



Tailored melt pool shape and temperature distribution by a dual laser beam LMD-w process

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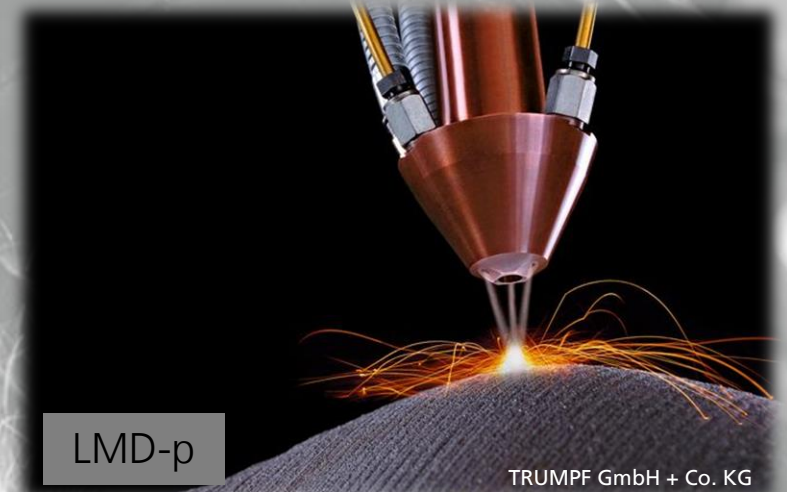
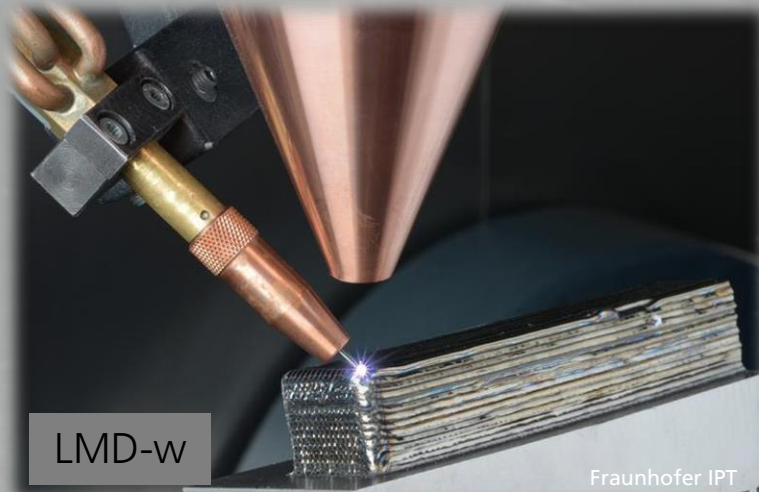
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Motivation



Applications

- Additive Manufacturing of parts and features
- Coating
- Repair
- Application markets: mobility, energy, mechanical engineering, tools

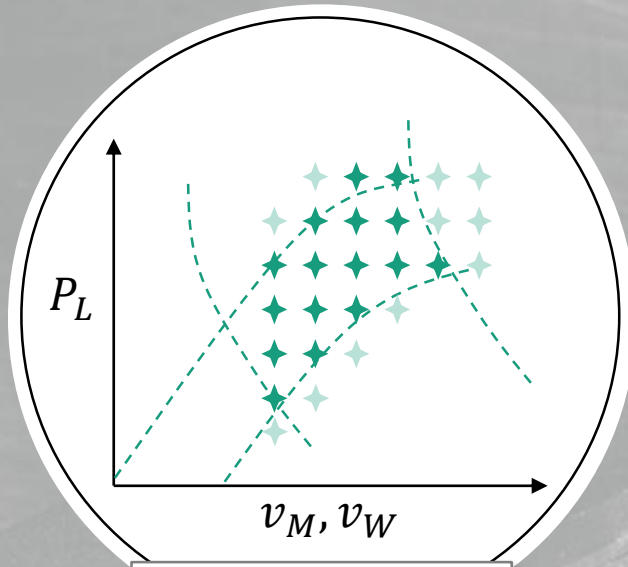
Wire-based Laser Metal Deposition (LMD-w)

- Small heat input
- High material efficiency
- Easy handling of filler material
- Small risks for health
- Low contamination of machines and production environment

[BEYE95, SYED05, KAIE12, BAMB18, NGO18]

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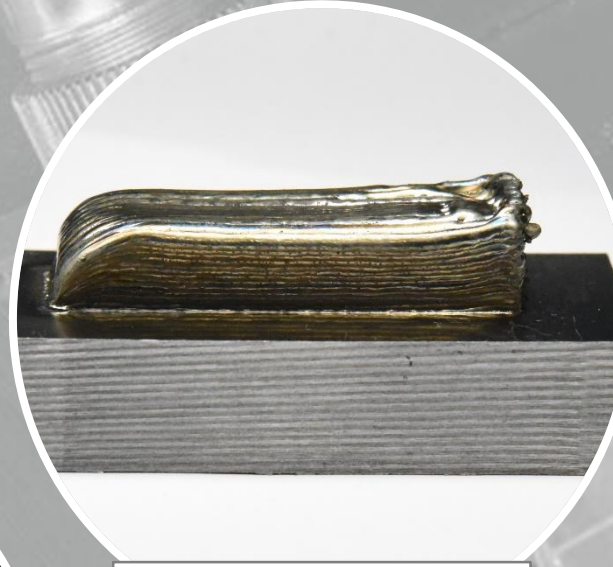
LMD-w with lateral wire feed – challenges



