



Source: A. Kish 1996

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Fraunhofer at a Glance

60 Institutes

17 000 employees

about €1,6 billion research budget

7 Groups

- Information and Communication Technology
- Life Sciences
- Materials and Components
- Microelectronics
- Production
- Surface Technology and Photonics
- Defense and Security









IZFP at a Glance



Saarbrücken

Dresden

Methods and Techniques

Ultrasonic, Eddy Current, Electromagnetics, Micromagnetics, Microwave, x-ray-Radioscopie, Tomo-, Laminography, Atomic-Force-Mikroscopy, Thermography, Acoustic Emission, Nuclear Magnetic Resonance

Employees

- 120 Scientists and engineers
 - 12 Technicians & 29 supporting personnel
- 130 PhD and Diploma students, Research assistants Guest Scientists

Finances

- 23 Mio €, from which
- 11,8 Mio € by orders from industry



IZFP at a Glance

Business Units

Railway SB Automotive SB Aviation, Aerospace DD Metal Production, Processing SB Plant, Installation SB Power Plant, Power Line SB Piping Systems, Pipelines SB **Electronics and** Micro-Nano-Systems DD Environment, Life Sciences DD

















Automated systems AURA and UFPE to detect defects in wheels





Automated system AUROPA to detect defects in wheels

EMAT Sensors in the rail, Train speed 15 km/h to be increased till up to 30 Km/h





Automated systems to detect defects in axles

Probe Head Module for Bore Hole Ø 60 mm







Automated system UER to evaluate the stress state of the rim of railroad wheels



Ultrasonic Techniques to Evaluate Stress States

The acousto-elastic effect



The strain state influences the propagation velocities of ultrasonic waves. The size of the acousto-elastic effect depends on the directions of wave propagation and vibration





Ultrasonic Techniques to Evaluate Stress States

Influence of strain or stress state on the longitudinal wave velocity

$$\rho_0 v_{ii}^2 = \rho v_L^2 + (2I + \lambda) (\varepsilon_i + \varepsilon_j + \varepsilon_k) + (4m + 4\lambda + 10\mu) \varepsilon_i$$

Approximation:	$2v_{L} = v_{ii} + v_{L}$
Hook's Law:	$\overline{\epsilon}_{i} = 1/E [\overline{\sigma}_{i} - \nu (\sigma_{i} + \sigma_{k})]$
Young's Modul:	$E = \mu (3\lambda + 2\mu) / (\lambda + \mu)$
Poisson ratio:	$v = \lambda/2 \ (\lambda + \mu)$

$$\frac{\mathbf{v}_{ii} - \mathbf{v}_L}{\mathbf{v}_L} = \frac{\mathbf{t}_L - \mathbf{t}_{ii}}{\mathbf{t}_{ii}} = \frac{\mathbf{A}}{\mathbf{C}} \cdot \mathbf{\sigma}_i + \frac{\mathbf{B}}{\mathbf{C}} (\mathbf{\sigma}_j + \mathbf{\sigma}_k)$$

 $\begin{array}{l} \mathsf{A}=2\;(\lambda{+}\mu)\;(4m{+}5\lambda{+}10\mu{+}2l)-2\lambda\;(2l{+}\lambda)\\ \mathsf{B}=2\;(2l{+}\lambda)\;(\lambda{+}\mu)\;{-}\lambda\;(2l{+}\lambda)-\lambda\;(4m{+}5\lambda{+}10\mu{+}2l)\\ \mathsf{C}=4\mu\;(\lambda{+}2\mu)\;(3\lambda{+}2\mu) \end{array}$



Ultrasonic Techniques to Evaluate Stress States

Influence of strain or stress state on the shear wave velocity

$$\begin{split} \rho_{0}v_{ij}^{2} &= \mu + (\lambda + m) \left(\epsilon_{i} + \epsilon_{j} + \epsilon_{k}\right) + 4\mu \epsilon_{i} + 2\mu \epsilon_{j} - 0,5n \epsilon_{k} \\ \text{Approximation:} & 2v_{T} = v_{ij} + v_{T} \\ \text{Hookes Law:} & \epsilon_{i} = 1/E \left[\sigma_{i} - v \left(\sigma_{j} + \sigma_{k}\right)\right] \\ \text{E} - \text{Youngs Modulus:} & \text{E} = \mu \left(3\lambda + 2\mu\right) / \left(\lambda + \mu\right) \\ \text{Poisson - Ratio:} & v = \lambda/2 \left(\lambda + \mu\right) \\ \frac{v_{ij} - v_{T}}{v_{T}} &= \frac{t_{T} - t_{ij}}{t_{ij}} = \frac{D}{K} \cdot \sigma_{i} + \frac{H}{K} \cdot \sigma_{j} + \frac{F}{K} \cdot \sigma_{k} \\ \text{D} = 2 \left(\lambda + \mu\right) \left(\lambda + m + 4\mu\right) - \lambda \left(2\lambda + 2m + 2\mu - 0, 5n\right) \\ \text{H} = 2 \left(\lambda + \mu\right) \left(\lambda + m + 2\mu\right) - \lambda \left(2\lambda + 2m + 4\mu - 0, 5n\right) \\ \text{F} = 2 \left(\lambda + \mu\right) \left(\lambda + m - 0, 5n\right) - \lambda \left(2\lambda + 2m + 6\mu\right) \\ \text{K} = 4\mu^{2} \left(3\lambda + 2\mu\right) \\ \frac{v_{ij} - v_{ik}}{v_{ik}} &= \frac{t_{ik} - t_{ij}}{t_{ij}} = \frac{\left(4\mu + n\right)}{8\mu^{2}} \left(\sigma_{j} - \sigma_{k}\right) \end{split}$$



