#### AVOIDANCE OF END CRATER IMPERFECTIONS AT HIGH-POWER LASER BEAM WELDING OF CLOSED CIRCUMFERENTIAL WELDS

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## **Motivation – Circumferential Welds**

#### **Pipeline construction**

Wind turbine towers





#### Hydraulic cylinder

#### Tank and apparatus construction









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# Challenges of circumferential laser beam welds

The problem with closing circumferential laser beam (LBW) or hybrid laser arc (HLAW) welds is the formation of end crater defects in a overlap area

Overlap area of a LBW pipe of grade X70 with a wall thickness of 8 mm



End crater hole and shrinkage cavity at abrupt switch-off of the laser beam power



Cracks in the overlap at laser power ramp

 End crater holes can be avoided with a laser power ramp, however cracks are formed in the material thickness





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## **Research project**

"Method for defect-free hybrid laser arc welding of closed circumferential welds"

#### Goals of the project

- Achieving a defect-free overlap of circumferential hybrid laser arc weld by adapting LB and GMA welding process parameters;
- Development of a method that can significantly expand the application field of laser hybrid technology

there are none yet universal solutions for defect-free execution of overlap areas closed circumferential I BW and HI AW welds in the thick sheet metal sector

0 2 mm

Pore in overlap area of a circumferential weld, HLAW of pipe segment with 9 mm thickness

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Results of the AiF project "Hybrid laser-GMA welding of thick-walled precision tubes" (BAM)

0 2 mm







×



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## Localisation of the imperfections



- Defects are distributed in the length of the overlap as well as over the material thickness
- Avoidance of the imperfections needs a complex strategy of heat transfer in the overlap





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# **Experimental Setup**

- High-power Yb:YAG disk laser TruDisk 16002
- Laser processing head BIMO with a MZ-collimator
  - Adjustment range of the focal position in Z-direction: -10 mm / +30 mm (optional +80 mm)
  - Magnification M: 2.5 6
  - Focus diameter at 200 µm optical fiber: 500 µm - 1200 µm
- Materials used for this study:
  - Flat specimens of S355J2 with a thickness of 10 mm
  - Pipes of X100Q (WT of 9.5 mm, outer diameter of 5 inches)







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# **Beam profile measurements – Variation of Z**

 Beam profile measurements were taken with an Ophir Spiricon BeamWatch noncontact laser measurement device at 2 kW laser power



 $\textbf{Z=0}~\textbf{mm};~\textbf{M}=2.8;~ \varnothing_{fz0}=560~\mu\text{m}$ 





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**Z = 30 mm**; M = 2.8; Ø<sub>fz30</sub> = 2100 μm



## Beam profile measurements – Variation of M



Z = fixed; **M = 2.8**;  $\emptyset_{fz0}$  = 560 µm





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Z = 30 mm; **M = 5.8**;  $\emptyset_{fz30}$  = 1160  $\mu$ m



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## **Results – Zone I (root defects)**



- higher defocusing >40 mm with a shorter outfeed length is preferable
  - → smooth transition from full penetration to partial penetration with root quality according to EN ISO 12932 valuation class B

 $P_L = 10 \text{ kW}, v_w = 1.0 \text{ m min}^{-1}, t = 10 \text{ mm}$ 





outfeed length = 30 mm





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#### Solidification cracking

Characteristics

- Occur at temperatures higher than the solidus in the late stages of solidification
- Involves the separation of grains or dendrites

Possible mechanical causes (stresses)

- Interdendritic pressure drop (forms a cavity) and aditional tensile stresses
- Tensile stresses exceed the fracture stress of liquid film
- The partial penetrated LBW or HLAW welds are primarily prone to center line solidification cracking than fully penetrated welds



Centreline solidification crack by laser beam welding

 $V = 2 \text{ m min}^{-1}$  $P_{i} = 10 \text{ kW}$  $Z_{f} = -3 \text{ mm}$ Material S355

Centerline crack in a hybrid laser arc weld



Gebhardt, 2013





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Variation of the magnification M 2.8 – M 5.8



 $P_{L} = 10 \text{ kW}, v_{w} = 1.0 \text{ m min}^{-1}, t = 10 \text{ mm}$ 





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Variation of the focal position in Z-direction 



defocusing

40 mm (fØ = 2.9 mm)60 mm (fØ = 4.3 mm)80 mm (fØ = 5.6 mm)

Highest impact on the weld shape formation was found with a high defocusing



40 mm





80 mm

- Smooth transition could be reached at a defocusing over 80 mm
- Shrinkage cavity on the top surface

 $P_{L} = 10 \text{ kW}, v_{w} = 1.0 \text{ m min}^{-1}, t = 10 \text{ mm}$ 





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Variation of the **outfeed length** 



 $P_1 = 10 \text{ kW}, v_w = 1.0 \text{ m min}^{-1}, t = 10 \text{ mm},$ defocusing 80 mm, M 2.8



- Increase of crack length with increasing outfeed length
- Increase of drop size with increasing outfeed length
- Cracks are formed in the partial penetrated part of the LBW
- Outfeed length of 10 mm to 15 mm lead to best results





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## **Results – Zone III (defects on the top surface)**

Transfer of results to circumferential welds

End crater shrinkage cavity on the top surface could be avoided with smoothing weld using 2 kW laser beam power and an defocussed laser beam with a focus of 4.3 mm on the top surface at a welding speed of 0.5 m min<sup>-1</sup>

 $P_1 = 11.5 \text{ kW},$  $v_{w} = 1.0 \text{ m min}^{-1}$ , t = 9.5 mm, defocusing z 80 mm, M 2.8, outfeed length 15 mm







und -prüfung



#### Conclusions

- Formation of the end crater imperfections at LBW of closed circumferential welds could be effectively minimized by the adjustment of the process parameters such as defocusing of the laser beam;
- Defocusing of >40 mm is recommended with regard to minimizing of root drop size at the end of the weld seam;
- Increase of the crack length with increasing overlap length → short outfeed length of 10 mm to 15 mm is recommended;
- Cracks and pores in the mid-thickness could be eliminated at a defocusing of the laser beam 80 mm → shrinkage cavity shifts to the weld top surface
- Shrinkage cavity on the weld top surface could be avoided with a smoothing weld using a low power of 2 kW at a spot diameter of 4.3 mm
- Transfer of the results to 9.5 mm thick pipe segments X100Q could be realized successful





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