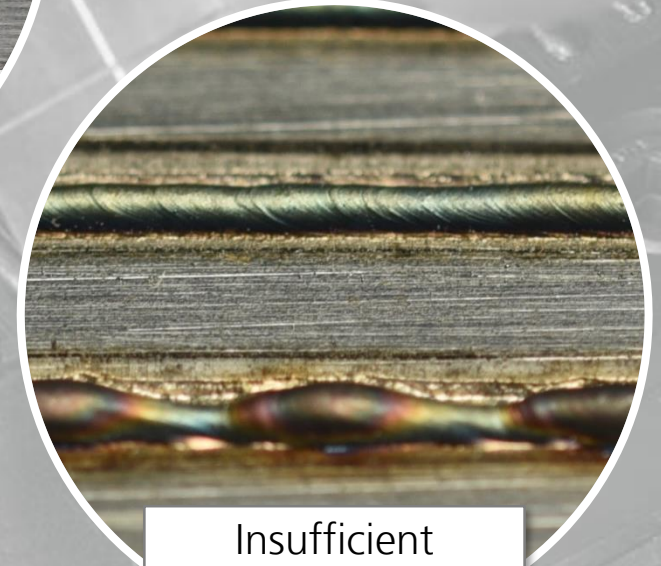
Small process window



Process instability



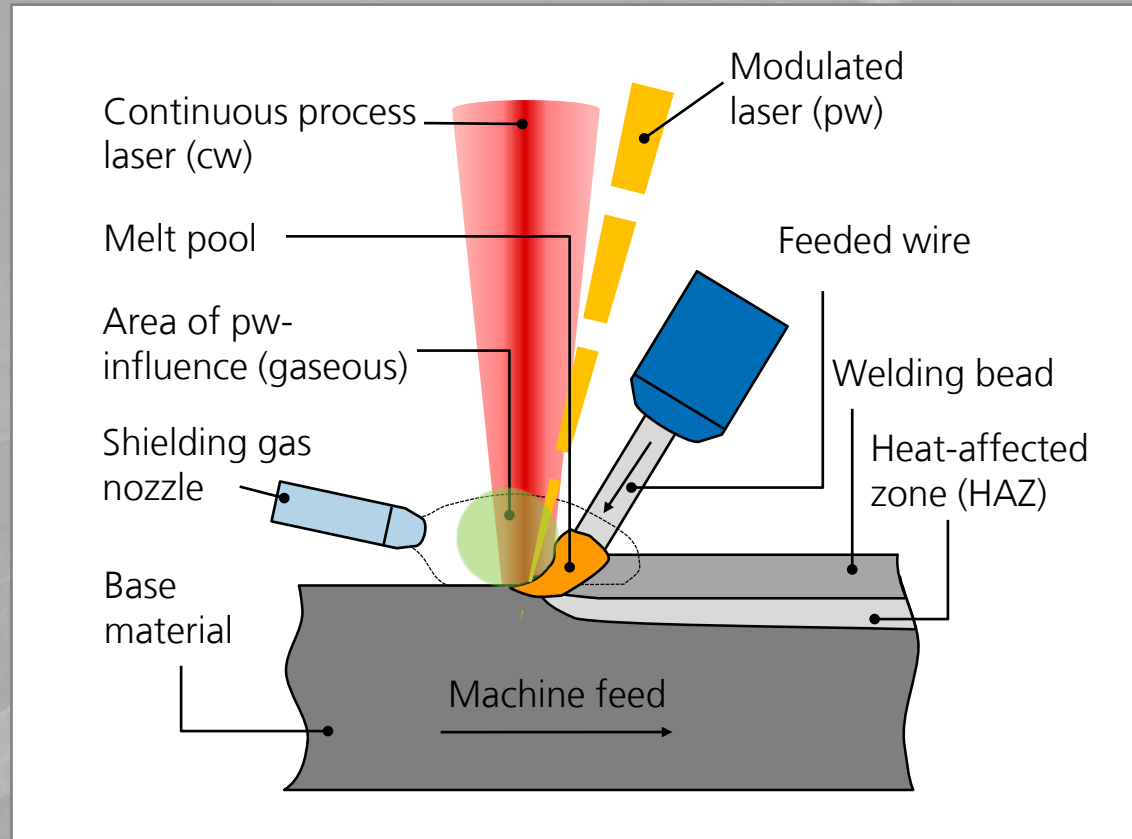
Insufficient surface quality



Insufficient reproducibility

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Dual beam process – principle and potential



cw = continuous wave, pw = pulsed wave

Effects

Modification of absorption behavior

Influence on welding bead geometry

Enlargement of stable process window



Potential

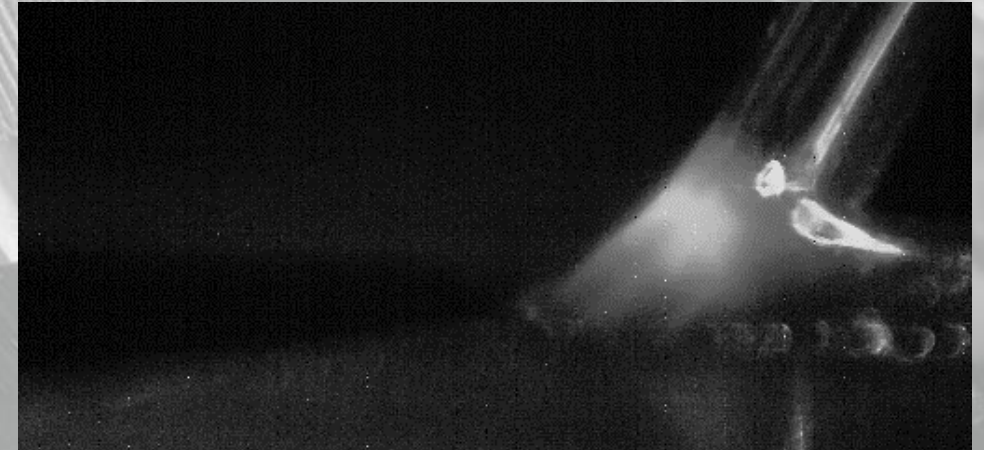
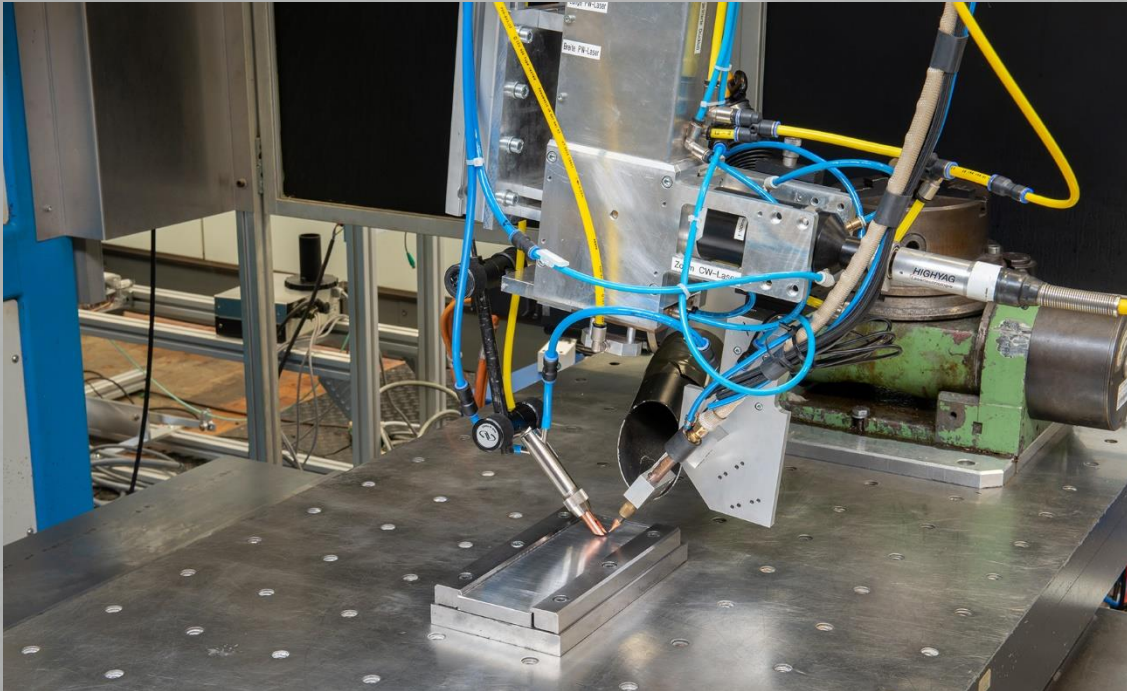
Specific temperature adjustment

Reduction of surface waviness and roughness

Process stabilization

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Dual beam process – principle and potential



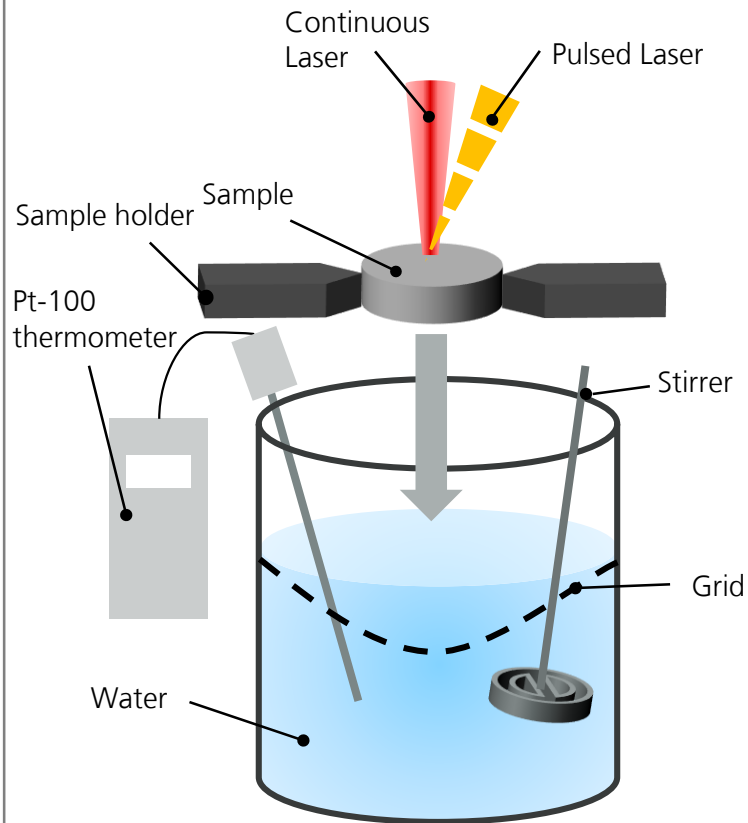
Used laser sources:

- Modulated beam: Edgewave IS20I-ET
- Continuous beam: Laserline LDF 5000-40

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Modulated laser influence on absorption (I/II)

