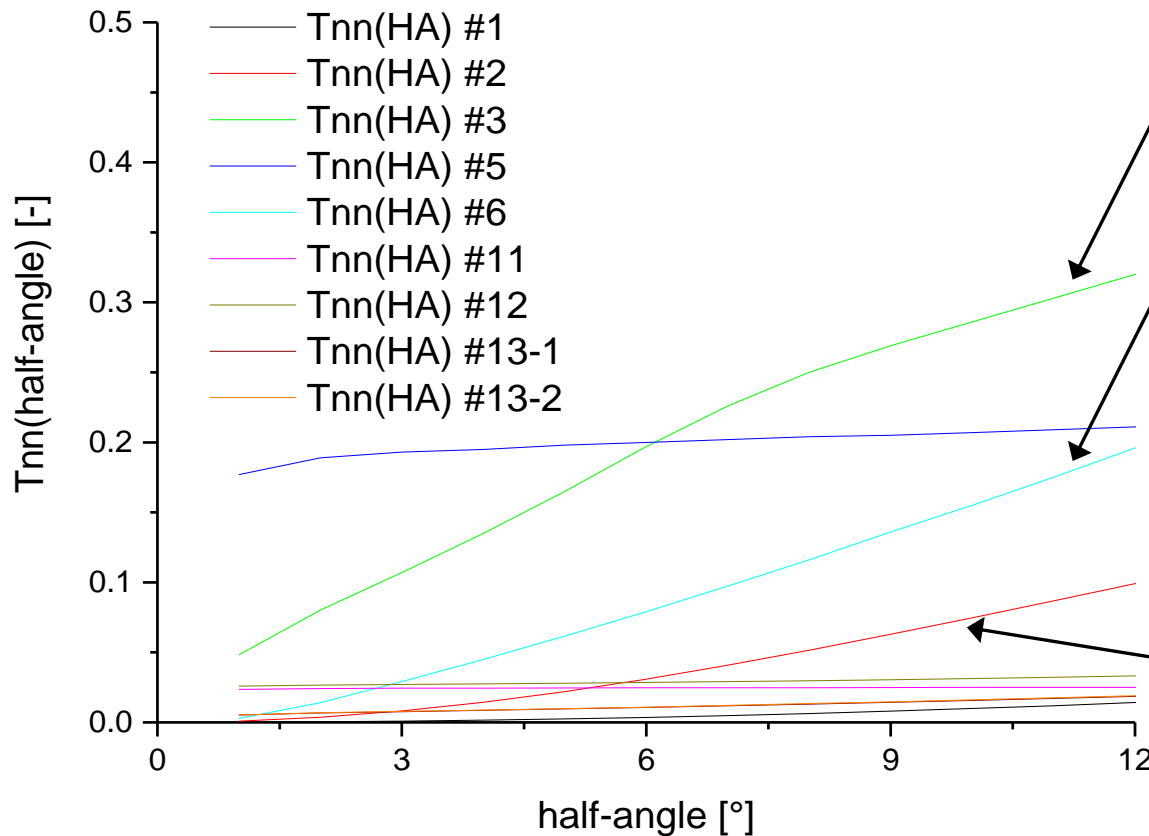
No13-2 (metallic)



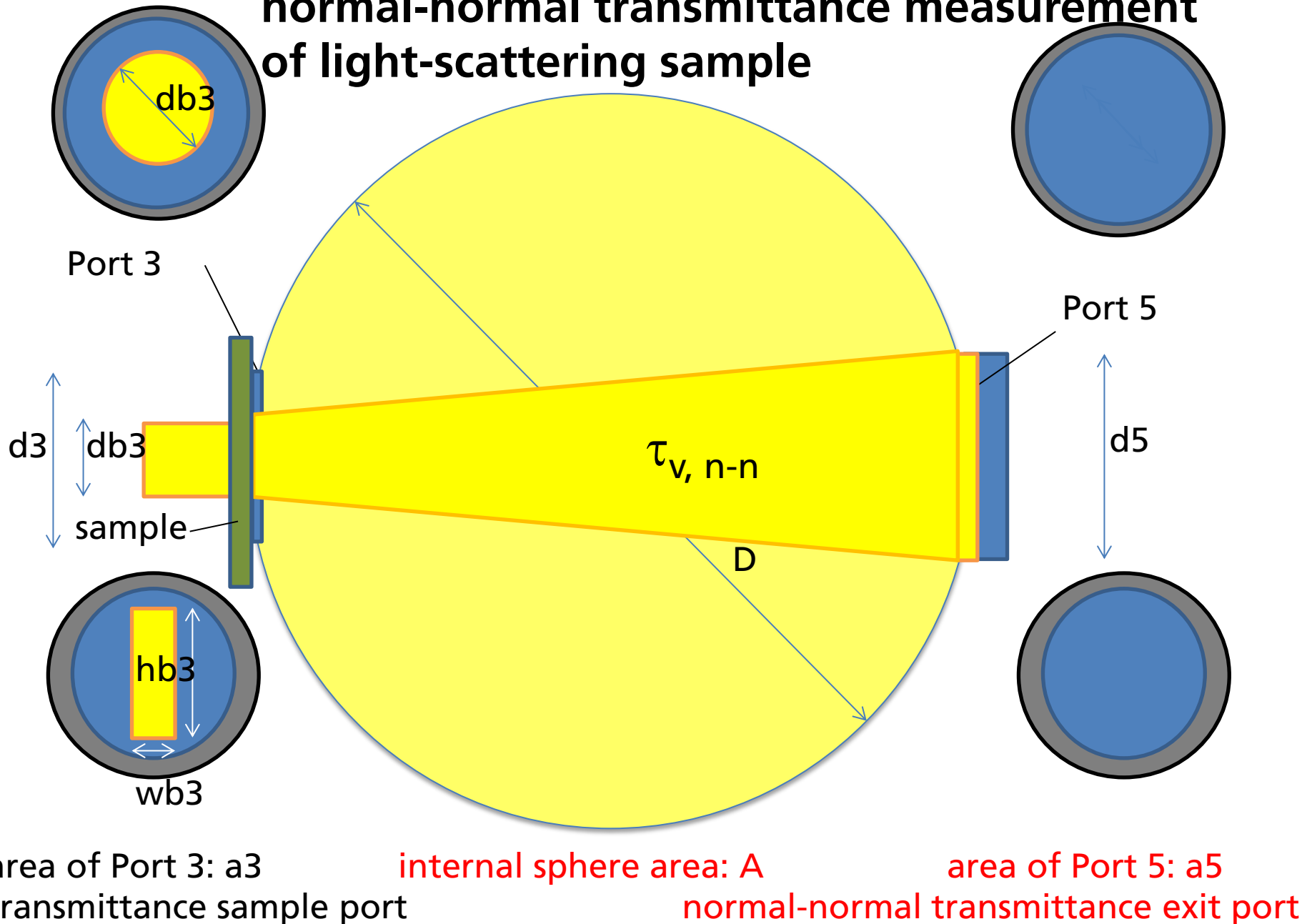
# Important parameters for the photogoniometer used for the analysis of the transmitted light



# Normal-normal transmittance obtained by integrating photogoniometric data over cap of given half-angle



# Integrating sphere configuration for normal-normal transmittance measurement of light-scattering sample



# Determining normal-normal transmittance with an integrating sphere

$$T_{nn}(\lambda) = T_{nh}(\lambda) - T_{ndif}(\lambda),$$

where  $T_{nh}(\lambda)$  is measured with Port 5 closed with a white plug and  $T_{ndif}(\lambda)$  is measured with Port 5 open.

