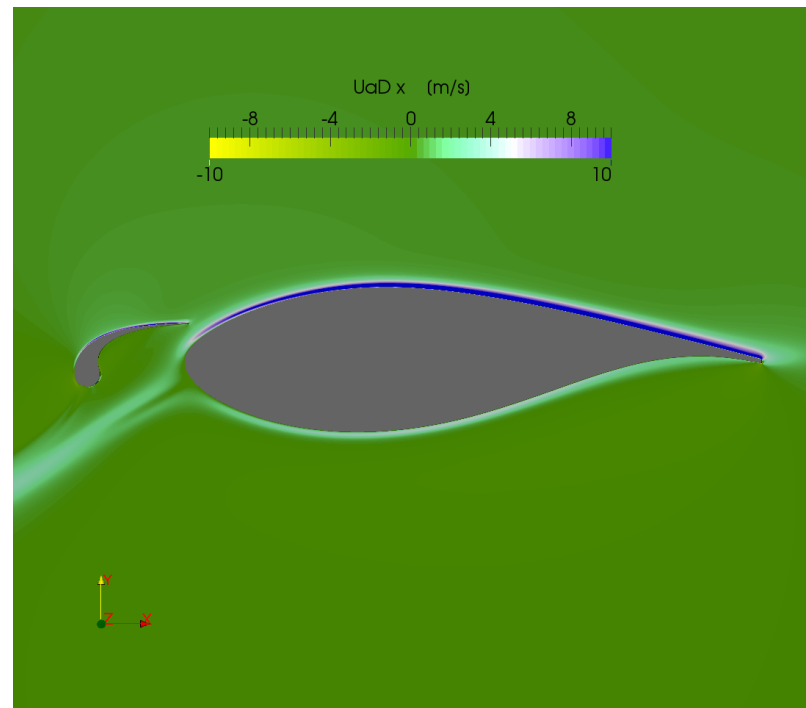


Optimization of Aerodynamic Shapes

Matthias Schramm^{1,2}, Lena Vorspel², Bernhard Stoevesandt¹, Joachim Peinke^{1,2}

¹Fraunhofer IWES, ²ForWind

SmartBlades Conference | 3. – 4. February 2016 | Stade

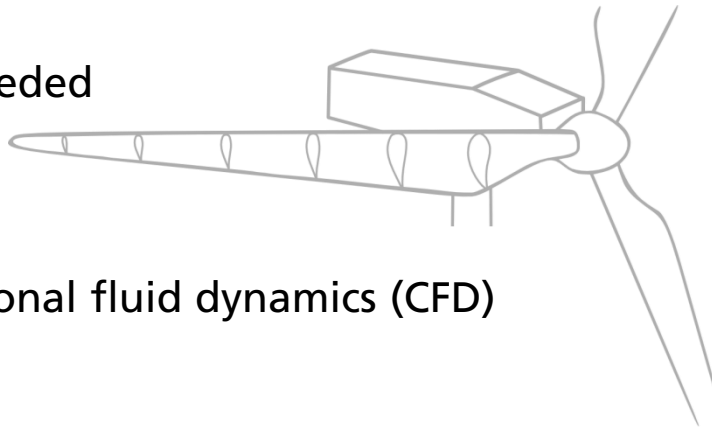


Agenda



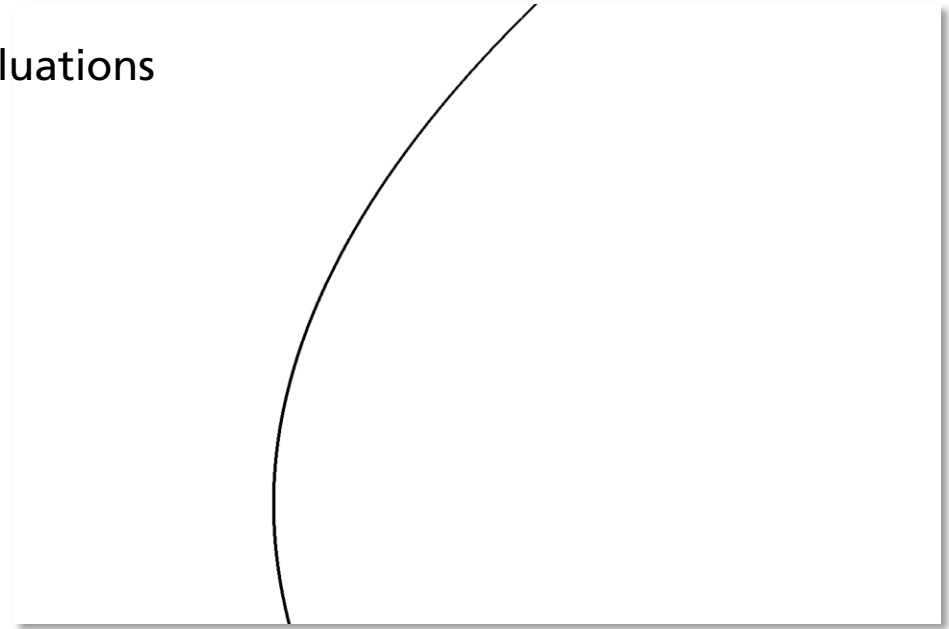
- Motivation
- Adjoint approach
- Verification of the gradients
- Optimization of thick airfoil
- Validation and optimization of leading edge slat
- Conclusions & Outlook

Motivation

- Rotor blades are complex geometries → no intuitive design possible
 - Optimization is necessary
 - Blades consists of airfoils → airfoil optimization needed
- 
- High accuracy for prediction of loads → computational fluid dynamics (CFD)
 - CFD + conventional optimization → expensive
 - adjoint approach

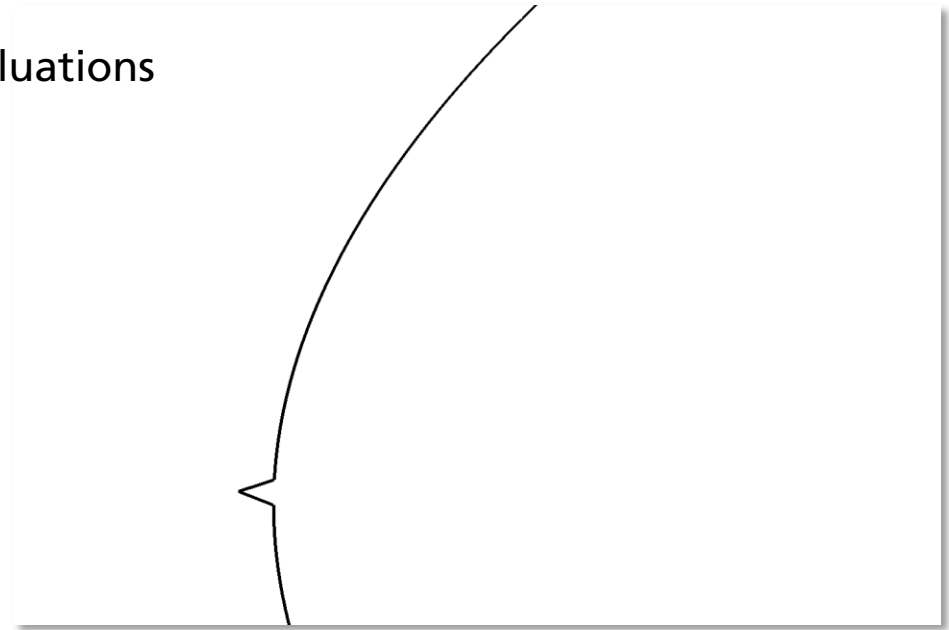
Gradient-Based Optimization: Traditional Approach