Calorimeter-like test stand

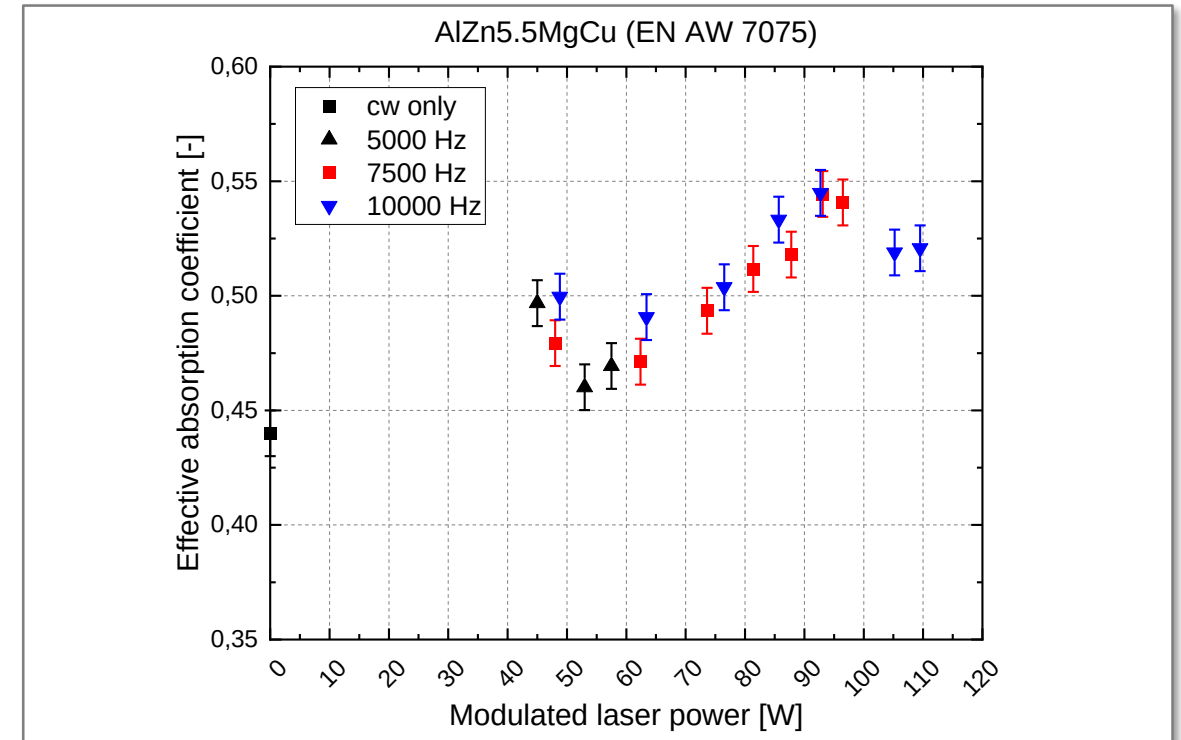
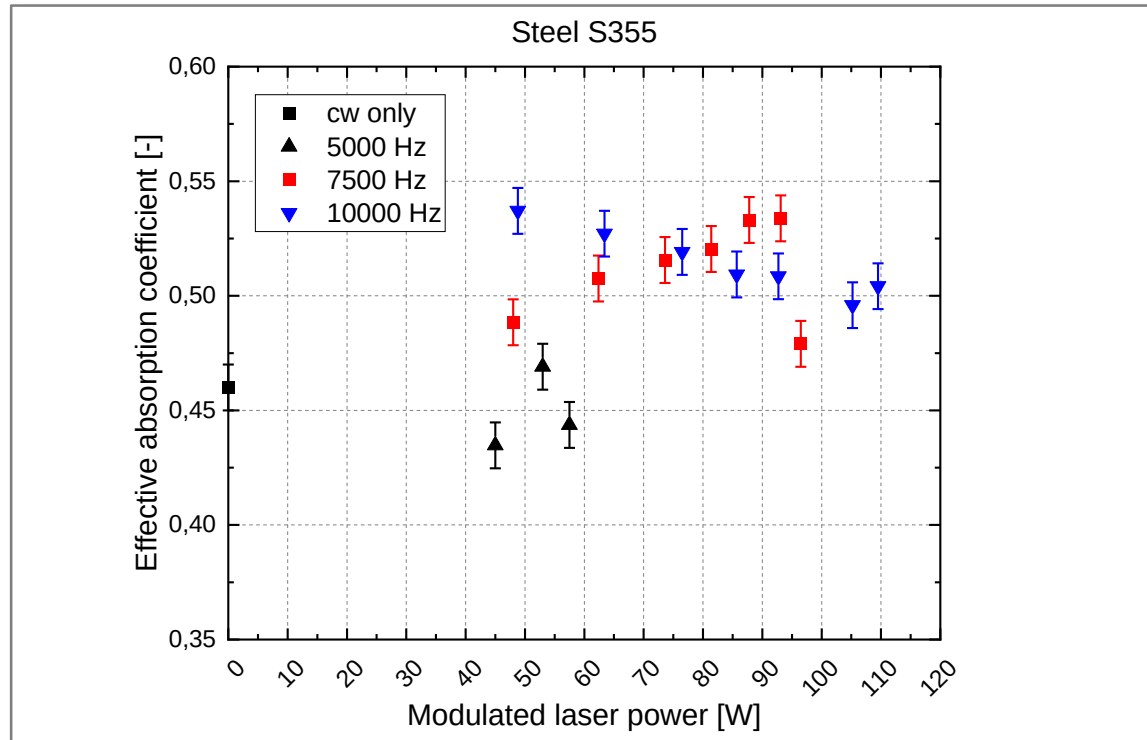


- Laser processing of the samples during 40 s (cw constant: 400 W, pw varied)
- Dropping the sample into an isolated water vessel
- Measuring the water's temperature raise until stagnation
- Determination of the absorbed energy
- Calculation of the effective absorption coefficient (cumulated pw+cw power)

Dependency of absorption on the modulated laser radiation

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Modulated laser influence on absorption (II/II)

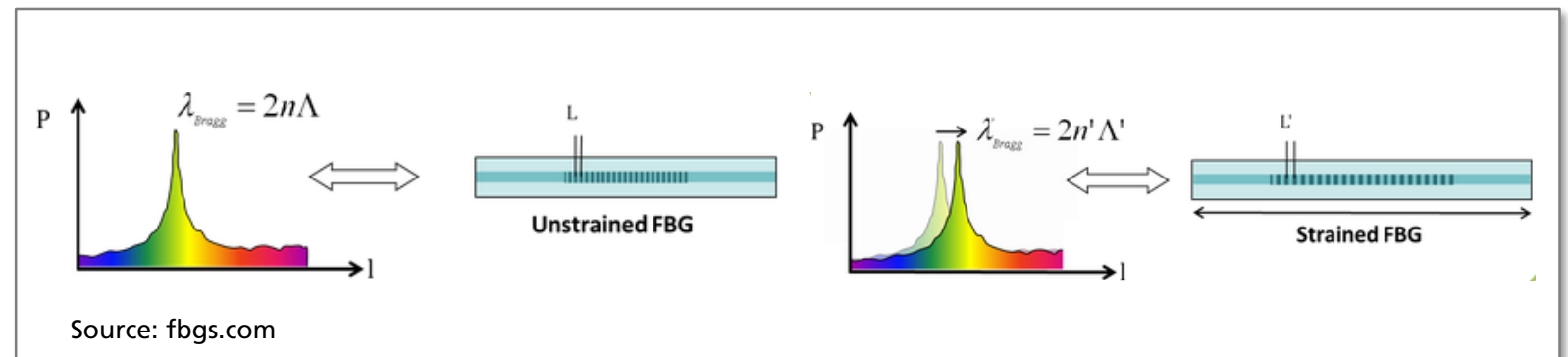
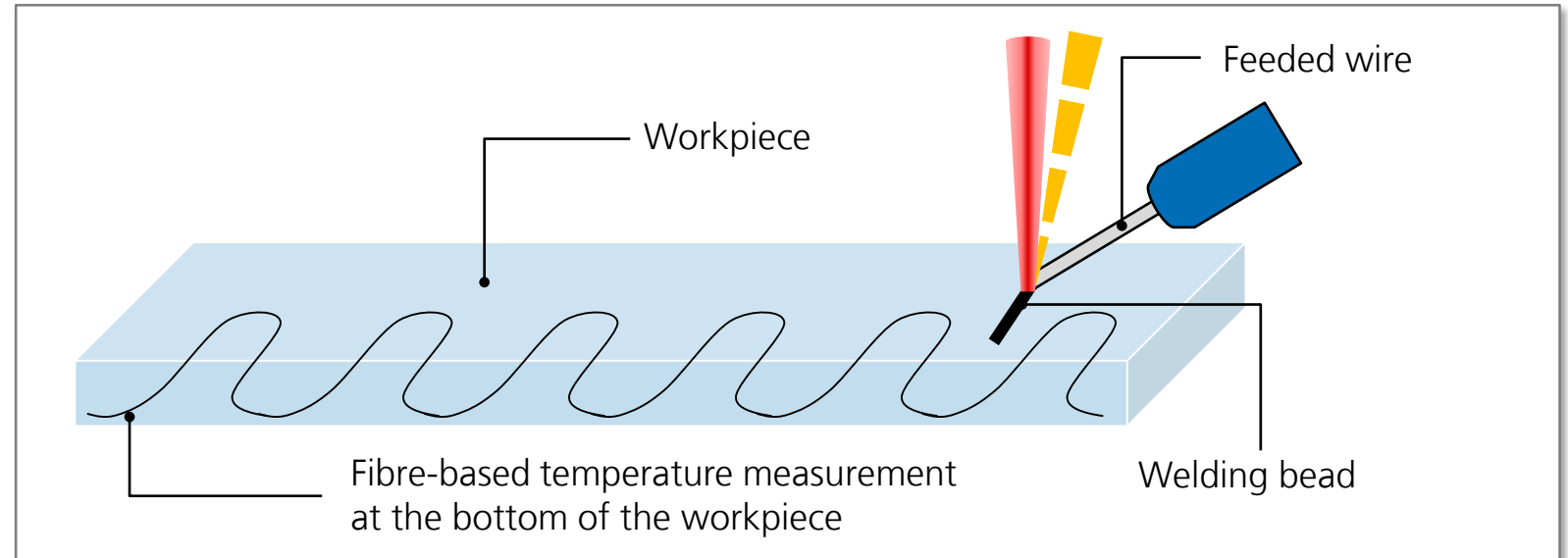