Two hypotheses:

- If the sample at Port 3 is not moved between the  $T_{nh}(\lambda)$  and  $T_{ndif}(\lambda)$  measurements,  **$T_{nn}(\lambda)$  can be determined from the equation above** even when the  $T_{nh}(\lambda)$  and  $T_{ndif}(\lambda)$  values themselves are incorrect (errors are identical for both measurements)
- The determined value of  $T_{nn}(\lambda)$  depends on  $a_5/A$ 
  - how much depends on the sample scattering distribution

## First hypothesis:

$T_{nn}(\lambda)$  can be determined from  $T_{nn}(\lambda) = T_{nh}(\lambda) - T_{ndif}(\lambda)$

- if sample at Port 3 is not moved between  $T_{nh}(\lambda)$  and  $T_{ndif}(\lambda)$  measurements
- despite incorrect  $T_{nh}(\lambda)$  and  $T_{ndif}(\lambda)$  values (errors are practically identical for both measurements)

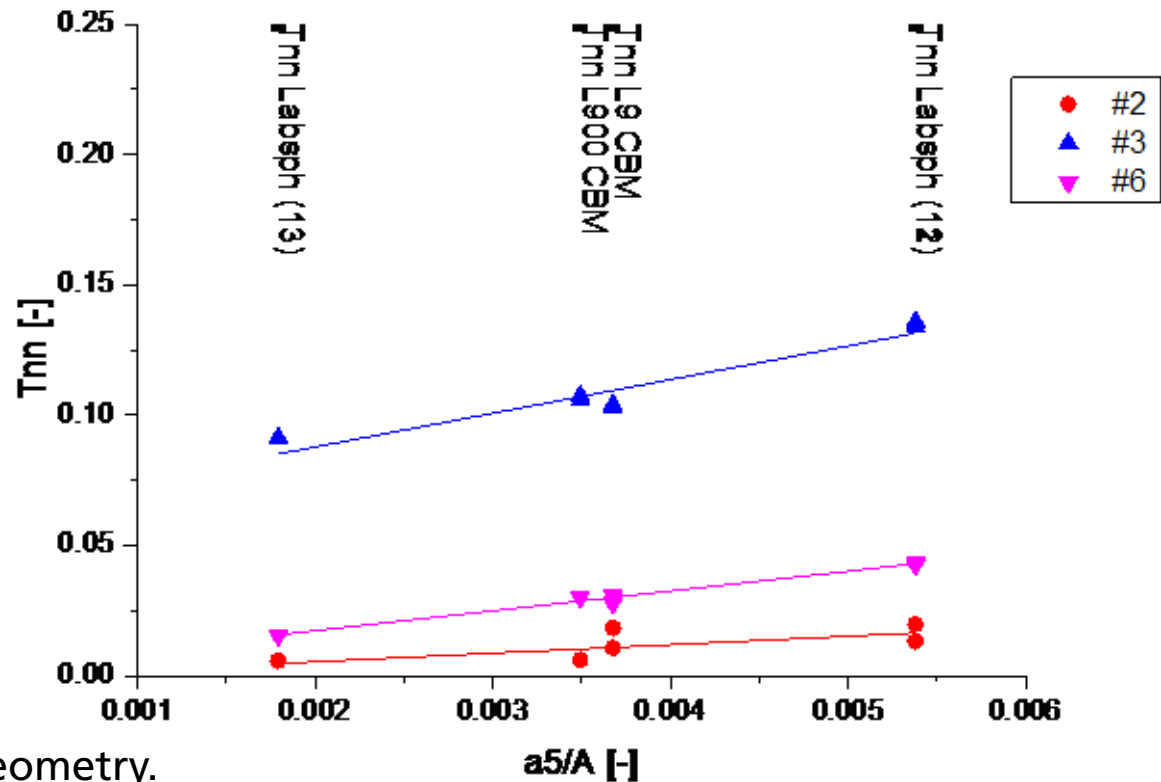
Typical causes of errors in  $T_{nh}(\lambda)$  and  $T_{ndif}(\lambda)$  determination:

- Losses due to lateral light shift within sample
- Inhomogeneous reflectance of sphere wall (including Port 5 plug)
- Departure from ideal spherical geometry (ports, detectors, baffles)
- Detector field of view (assuming this does not include Port 5)

## Second hypothesis: $T_{nn}$ ( $= T_{nh} - T_{ndif}$ ) depends on $a5/A$

$T_{v,nn}$  versus  $a5/A$  for three „critical“ textile samples (#2, #3, #5):

“Critical” refers to variation of  $T_{v,nn}$  value with  $a5/A$



$a5/A$  varied by sphere geometry.

Labsph 11, 12, 13, L9, L900 refer to integrating spheres with different dimensions.

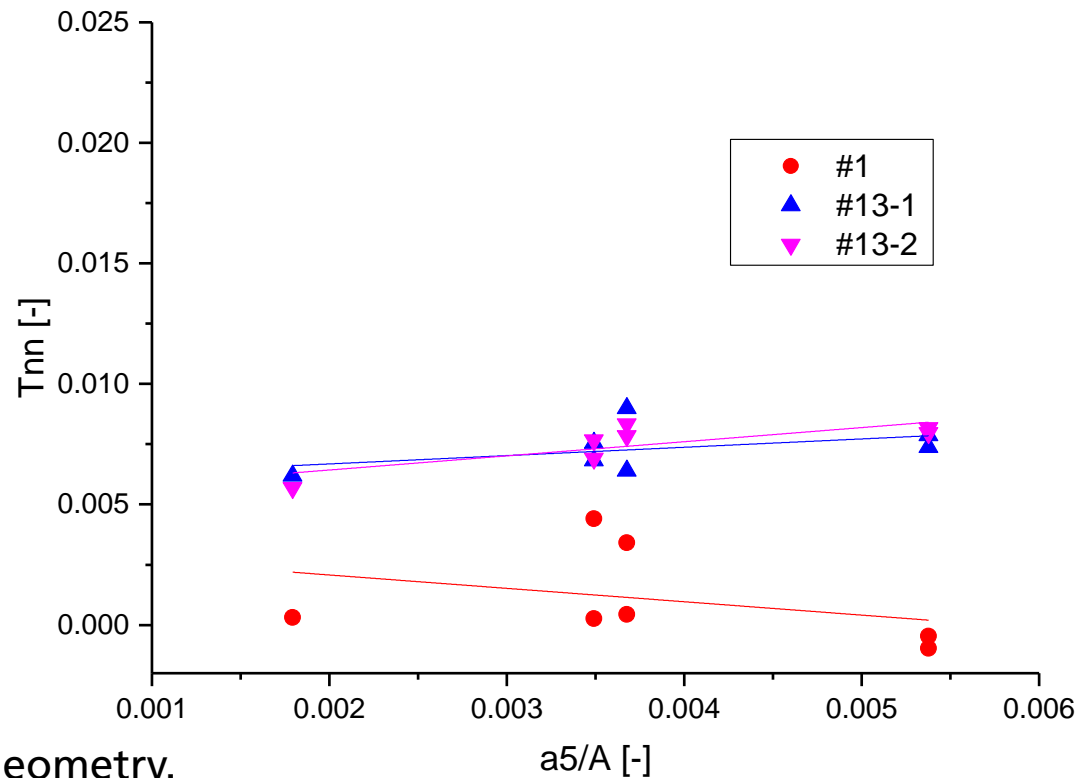


**Second hypothesis:  $T_{nn}$  ( $= T_{nh} - T_{ndif}$ ) depends on  $a5/A$**

**- but is significant only for “critical” samples**

$T_{v,nn}$  versus  $a5/A$  for three „non-critical“ textile samples (#1, #13-1, #13-2):

“Critical” refers to variation of  $T_{v,nn}$  value with  $a5/A$



$a5/A$  varied by sphere geometry.