- Optimization using gradients
- Traditionally by finite differences
- More design parameters → more evaluations
- Every time full CFD necessary
- Computationally expensive



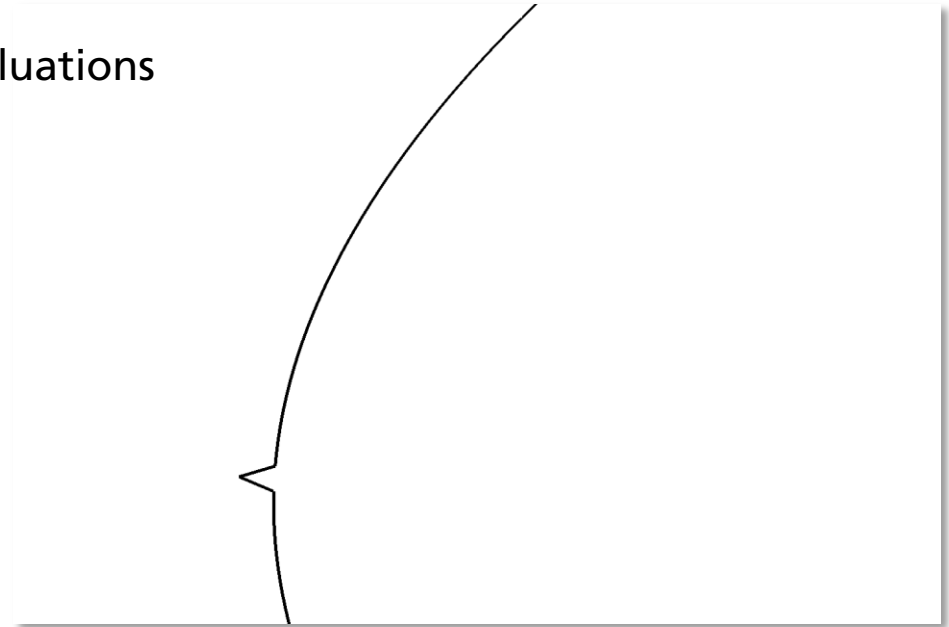
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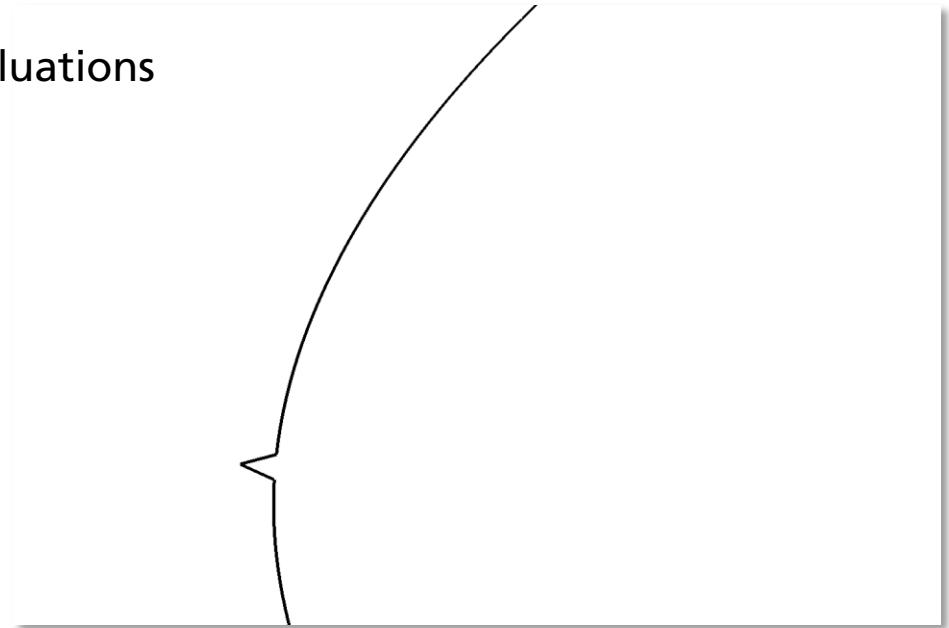
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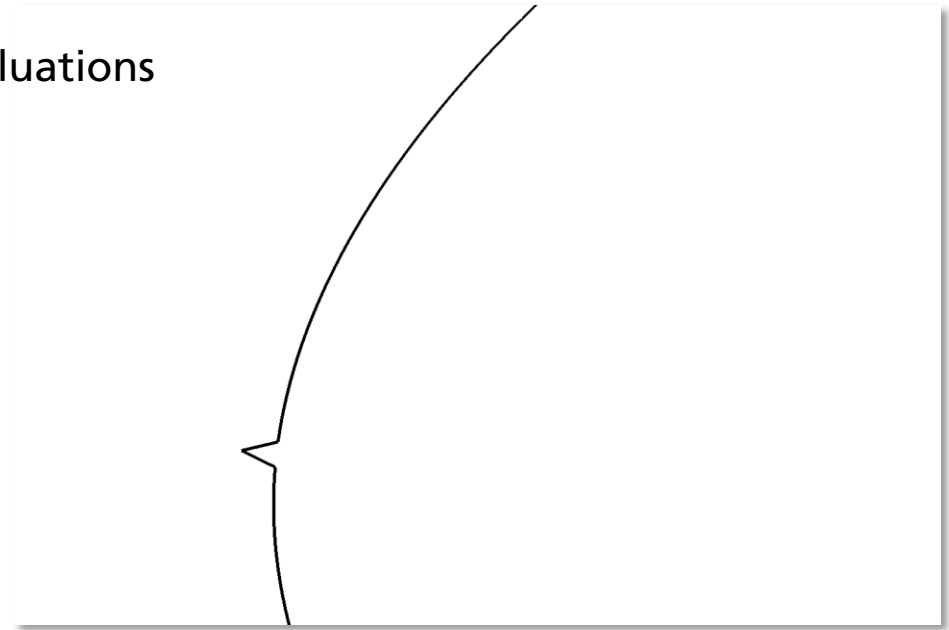
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Gradient-Based Optimization: Adjoint Approach