- The vapor created by the modulated laser has a significant influence on the global absorption
- Local minimum at intermediate powers and a decrease at high powers are observed
- Explanation possible by dissipation in the plasma (collision-based and collision-free effects) [Cui et al., 2013]

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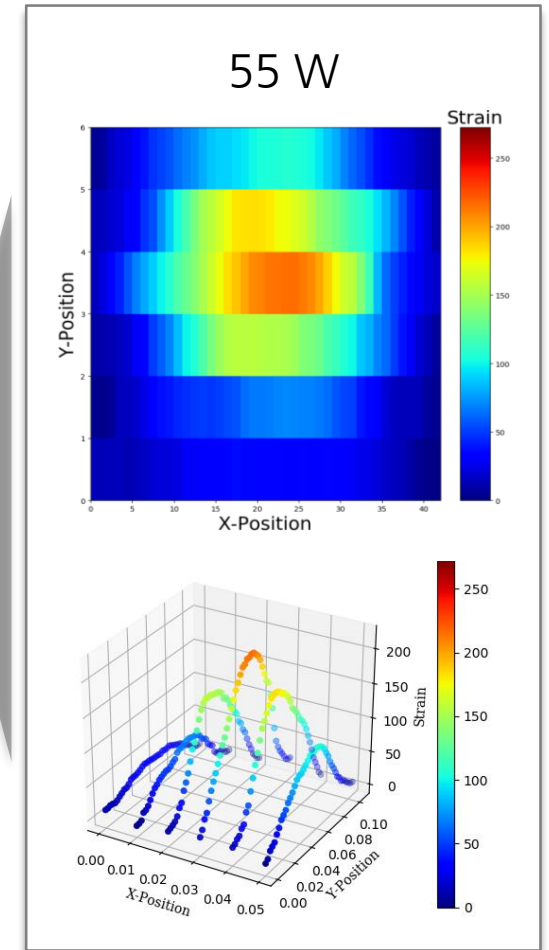
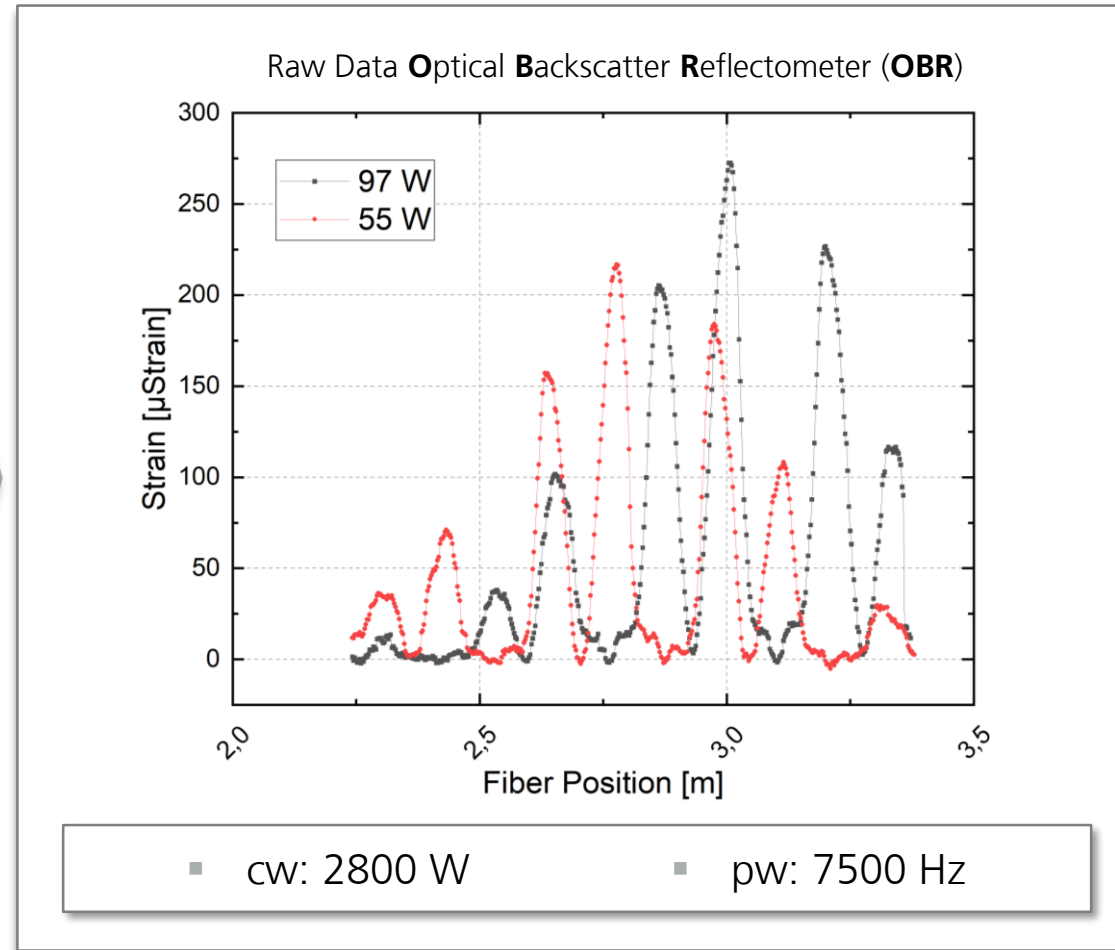
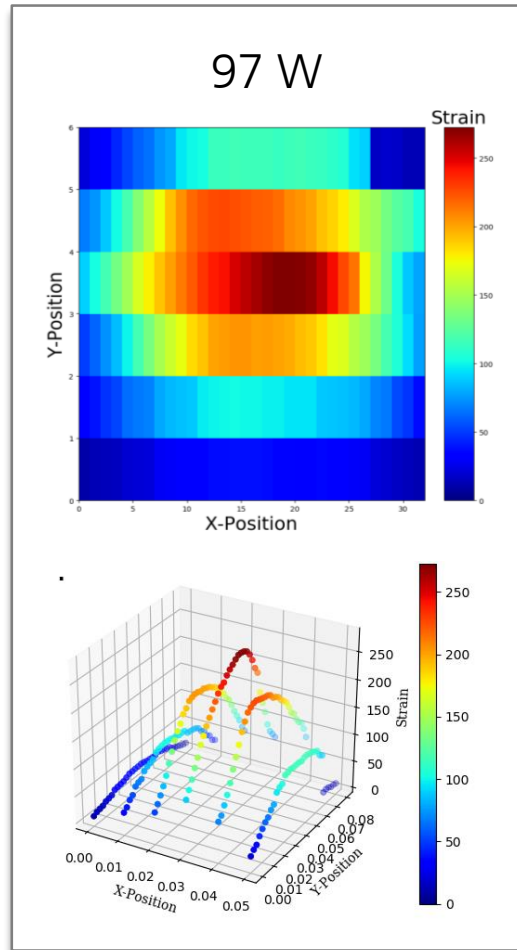
Modulated laser influence on workpiece temperature (I/III)