**Note reduction in y-axis scaling compared to previous slide!**

# Problem

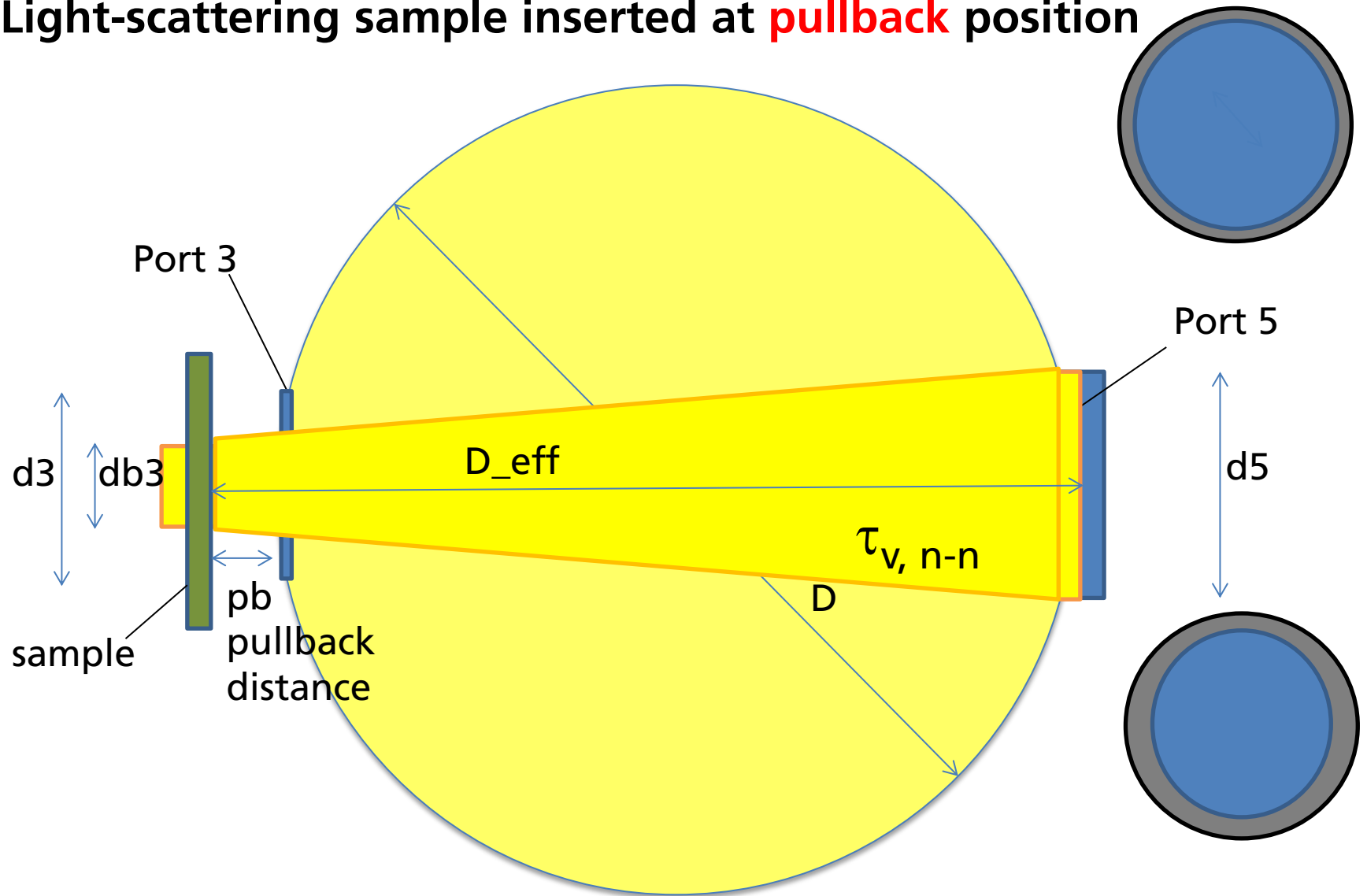
As  $T_{nn}(\lambda)$  ( $= T_{nh}(\lambda) - T_{ndif}(\lambda)$ ) depends on  $a5/A$ ,

how can  $T_{nn}(\lambda)$  be determined reproducibly with different integrating spheres?

## Solution:

- Limit the allowable range of  $a5/A$  (or  $a5/A_{eff}$ : see below)
- Apply the pullback method to measure within this range

# Definition of geometrical parameters for integrating spheres: Light-scattering sample inserted at **pullback** position



area of Port 3:  $a3$   
transmittance sample port

internal sphere area:  $A$   
normal-normal transmittance

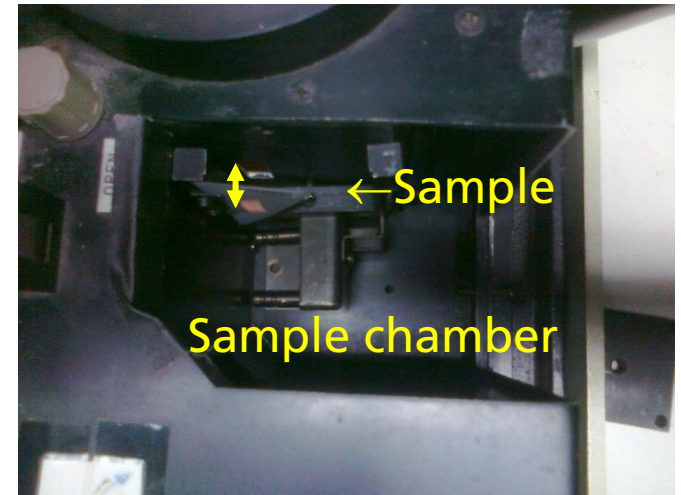
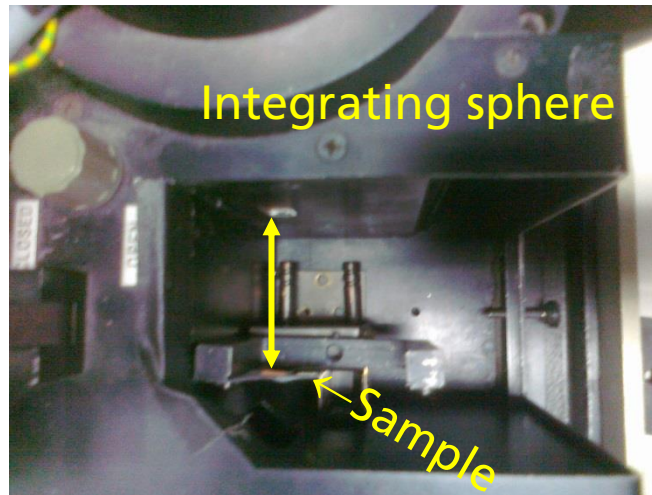
area of Port 5:  $a5$   
exit port