- Solving a **few more equations**

$$\text{Min. } I(\mathbf{u}, p, \beta) \quad \text{w.r.t. } \mathbf{R}(\mathbf{u}, p, \beta) = 0$$

$$L := I + \int_{\Omega} (\Psi^u, \Psi^p) \cdot \mathbf{R}$$

$$\delta L = \left(\frac{\partial I}{\partial \beta} + \int_{\Omega} (\Psi^u, \Psi^p) \cdot \frac{\partial \mathbf{R}}{\partial \beta} \right) \delta \beta$$

$$\left[+ \left(\frac{\partial I}{\partial \mathbf{u}} + \int_{\Omega} (\Psi^u, \Psi^p) \cdot \frac{\partial \mathbf{R}}{\partial \mathbf{u}} \right) \delta \mathbf{u} + \left(\frac{\partial I}{\partial p} + \int_{\Omega} (\Psi^u, \Psi^p) \cdot \frac{\partial \mathbf{R}}{\partial p} \right) \delta p \right] = 0$$

Adjoints in CFD

Gradient-Based Optimization: Adjoint Approach

- Solving a **few more equations** and **each single point** can be design parameter

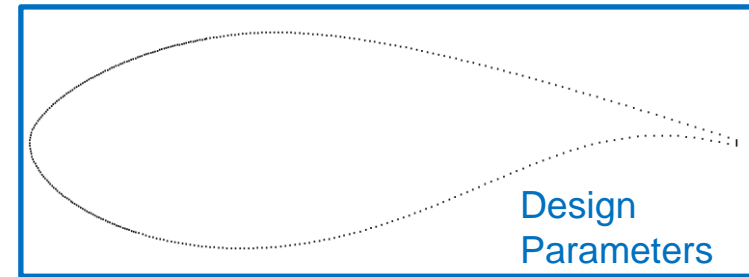
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Gradient-Based Optimization: Adjoint Approach

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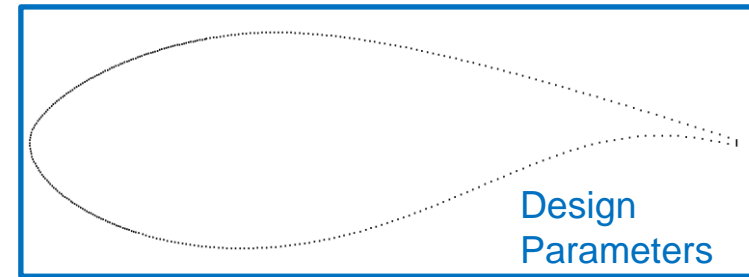
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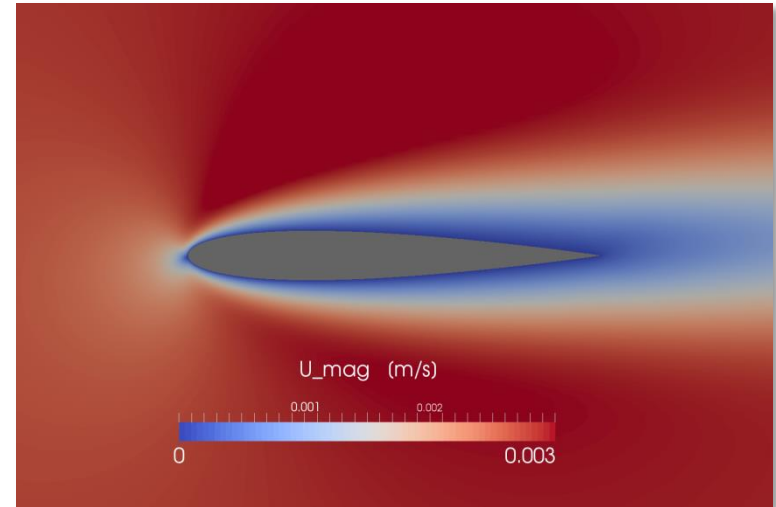
Adjoint in CFD



- Computation of gradient independent from number of design parameters
- Only two solver runs for each gradient necessary
- Arbitrary amount design parameters possible

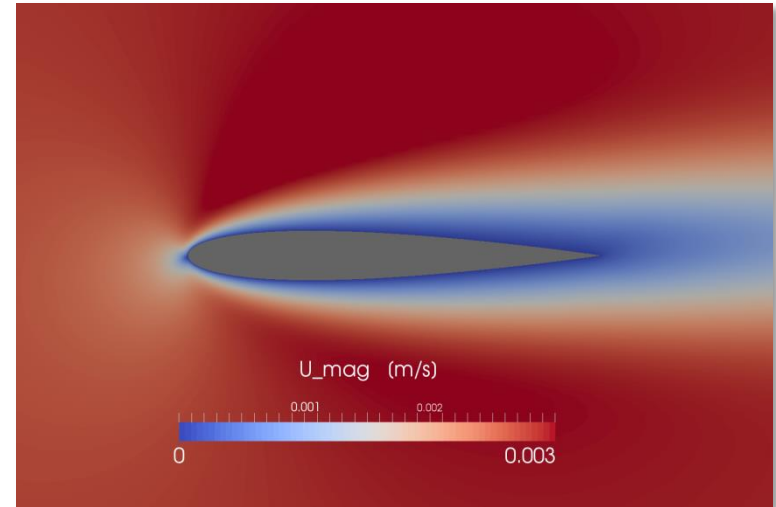
Setup of Verification Case

- NACA 0012
- $Re = 2,000$
- $AoA = 3^\circ$
- Laminar flow, $y^+ < 1$
- Approx. 55,000 cells, 350 faces on airfoil
- OpenFOAM-2.3.0