- Study of the workpiece temperature as a function of the pulsed laser parameters
- In-situ optical fiber-based temperature measurement via measurement of the fiber strain (**O**ptical **B**ackscattering **R**eflectometry, OBR)
- Strain measurement possible thanks to a periodic modulation of the refractive index in the fiber (**F**iber **B**ragg **G**rating, FBG)
- Comparison of maximum strains/temperatures and of the heat propagation behavior



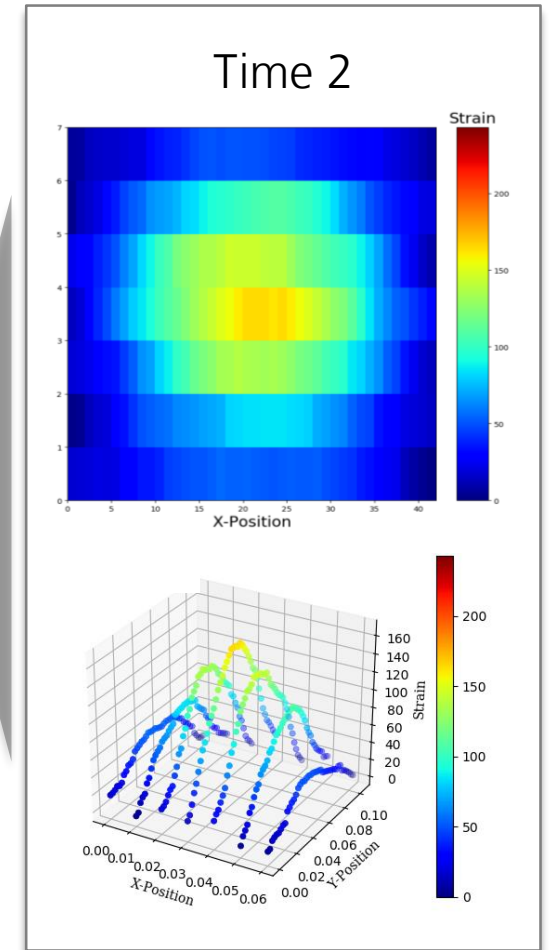
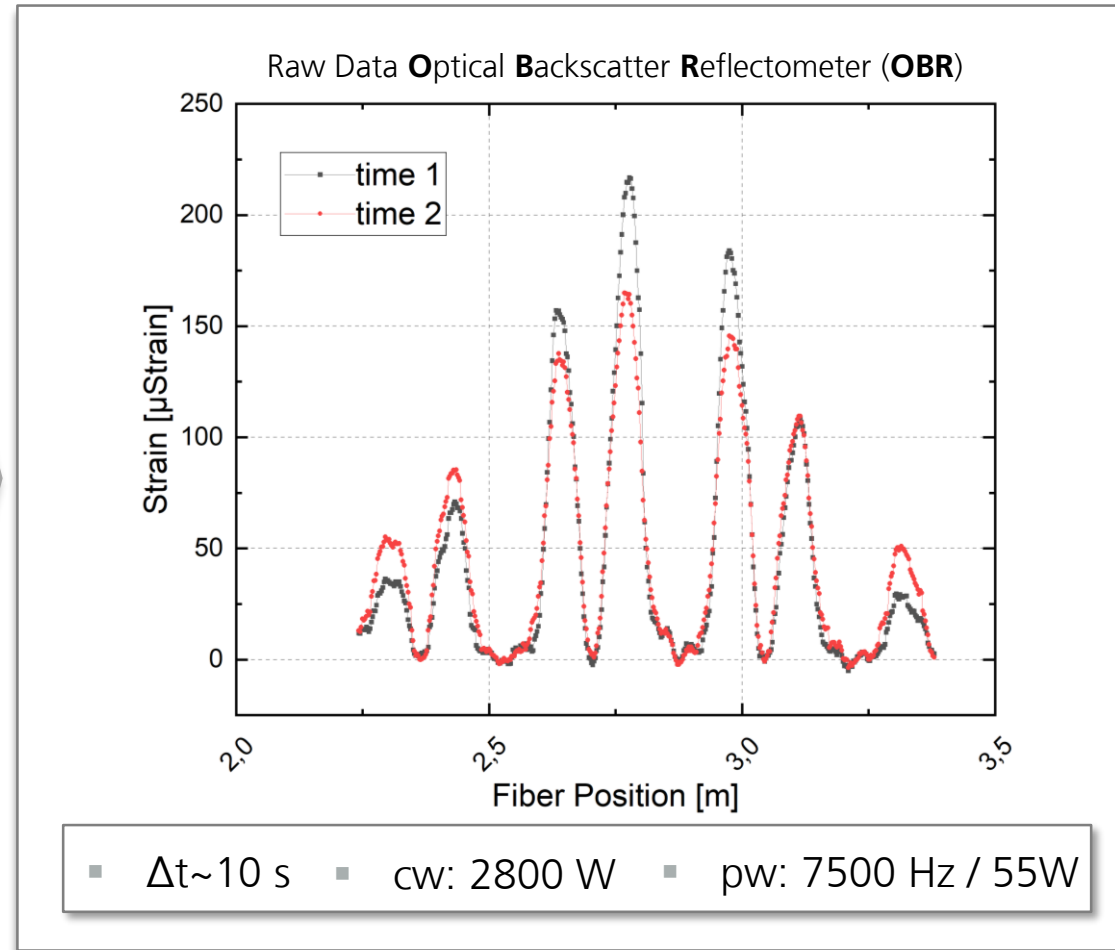
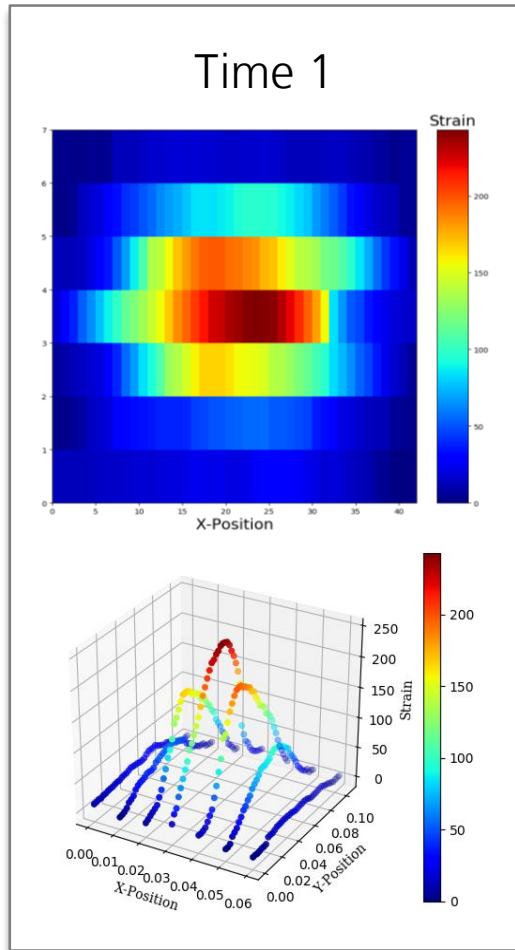
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Modulated laser influence on workpiece temperature (II/III)



Tailored melt pool shape and temperature distribution by dual laser beam LMD-w

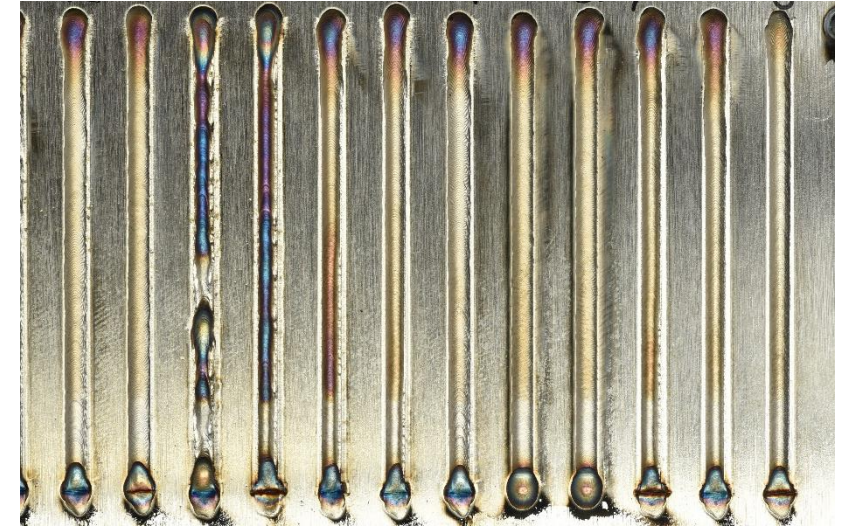
Modulated laser influence on workpiece temperature (III/III)