# Pullback of sample from transmittance port (port 3)

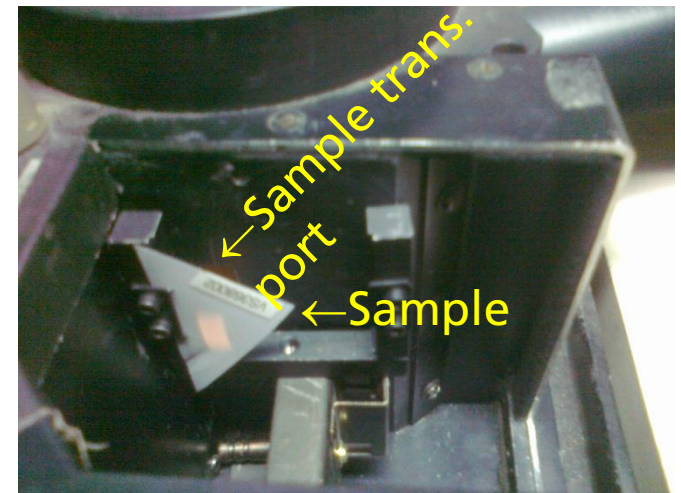
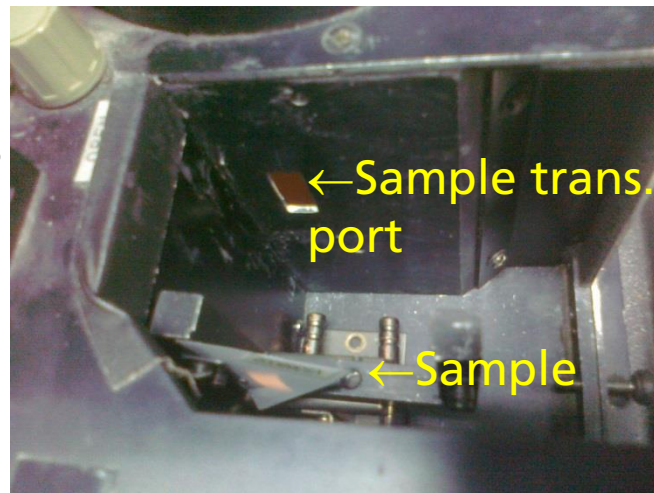
53 mm pullback

12 mm pullback

Top views



Oblique views



If pb is the pullback distance,  $D_{\text{eff}} = D + \text{pb}$

and  $A_{\text{eff}} = \pi (D_{\text{eff}})^2$

# $T_{nn}$ with and without pullback for Screen S2 col S065 white grey (non-critical for $T_{nn}$ )

For integrating spheres (220 mm, 150 mm) at Fraunhofer ISE

D [mm]	Pullback [mm]	$a_5/A$ or $a_5/A_{eff}$	$T_{nh}$ (pseudo) [-]	$T_{ndif}$ (pseudo) [-]	$T_{nn}$ [-] (550 nm or vis)
220	75	0.00194	0.0380	0.0025	0.0355
220	0	0.00349	0.0788	0.0438	0.0350
150	0	0.00368	0.0774	0.0412	0.0361

Good agreement between  $T_{nn}$  results with sample at Port 3 (pullback = 0 mm) and at pullback = 75 mm – despite low  $a_5/A_{eff}$  value

# $T_{nn}$ with and without pullback for Screen S2 col S094 white pearl (non-critical for $T_{nn}$ )

For integrating spheres (220 mm, 150 mm) at Fraunhofer ISE

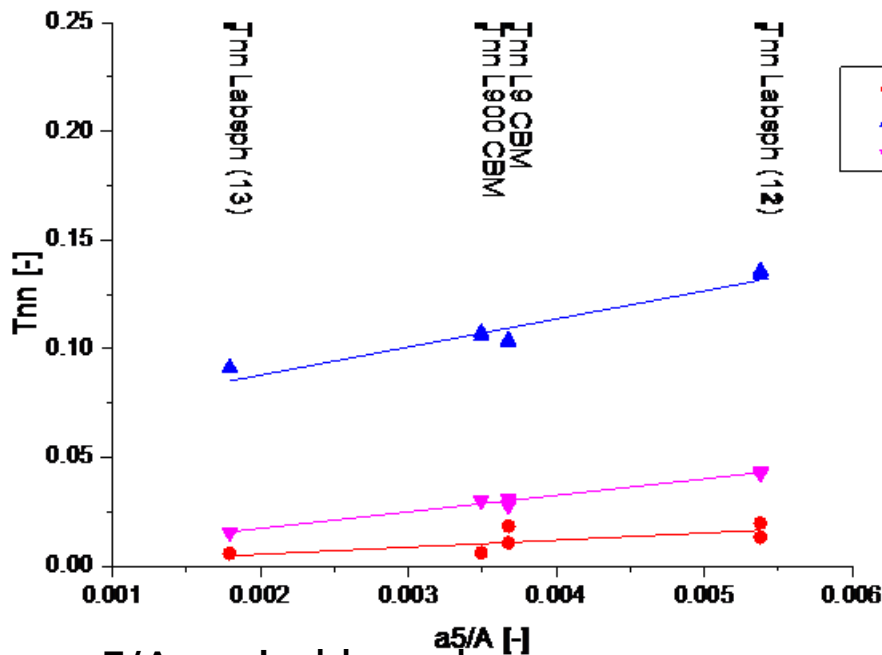
D [mm]	Pullback [mm]	$a_5/A$ or $a_5/A_{eff}$	$T_{nh}$ (pseudo) [-]	$T_{ndif}$ (pseudo) [-]	$T_{nn}$ [-] (550 nm or vis)
220	75	0.00194	0.0380	0.0033	0.0347
220	0	0.00349	0.1094	0.0722	0.0371
150	0	0.00368	0.1087	0.0722	0.0365

Good agreement between  $T_{nn}$  results with sample at Port 3 (pullback = 0 mm) and at pullback = 75 mm – despite low  $a_5/A_{eff}$  value

# Comparison for three „critical“ textile samples (2, 3, 5) - Dependence of $T_{nn}$ on $a5/A$ or $a5/A_{eff}$

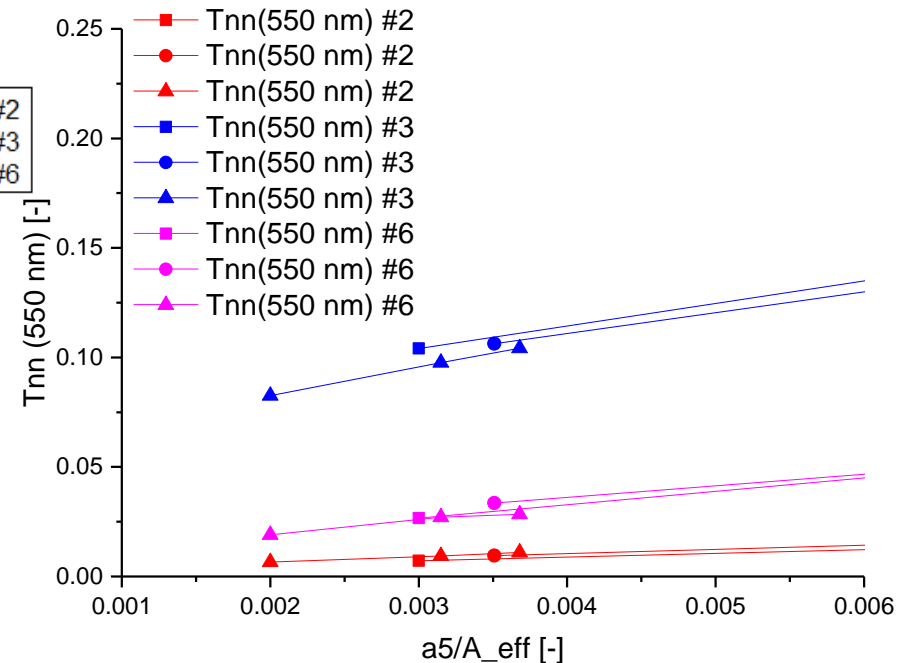
“Critical” refers to variation of  $T_{nn}$  value with  $a5/A$