Setup of Verification Case

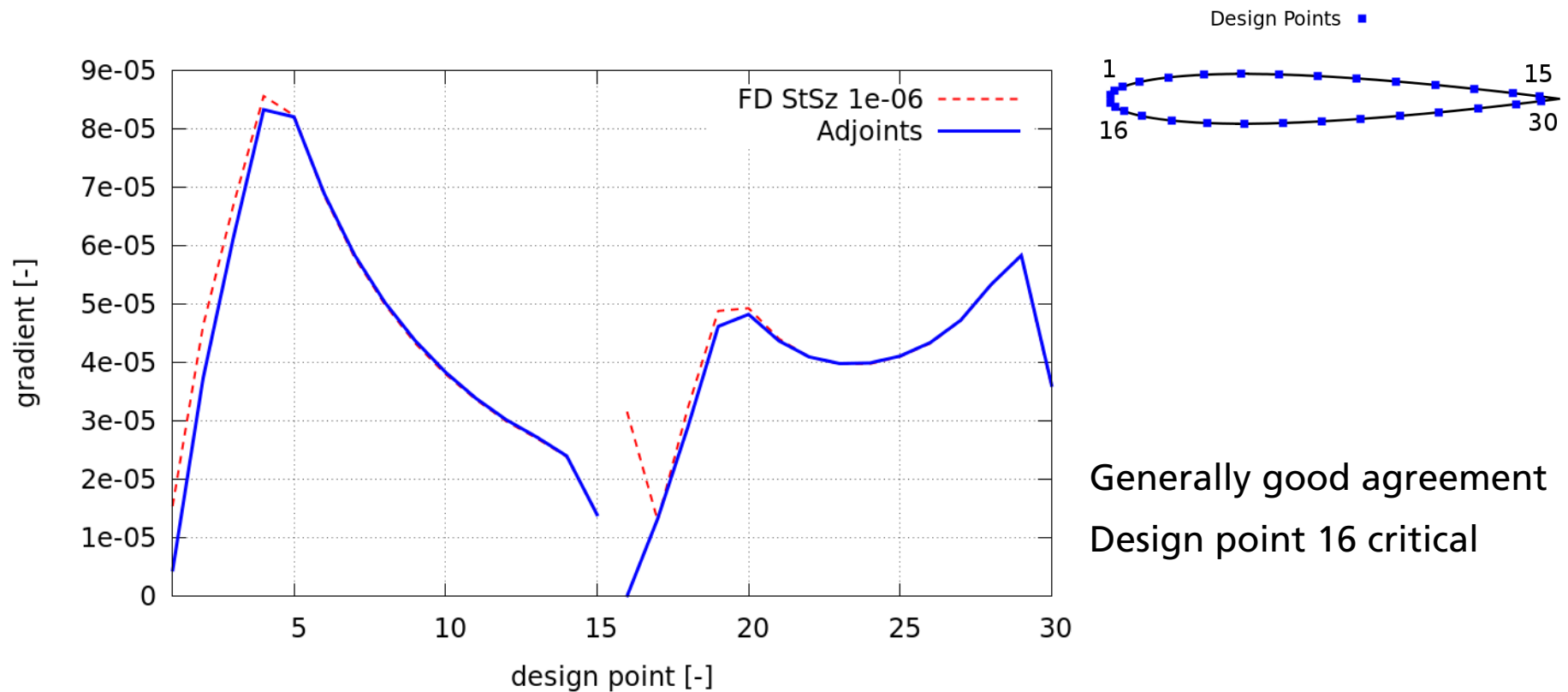
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-
- Gradients from the adjoint approach compared with gradients obtained by finite differences FD (forward, 1st order)
 - Finite differences:
 - Fine mesh \rightarrow small mesh movement \rightarrow small force changes \rightarrow high convergence
 - \rightarrow **expensive computation**



Verification of Gradients

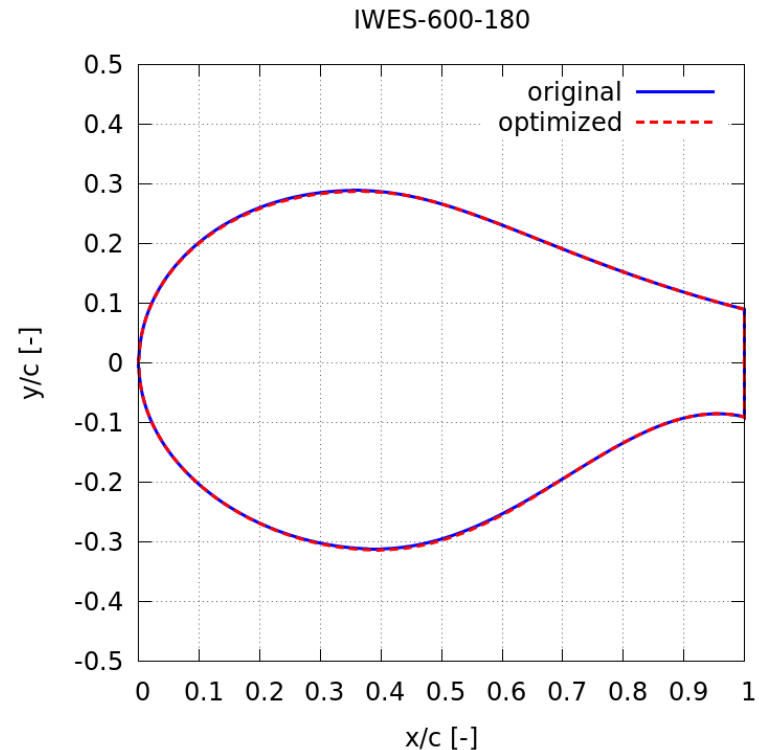


- Evaluation at selected design points only (→ expensive FD)

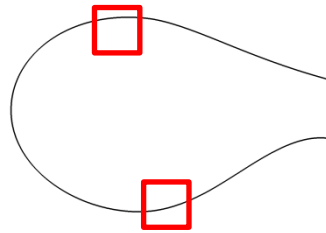


Drag Reduction of IWES 600-180

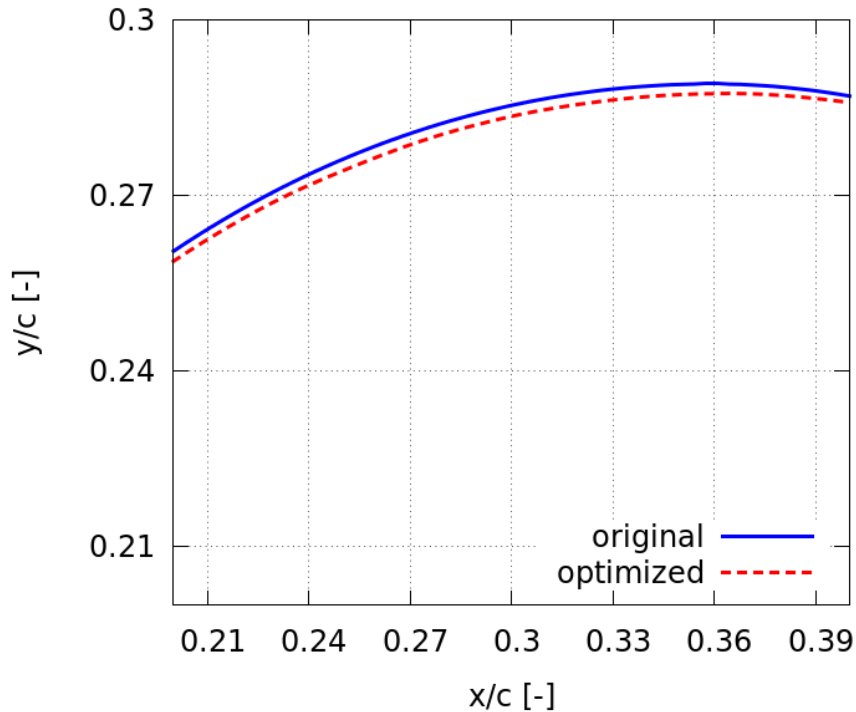
- IWES 600-180
- $Re = 3 \cdot 10^6$, $AoA = 12^\circ$
- Objective: $\min I = \frac{1}{2} \cdot (c_d - 0.15)^2$ w.r.t. $c_l \geq c_{l,0}$
- Spalart-Allmaras turbulence model
- Optimization including adjoints to turbulence model
- Drag reduction $> 3\%$