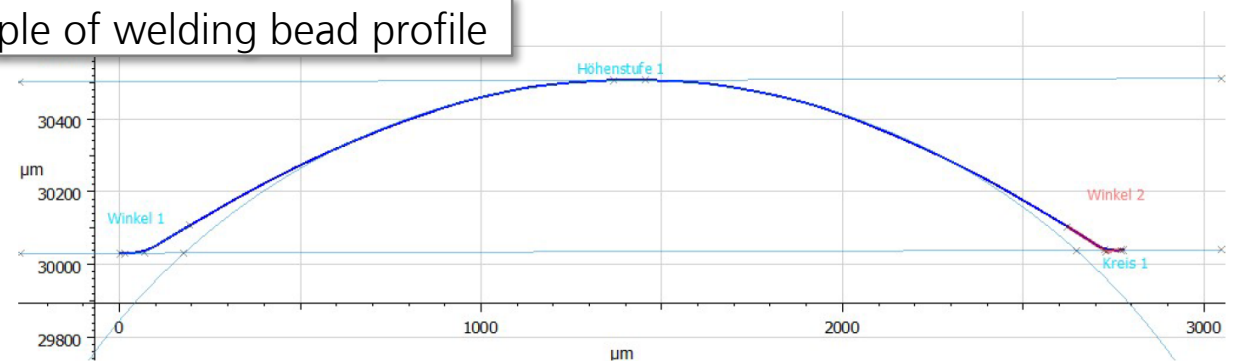
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Modulated laser influence on welding bead geometry (I/V)

- Deposition experiments (tool steel QuFe13 on S355)
- Constant parameters:
 $P_{L,c} = 2400 \text{ W}$
 $v_M = 1100 \text{ mm/min}$
 $v_W = 1600 \text{ mm/min}$
- pw parameters variated (frequency and power)
- Repetition to ensure reproducibility
- Surface characterization by depth-of-field measurement (Alicona G5)
- Evaluation of bead roughness and cross section

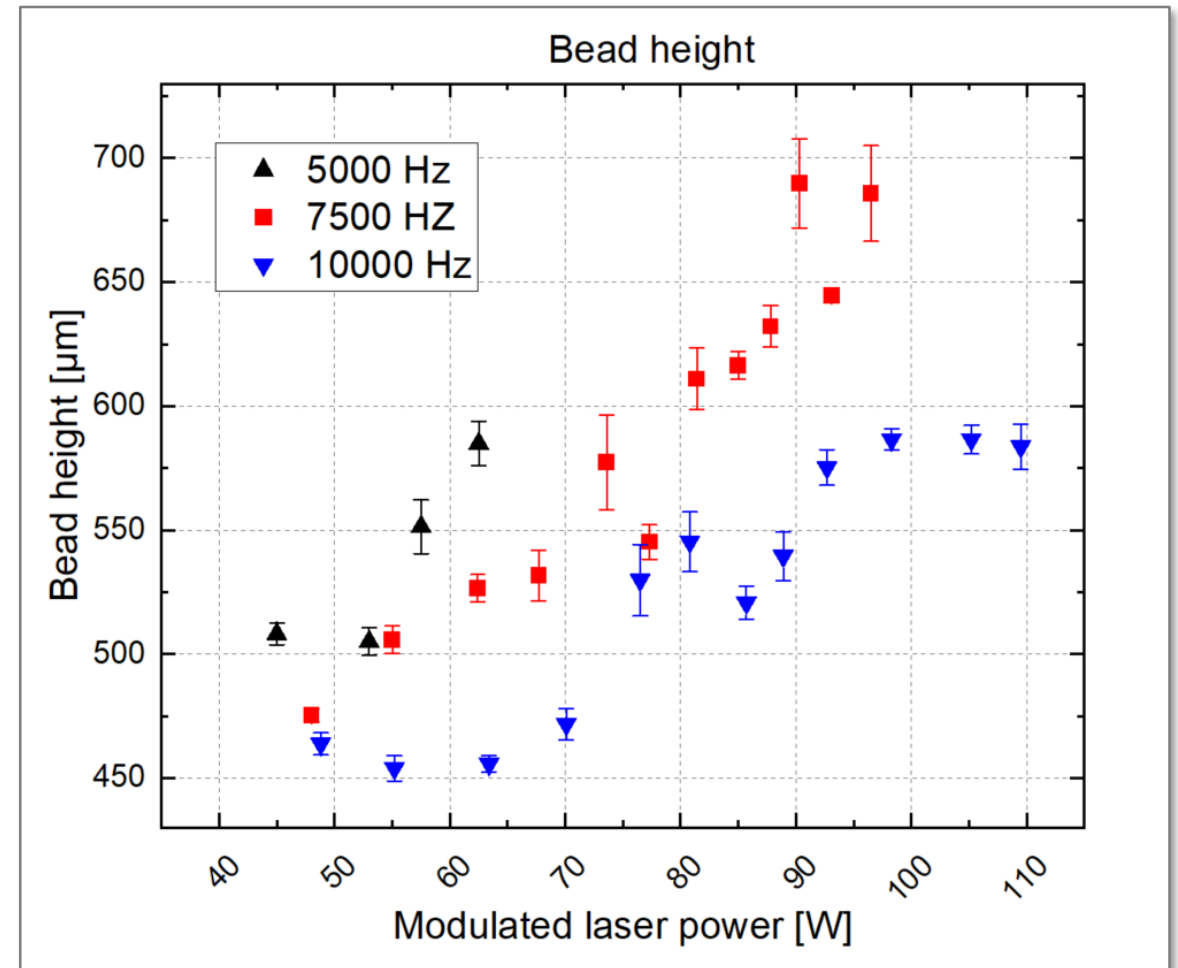
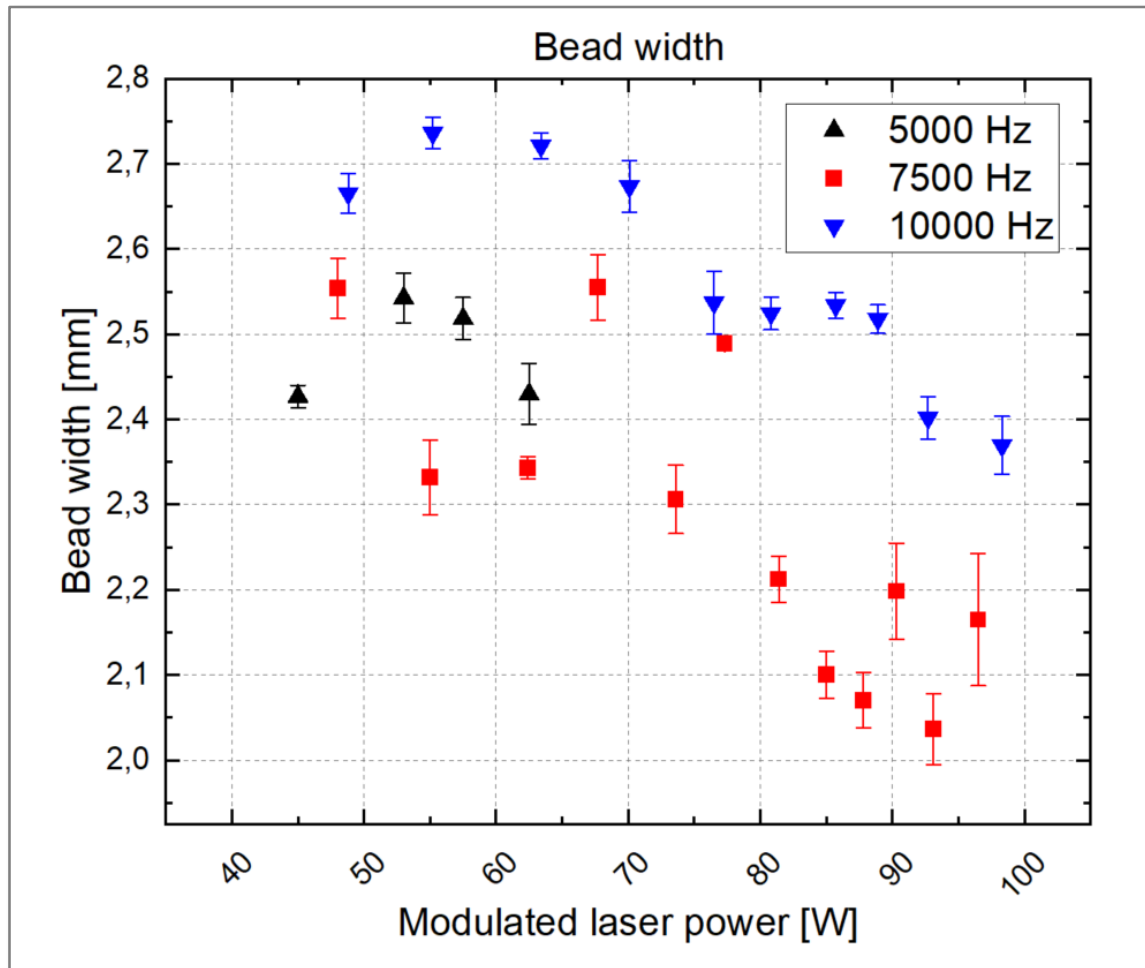