$T_{v,nn}$  versus  $a5/A$



$a5/A$  varied by sphere geom.  
Labsph 11, 12, 13, L9, L900 refer to  
different integrating spheres

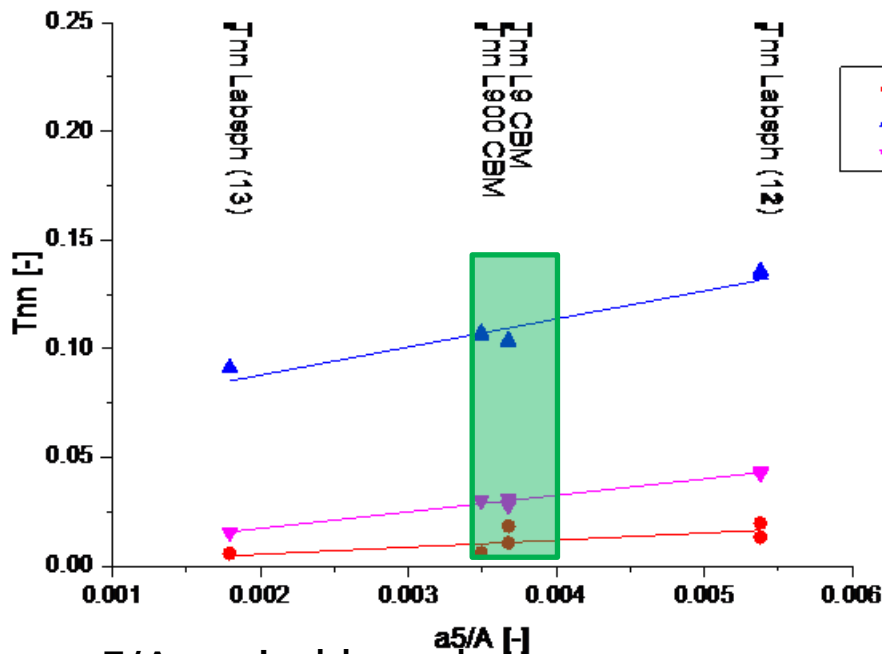
$T_{nn}(550 \text{ nm})$  versus  $a5/A_{eff}$



Pullback results using three  
different 150 mm spheres

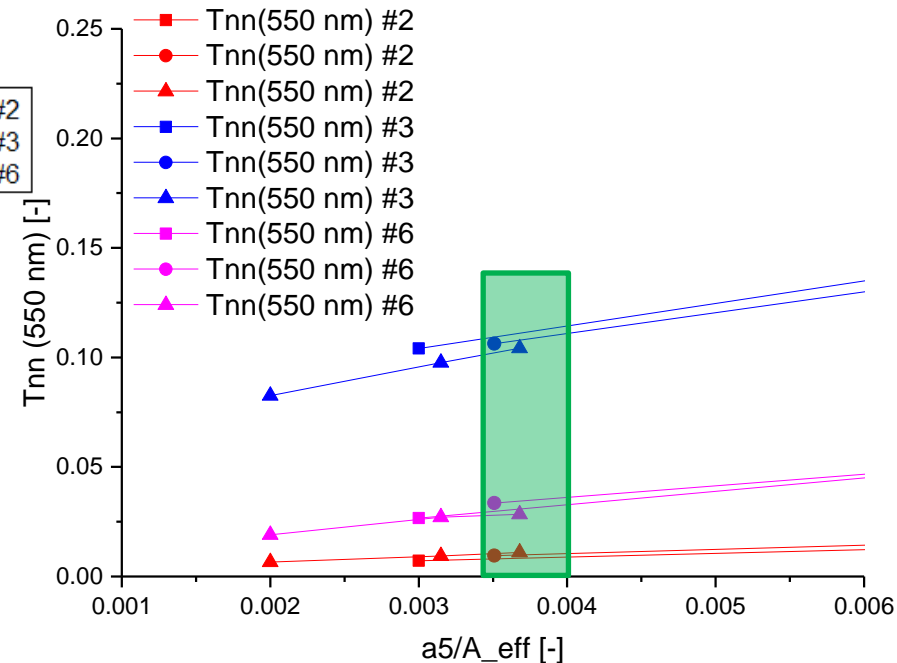
# Comparison for three “critical” textile samples (2, 3, 5) - Dependence of $T_{nn}$ on $a5/A$ or $a5/A_{eff}$ -> limit allowable values of $a5/A$ or $a5/A_{eff}$

$T_{v,nn}$  versus  $a5/A$



$a5/A$  varied by sphere geom.  
Labsph 11, 12, 13, L9, L900 refer to  
different integrating spheres