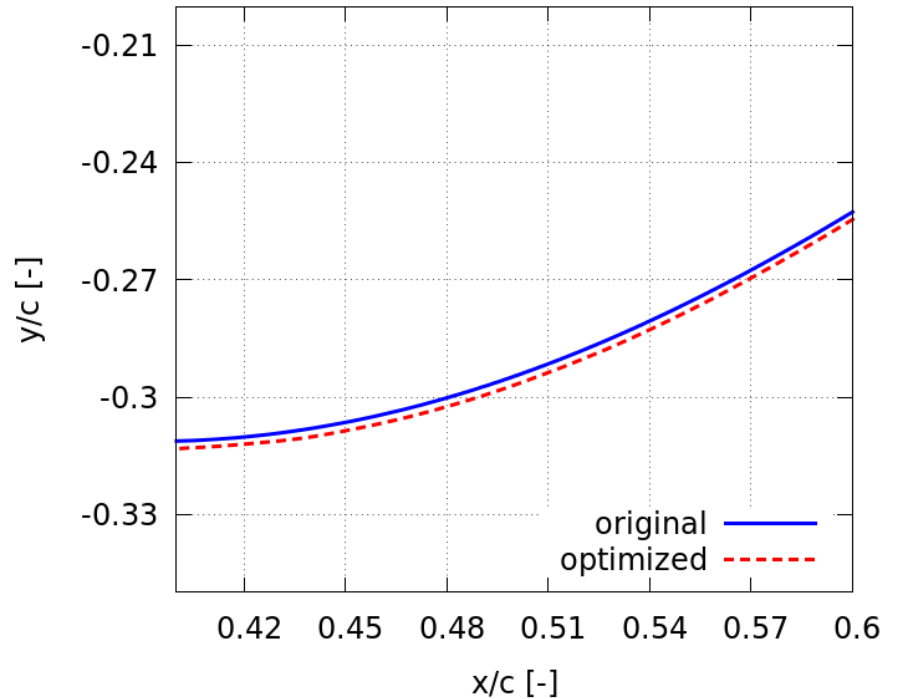
Detail View of Shapes



IWES-600-180



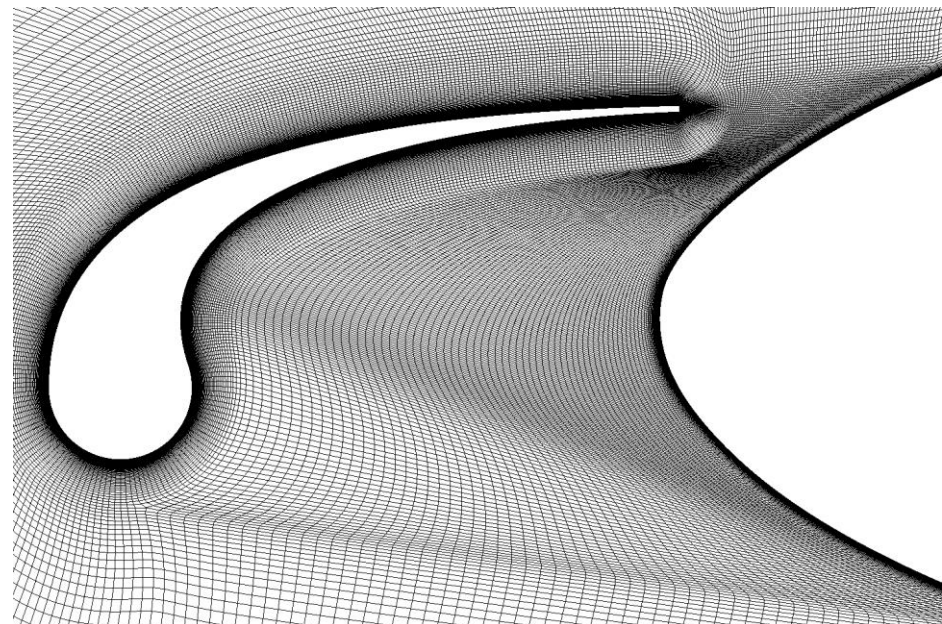
IWES-600-180



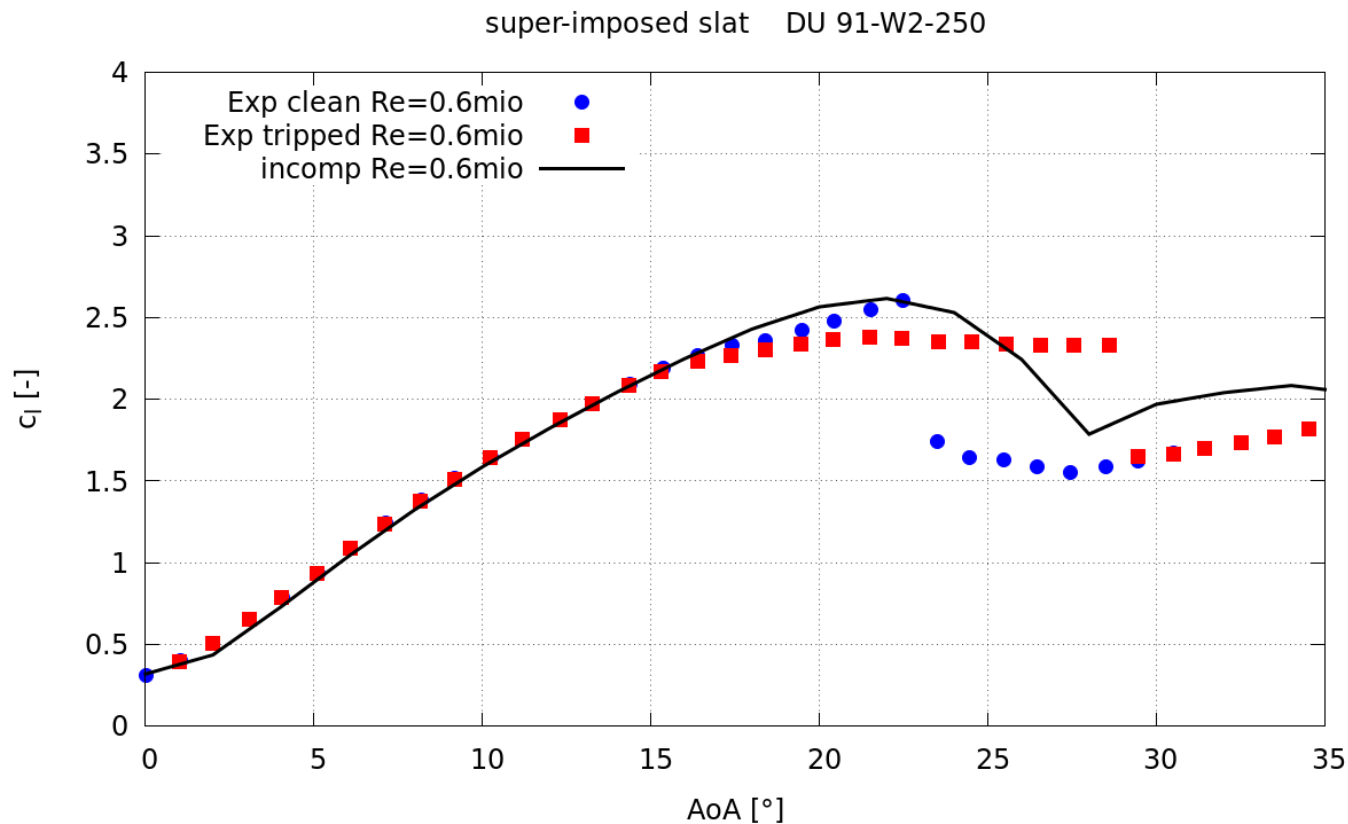
- Pure numerical problem, no wind tunnel data existing
- Shape moves downwards

Setup for Leading Edge Slat

- Comparison with experimental data from wind tunnel in Oldenburg
- $Re=0.6 \cdot 10^6$, incompressible solver
- $Re=7.89 \cdot 10^6$, incompressible and compressible solver ($Ma>0.3$)
- Spalart-Allmaras turbulence model, $y^+<1$
- 480 faces on slat, 700 faces on airfoil, 160,000 cells in total
- Block-structured O-mesh
- Radius $25 \cdot \text{chord}$