Example of welding bead profile



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Modulated laser influence on welding bead geometry (II/V)



Tailored melt pool shape and temperature distribution by dual laser beam LMD-w

Modulated laser influence on welding bead geometry (III/V)



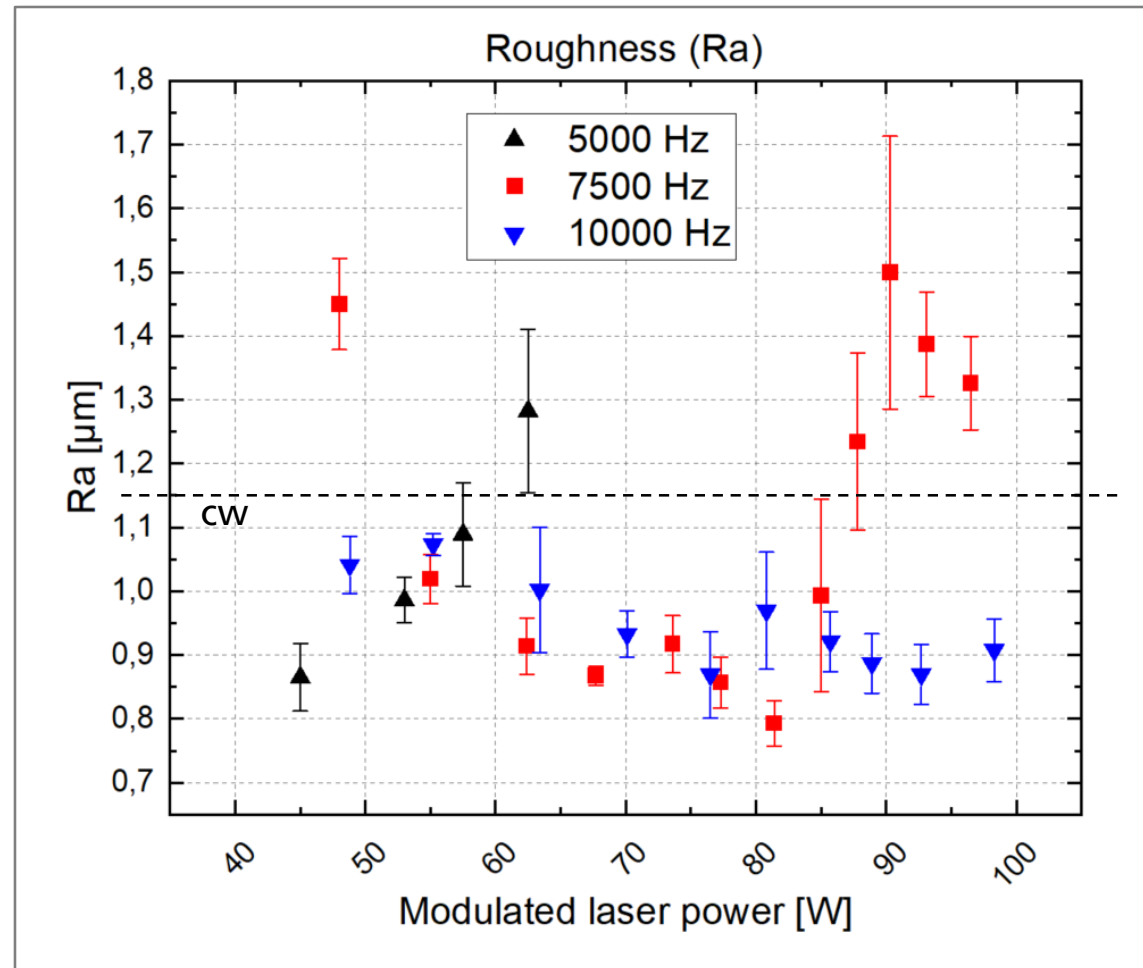
$$P_{L,c} = 2400 \text{ W}, v_M = 1100 \text{ mm/min}, v_W = 1600 \text{ mm/min}$$

$$f_p = 10000 \text{ Hz}, P_{L,m} = 49 \text{ W}$$

$$f_p = 10000 \text{ Hz}, P_{L,m} = 110 \text{ W}$$

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Modulated laser influence on welding bead geometry (IV/V)

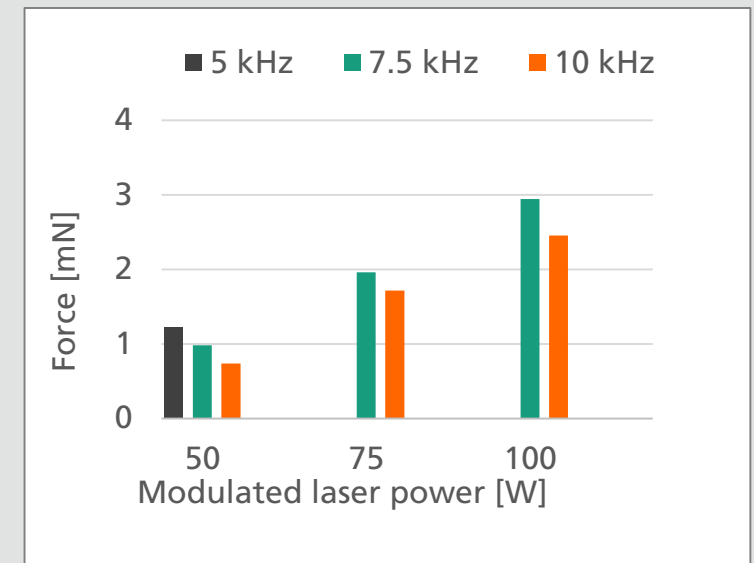
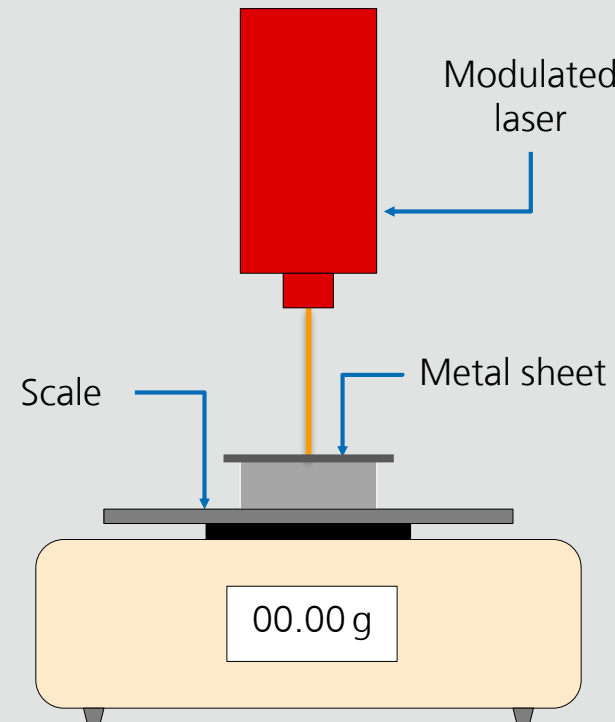