$T_{nn}(550 \text{ nm})$  versus  $a5/A_{eff}$

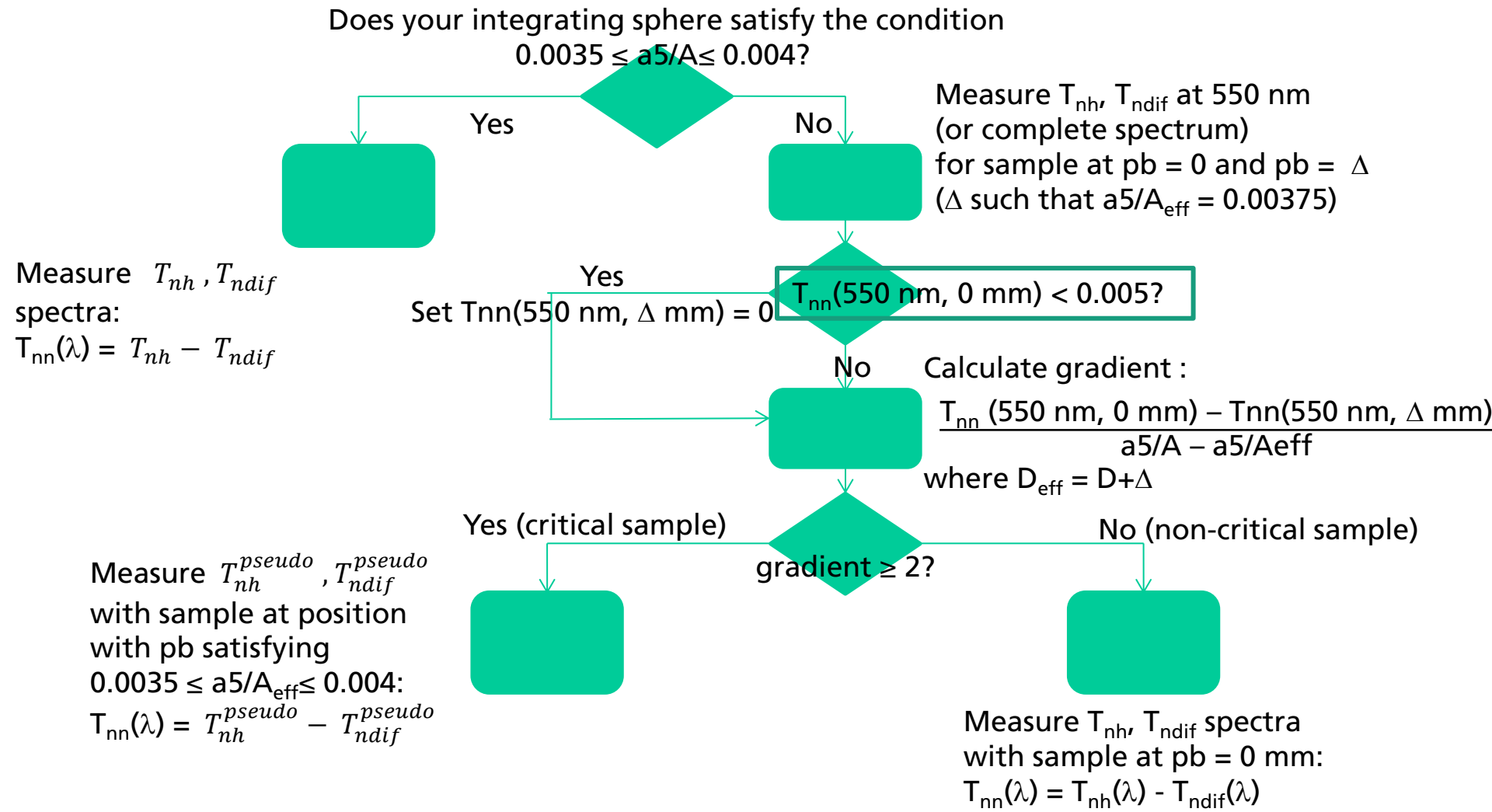


Pullback results using  
three different spheres



# Revised decision tree for $T_{nn}$ measurements

Def.:  $T_{nn}$  of "critical" samples varies significantly with the relative area of port 5



**Caution:** Special instrumentation may be needed

© Fraunhofer ISE to measure the correct values of  $T_{nh}, T_{ndif}$

# Conclusions

What does "normal-normal transmittance" mean for light-scattering materials?

- Answer (from EN 14500:2008):  
Fraction of normally incident radiation flux that is transmitted in accordance with the laws of geometrical optics, without diffusion or redirection
- Answer (if determined using an integrating sphere):  
 $T_{nn}(\lambda) = T_{nh}(\lambda) - T_{ndif}(\lambda)$ 
  - $T_{nn}(\lambda)$  is valid, even if  $T_{nh}(\lambda)$  and  $T_{ndif}(\lambda)$  are not, as the main errors cancel out

As  $T_{nn}(\lambda)$  depends on the relative area of the exit port ( $a_5/A$  or  $a_5/A_{eff}$ ), the range of this relative area must be restricted to achieve comparability.

- The pullback method is a practicable method to achieve this.
  - $T_{nn}(\lambda) = T_{nh}^{pseudo} - T_{ndif}^{pseudo}$  in this case.

# Outlook

- CEN TC33, WG3, TG5 intends to adopt the approach of restricting the range for  $a_5/A$  or  $a_5/A_{\text{eff}}$  and allowing the pullback method to determine  $T_{\text{nn}}$  in its revision of EN 14500 for solar-shading materials.
- As the approach should be valid for other light-scattering materials, the NFRC Diffuse Glazing TG is also currently considering its adoption.

# Supplementary information

For an 150 mm integrating sphere and Port 5 with a diameter of 25 mm:

$a5/A_{\text{eff}}$	$p_b$ [mm]	$D_{\text{eff}}$
0.003	78.2	228.2
0.0035	61.3	211.3
0.00375	54.1	204.1
0.004	47.6	197.6
0.0069	0	150

$p_b$  = pullback = distance between sample and Port 3 in mm

# Thank you for your attention!



## Fraunhofer Institute for Solar Energy Systems ISE

Helen Rose Wilson

[www.ise.fraunhofer.de](http://www.ise.fraunhofer.de)

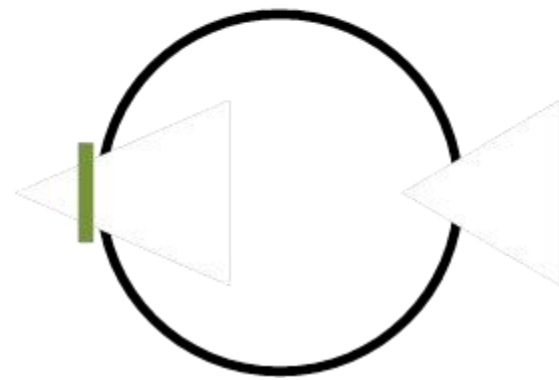
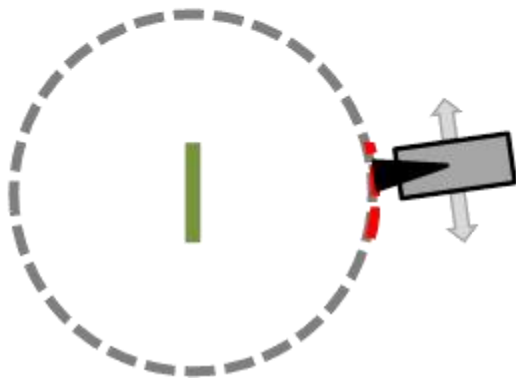
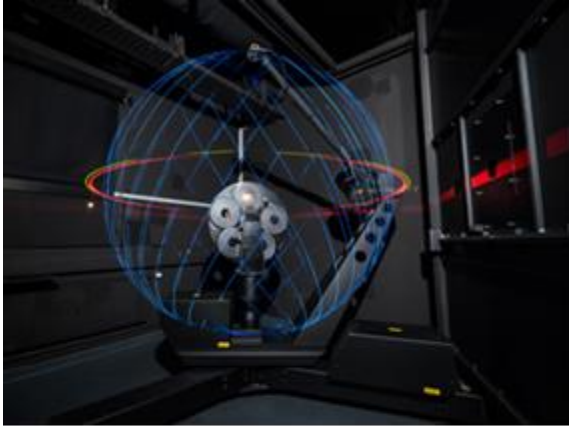
[helen.rose.wilson@ise.fraunhofer.de](mailto:helen.rose.wilson@ise.fraunhofer.de)