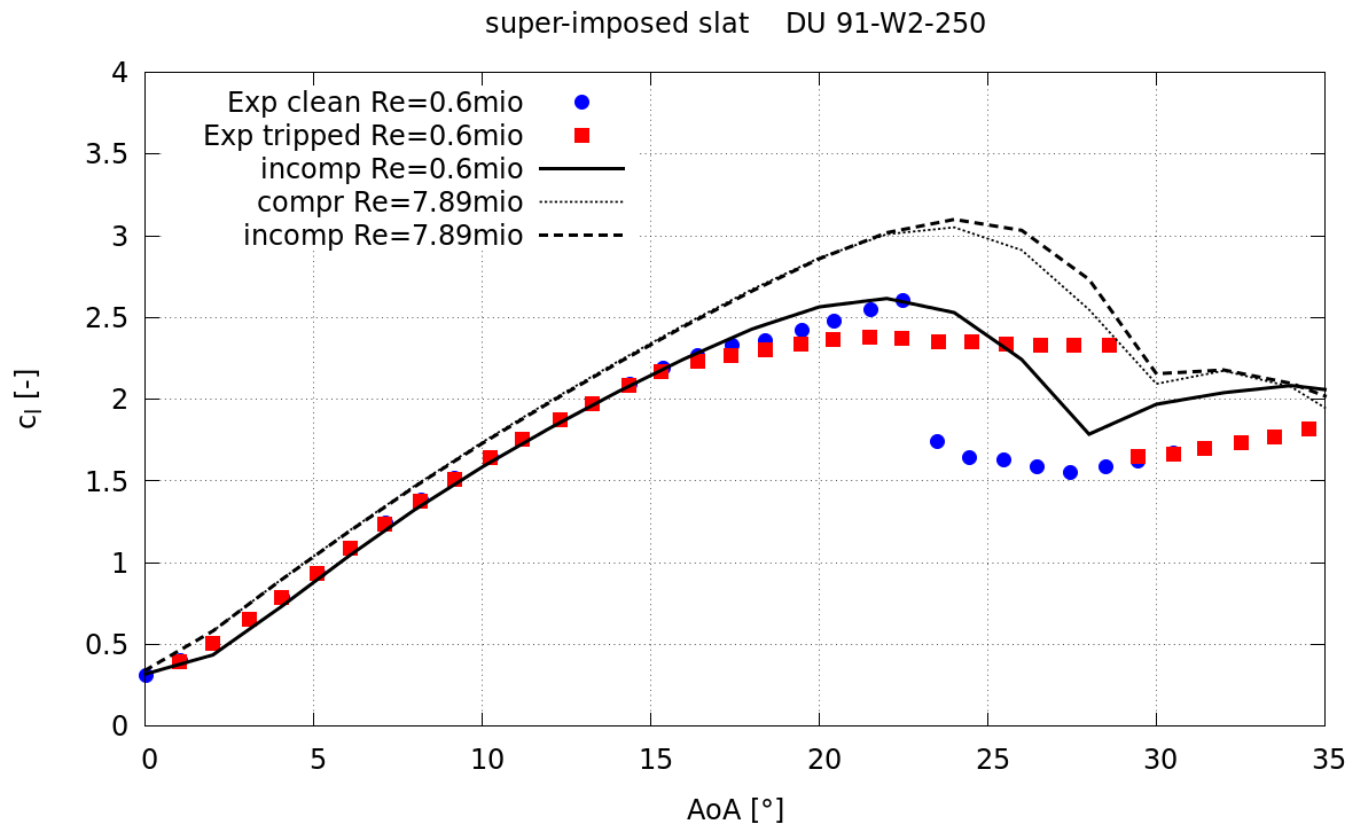


Validation for Leading Edge Slat



- Differences in stall

Validation for Leading Edge Slat

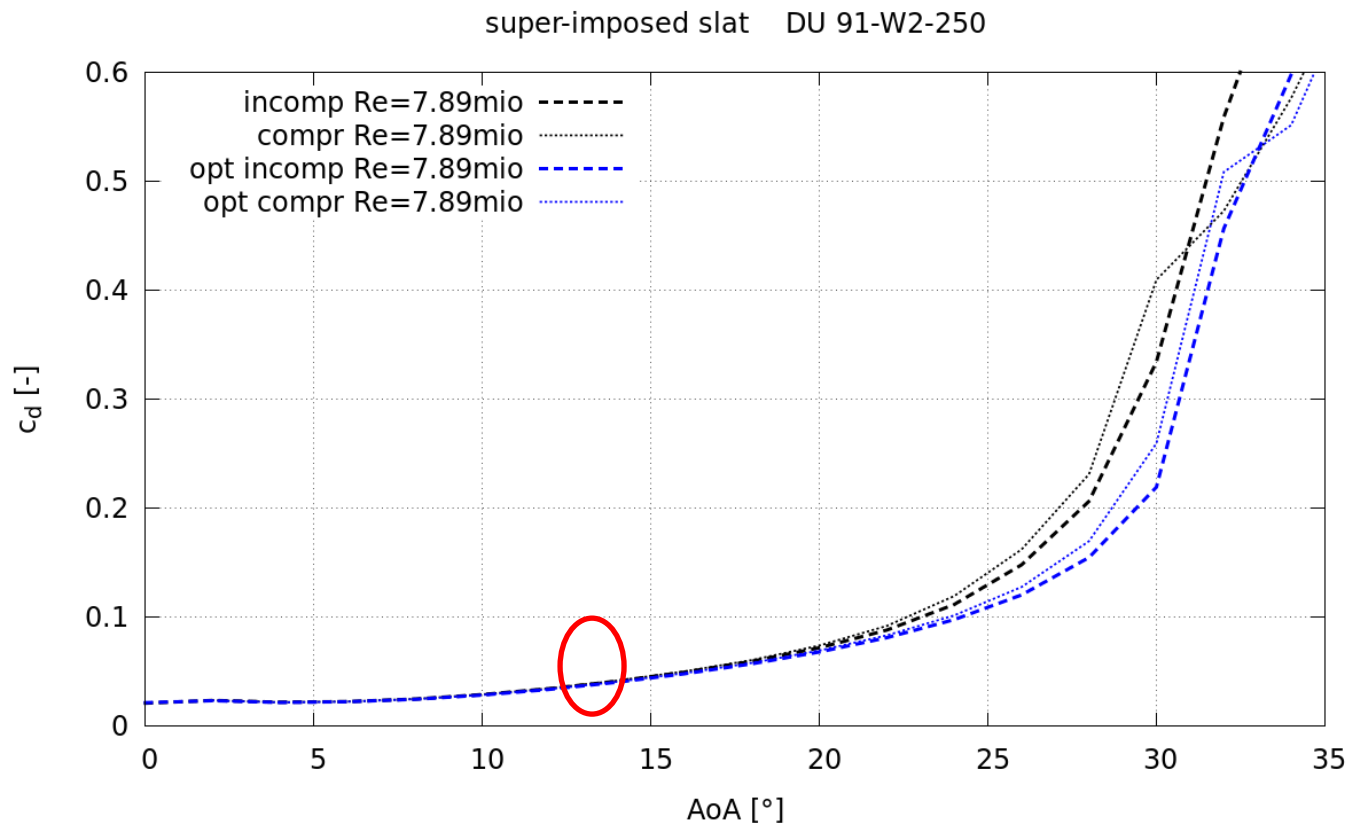


- Similarities in linear range
- Differences between compressible and incompressible solvers

Optimization of Leading Edge Slat

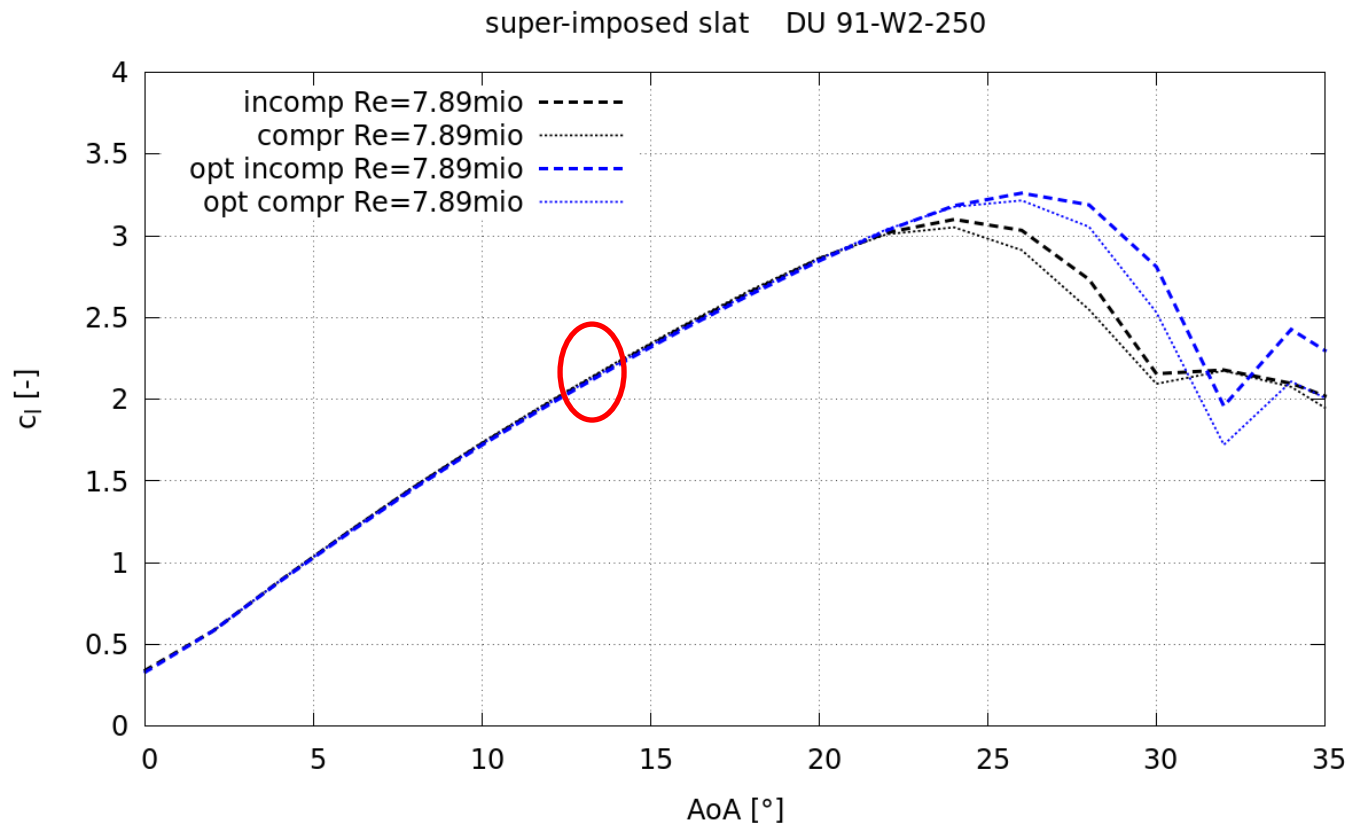
- $Re=0.6 \cdot 10^6$, $AoA=13^\circ$
- Objective: $\min l=c_d$ w.r.t. $c_l \geq c_{l,0}$
- Optimization at low $Re=0.6 \cdot 10^6$, incompressible solver
 - (optimization framework more stable at low Re)
- Check design at high $Re=7.89 \cdot 10^6$, compressible solver
 - (final slat on 80m blade)
- Drag reduction $> 2\%$ at $AoA=13^\circ$