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Modulated laser influence on welding bead geometry (V/V)

- The bead geometry is strongly influenced by the evaporation-induced forces
- The stronger the forces, the higher and the narrower the welding beads
- At lower forces, the surface is smoothed; at higher forces, R_a increases as the liquid material is stirred up

Force measurements [Bergs et al., LiM 2019]



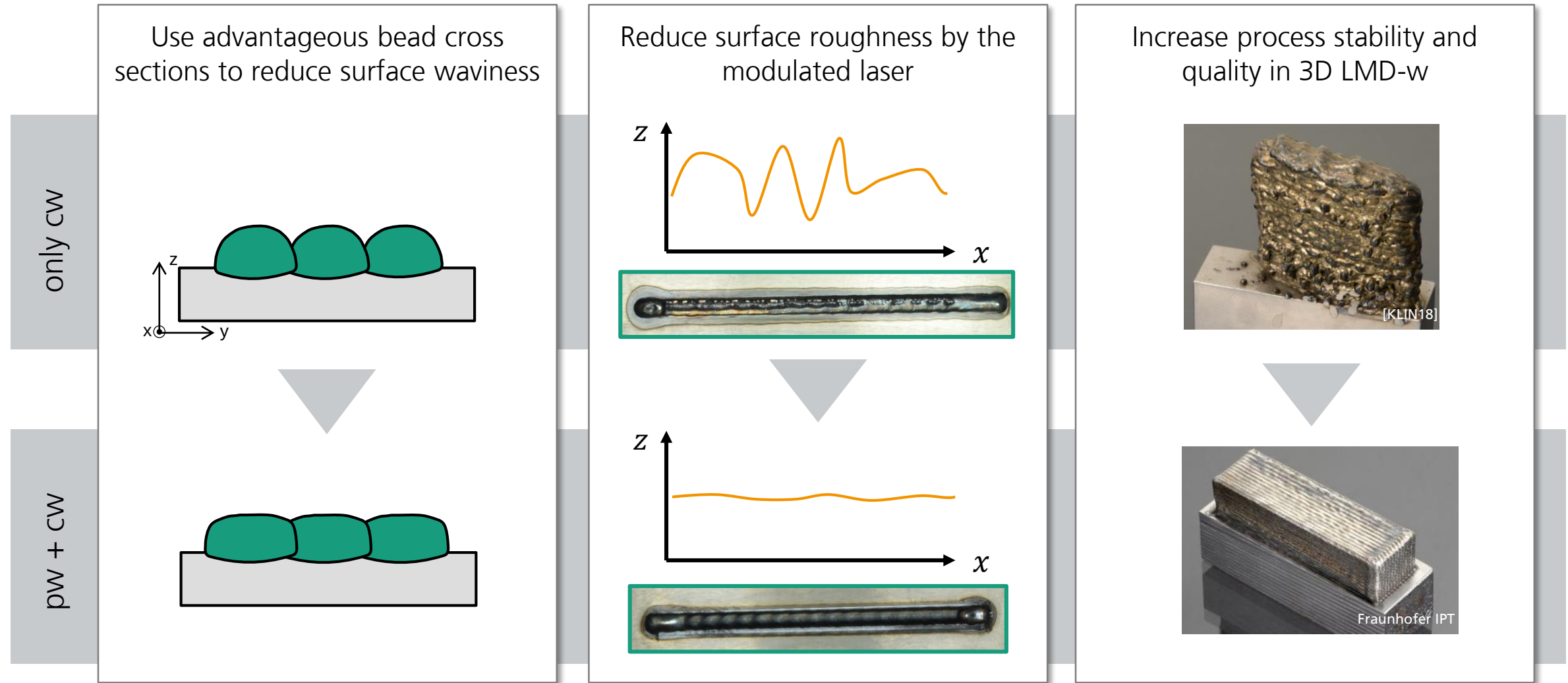
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Summary and conclusion

- Analysis of the modulated laser influence in a dual laser beam LMD-w process
- Identification of two main effects
 - Modification of the energy input / workpiece temperature (absorption-related)
 - Modification of the melt pool shape (force-related): welding bead cross section and roughness control
- The absorption coefficient can be increased by about 20 %
- The welding bead height and width can be tailored by a factor of maximum 2
- The welding bead surface roughness can be reduced

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Outlook



Tailored melt pool shape and temperature distribution by dual laser beam LMD-w

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Thank you for your
attention!

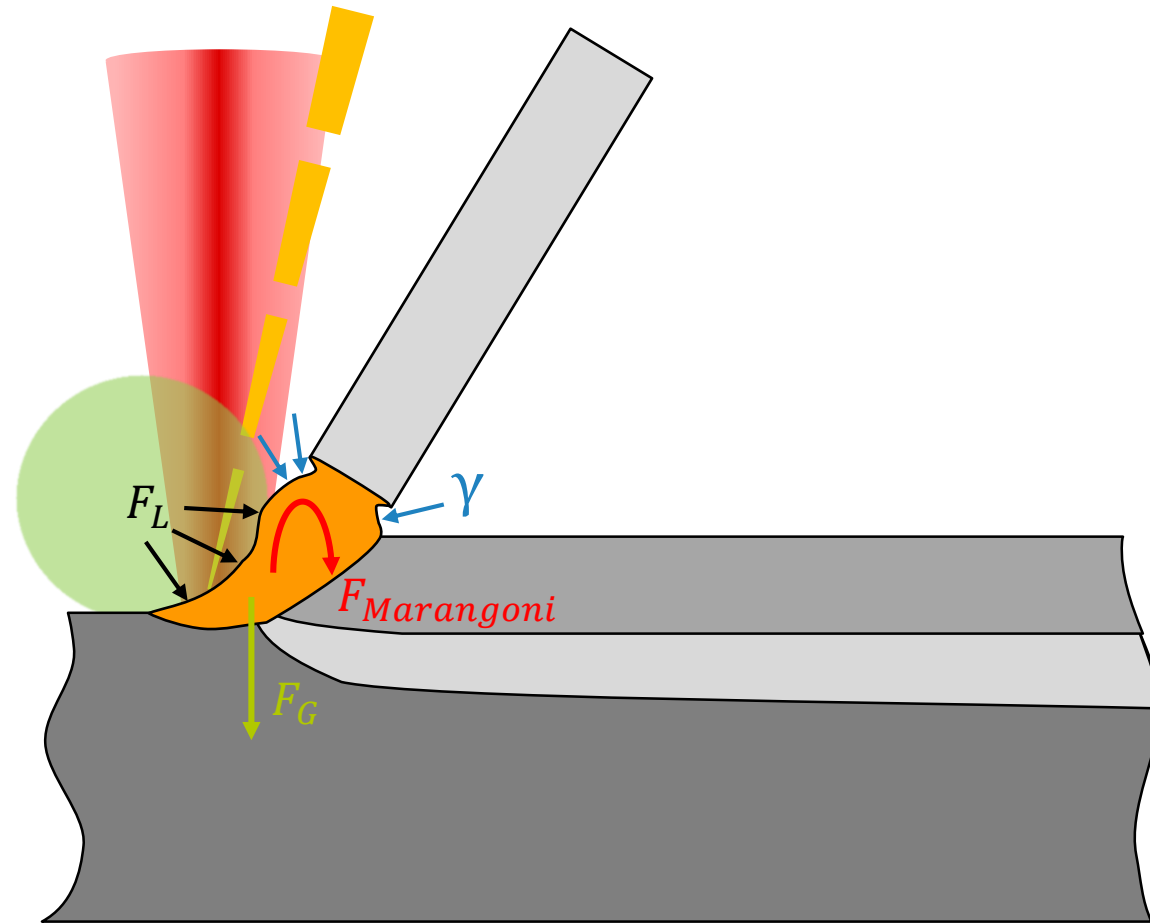
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Backup

Wt. %	C	Si	Mn	Mg	Cr	Cu	Mo	Ti	Ni	Zn	Fe	Al
S355 J0	0.2	0.55	1.6	-	-	0.55	-		0.01	-	Bal.	-
QuFe13 (Quada)	0.25	0.5	0.7	-	5.0	-	4.0	0.6	-	-	Bal.	-
EN AW 7075	-	0.4	0.3	2.5	0.23	1.5	-	0.2	-	5.5	0.5	Bal.

Backup



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Literature sources (I/II)

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