### Acknowledgement

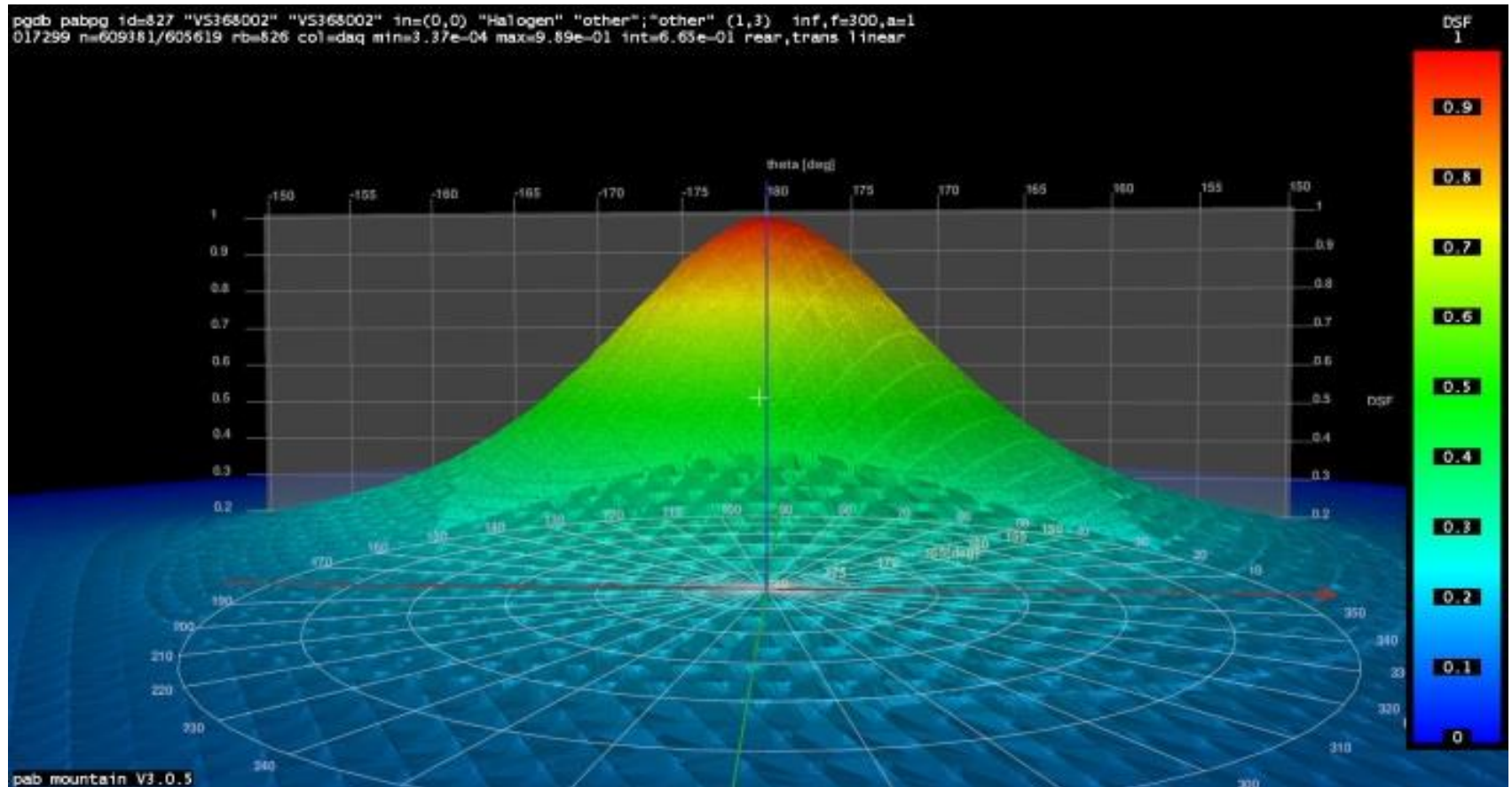
The work reported has been supported by the German Federal Ministry for Economics and Energy within the "Textil-KFFS" project with the funding number 03ET1432A.