Optimization of Leading Edge Slat



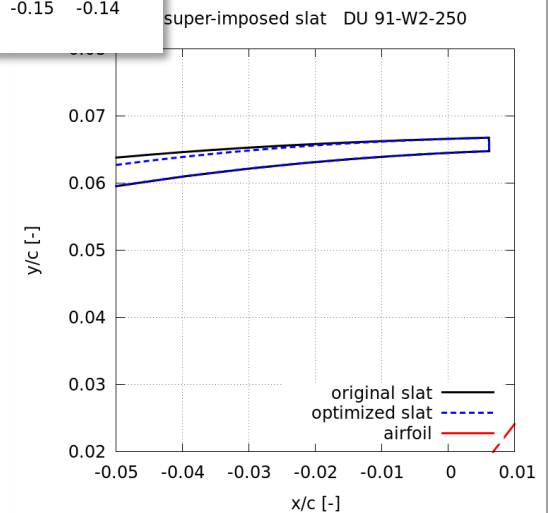
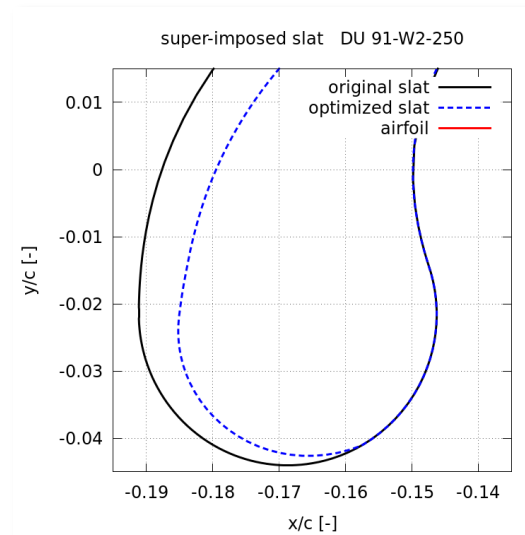
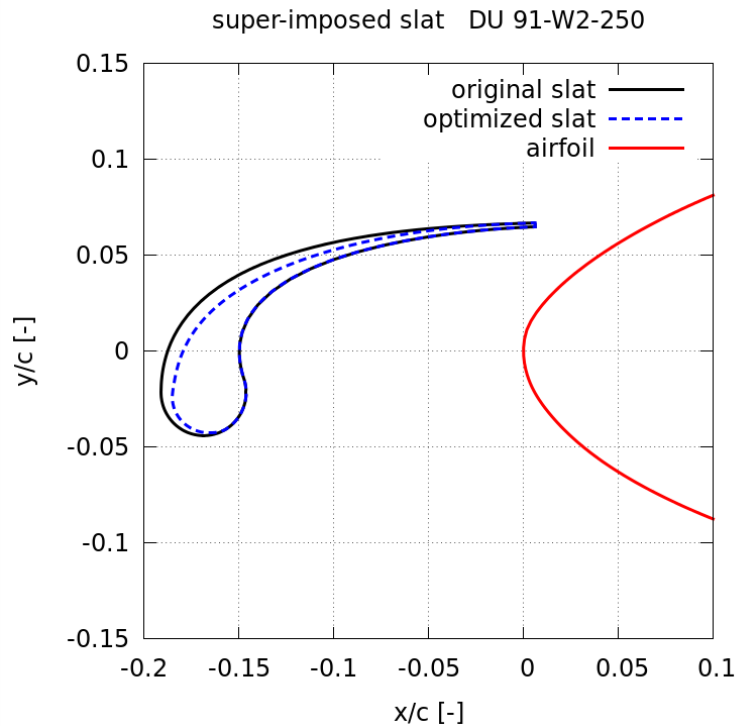
- Lower drag at higher angles of attack
- Drag reduction > 2% at AoA=13°

Optimization of Leading Edge Slat



- Higher maximum lift
- Max. lift at higher angle of attack

Detail View of Shapes



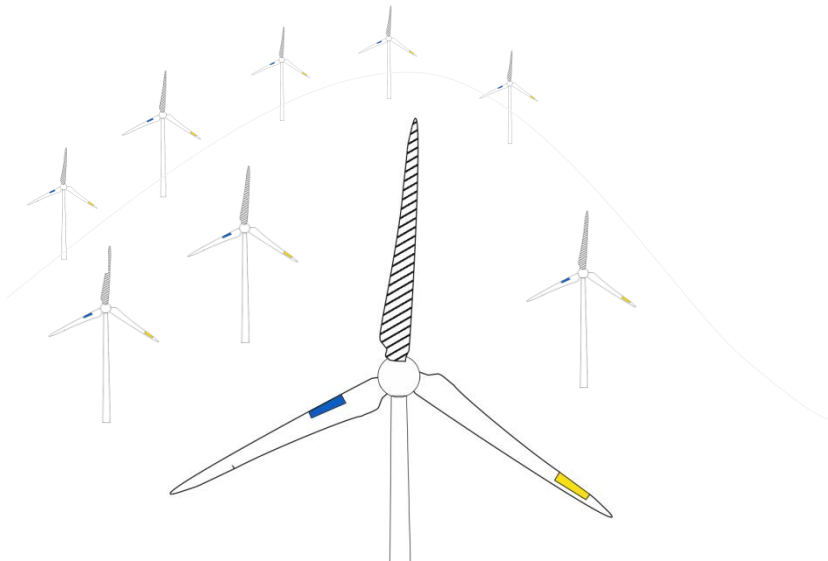
- Thinner shape, same position
- Increase in c_l^3/c_d^2 of approx. 3% at $AoA=13^\circ$

Conclusions & Outlook

- Implementation of adjoints for shape optimization in OpenFOAM
- Verification of gradients
- Numerical optimization of thick airfoil
- Validation and optimization of leading edge slat
- Extension of framework for the use of constraints

Thank you for attention!

matthias.schramm@iwes.fraunhofer.de



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