# Supplementary slides

# Photogoniometer versus integrating sphere

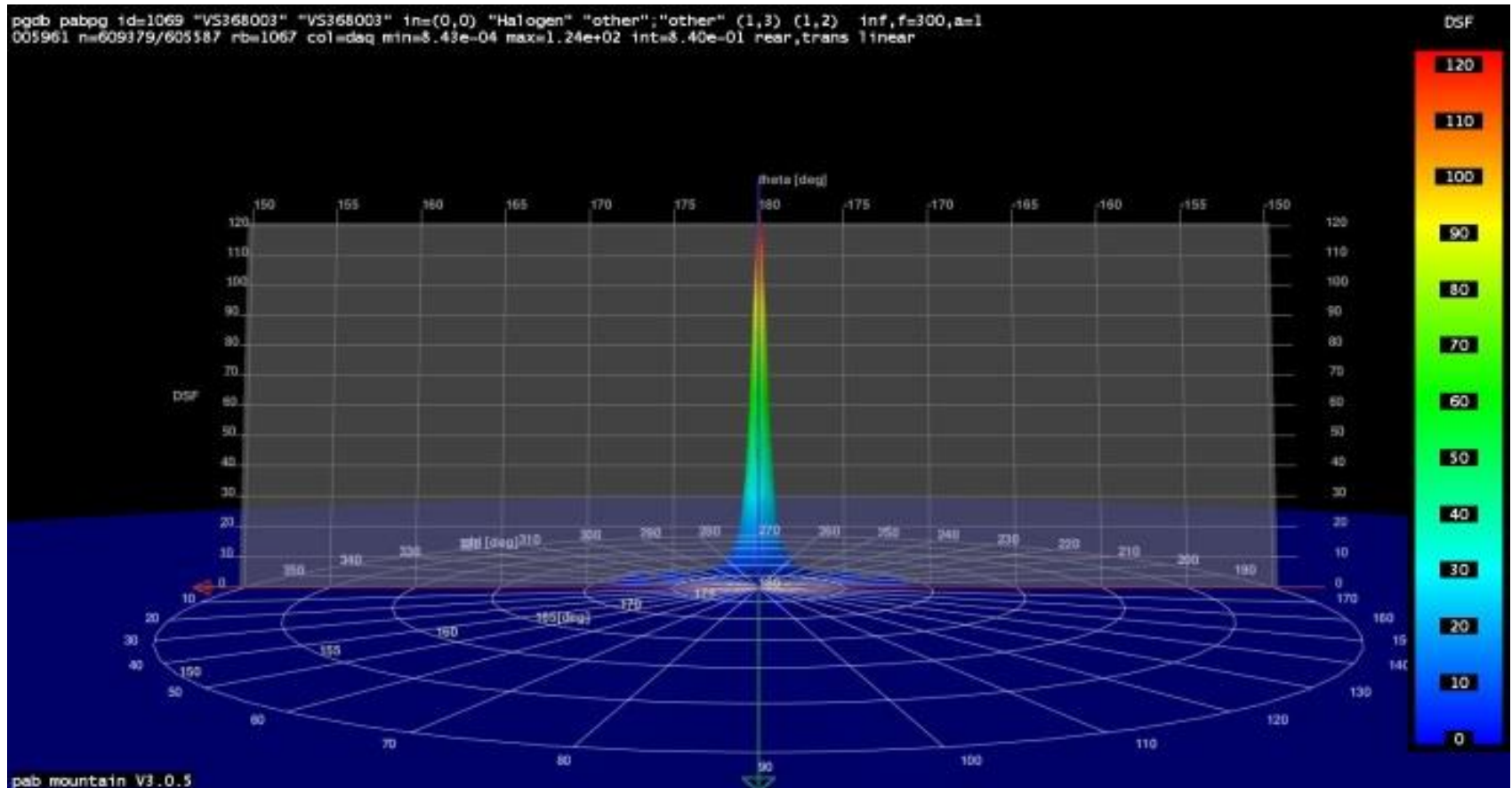


# $\tau_{n-n}$ : BDTF of "critical" sample #2

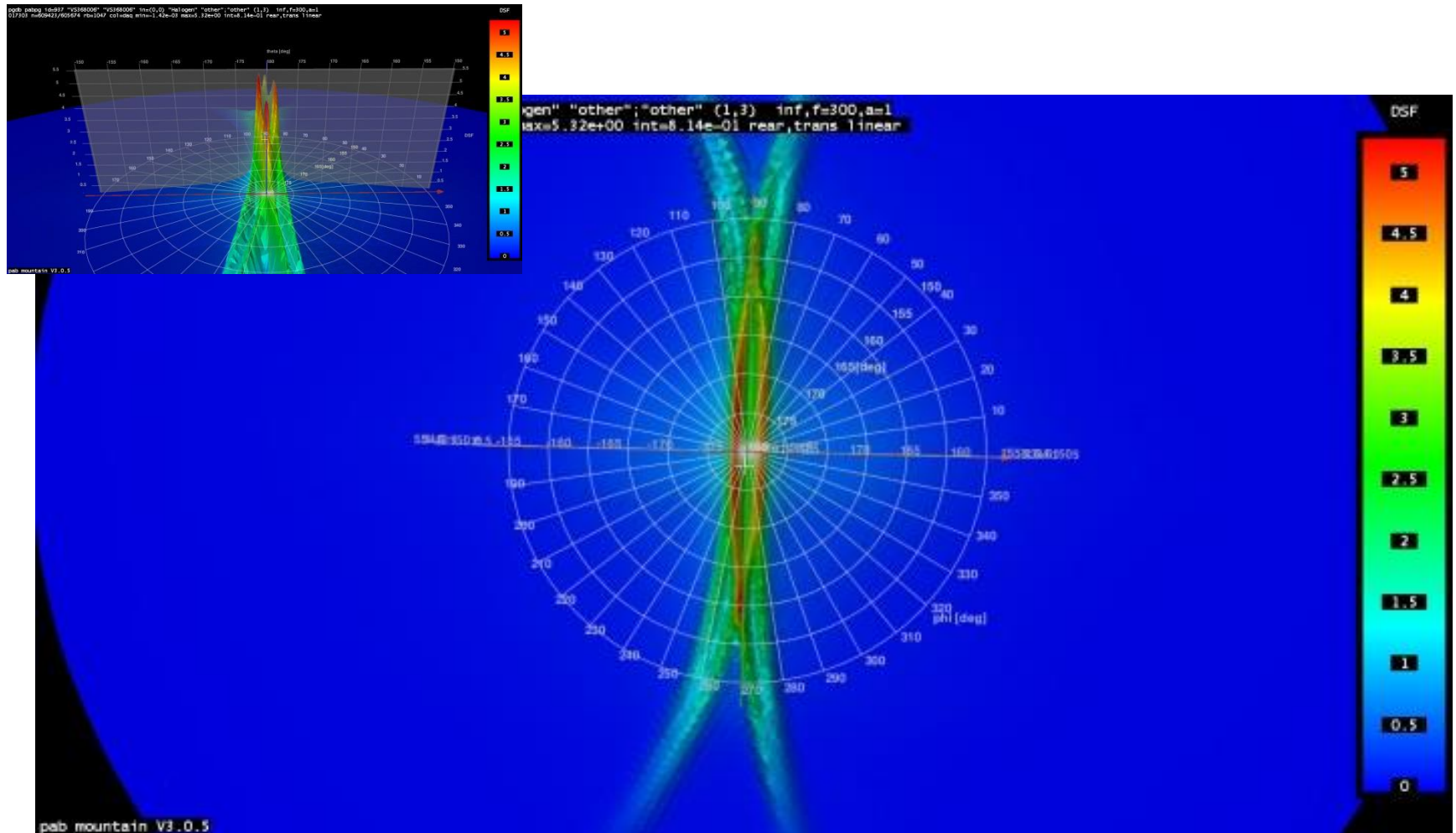




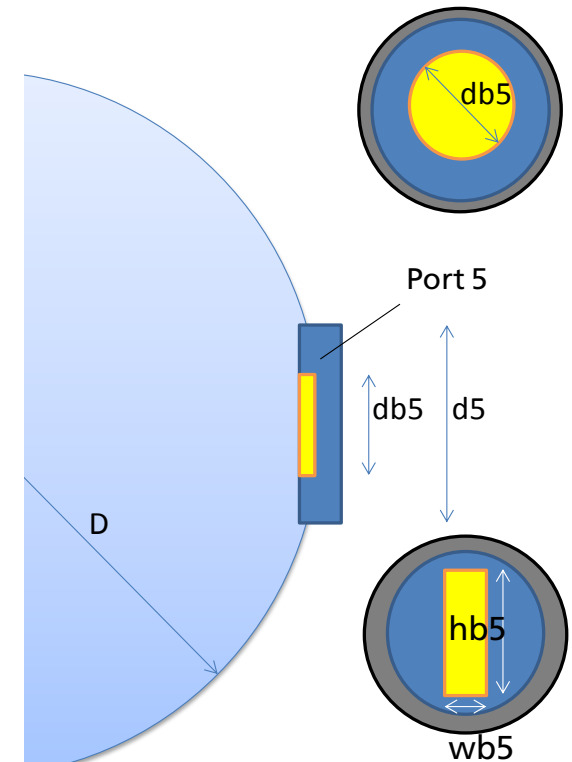
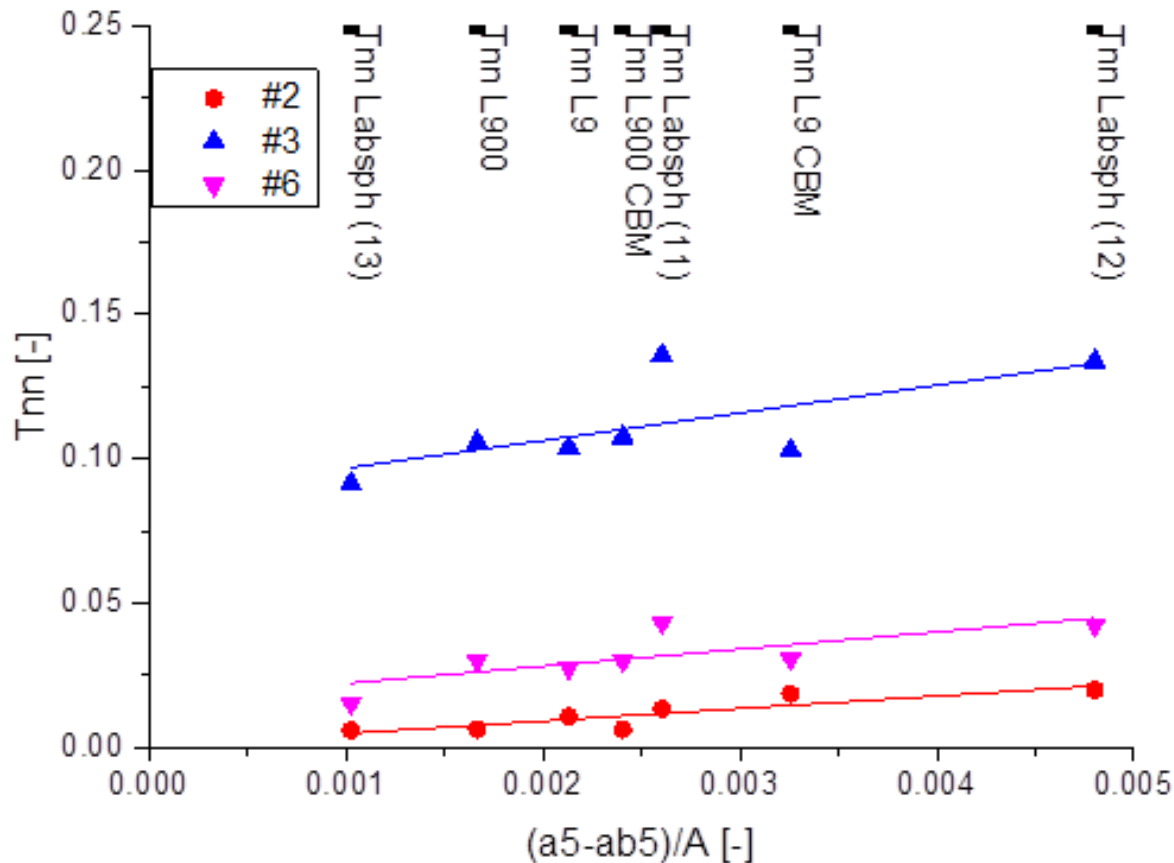
# $\tau_{n-n}$ : BDTF of "critical" sample #3



# $\tau_{n-n}$ : BDTF of "critical" sample #6



# $\tau_{n-n}$ : Effect of relative areas of port 5 and beam at port 5 Integrating sphere measurements for critical samples 2, 3, 6



# $\tau_{n-n}$ : Effect of relative areas of port 5 and beam at port 5

## $T_{nn}$ for all eight samples for three pairs of instruments with identical values of $a5/A$ but different values of $(a5 - ab5)/A$