Situation and Task

Very typical distribution of the stress component σ_{Length} along height of new rail



Fig.2. Distribution of longitudinal residual stress in a cross-section of a rail.

Source: A. Brokowski, J. Deputat, WCNDT, 1985

Typical result:

- + Tensile stress in the head
- + Compressive stress in web
- + Tensile stress in foot area
- + stress distribution mainly influenced by roller straightening condition



Situation and Task

Assumption

* residual stress averages to zero at any length position

* rail has neutral temperature during final welding

Result

=> there is no stress, except stress σ_{Lenath} induced by temperature change

Request

! Evaluation of temperature induced stress

! Evaluation of neutral temperature or stress free temperature

Problem

- Measurements covering the cross section are at least time consuming
- Strain or stress states superimpose each other, independent of origin
- There is no reliable non destructive technique to evaluate or check the neutral temperature except during bedding and final welding



Stress State of Tread Area of New Rails

Results of destructive ring-core-technique; MPA Stuttgart



Principal result:

- + One dimensional stress state
- + Principal stress along width negligible
- + Tensile stress along length, mainly due to roller straightening



DEBRO-approach and system of the Polish Academy of Science, Warsaw



Fig. 2. Layout of ultrasonic transducers to measure the difference in travel times of subsurface ultrasonic longitudinal waves (1 - transmitter, 2, 3 - receivers); and transverse waves (4 - transmitters, 5, 6 - receivers). Relevant pulses are shown above.

Idea

The same stress state influences the velocities of ultrasonic waves differently in size and sign, depending on the propagation and vibration direction with respect to the principal stresses

Use of different wave types to discriminate e.g. the microstructural influences

Source: J. Deputat; ACUSTICA 79 (1993) 161-169



Different possibilities of ultrasonic applications, tested by IZFP





Time-of-flight (TOF) of a longitudinal wave propagating between transmitter and receiver probe with fixed distance, penetration depth about 3 mm





Time-of-flight (TOF) of a longitudinal wave propagating between transmitter and receiver probe with fixed distance, penetration depth about 3 mm

Continuous measurement of time-of-flight along length of new rail samples 5, 2; Sound propagates the tread (red) and the outer side of rail head (blue)

TOF [ns]





Results of ultrasonic stress analysis

Stress along length of new rail sample 5 and 2;

 σ_{Length} in tread area (red) and σ_{Length} in outer side of rail head (blue)



Stress along Length [MPa]

Fraunhofer

Comparison of ultrasonic and ring-core results of stress analysis



In order to avoid errors caused by local inhomogeneities of the material, the stress results should be averaged along a certain part of rail length



State

- + There is a quasi one dimensional stress state in new rails with the major stress component σ_{Length} along the length of rail
- + The stress state varies at different positions along the length of the rail mainly because of influences of straightening and cooling conditions
- + Different ultrasonic and micromagnetic techniques are available to evaluate the stress σ_{Lenath} along the length





Situation concerning Rails in the Track

Very typical distribution of the stress component σ_{Length} along height of used rail



Source: P.R. Cheesewright: A Critical Review of Residual Stress Measurement in Rails, British Railway Board, Technical Note, TN STM 15, 1980 Important result:

- + Compressive stress σ_{Length} (blue, S_L) in tread area
- + Compressive stress σ_{Width} (red, S_T) in tread area
- + Stress σ_{Width} larger in size than stress σ_{Length}
- + no significant change of stress profiles with increasing load tons (threshold at about 0.5 Mt)



Situation and Task, concerning Rails in the Track





Situation and Task, concerning Rails in the Track

Very typical distribution of the stress component σ_{Length} along height of used rail



Source: E. Jericho; ETR 46 Heft 10 (1997) 663-666



Stress State of Used Rails, Cut from the Track



Results of destructive ring-core-technique; MPA Stuttgart



Stress State of Used Rails

0 -50 Principal result: -100 + Two dimensional -150 stress state -200 + Principal stresses along Stress [MPa] -250 length and width -300 + Compressive stresses + Stress along width -350 usually larger in size -400 than stress along length -450 ARail11Width Rail11Length -500 Rail12Length -550 -Rail12Width -600 0,0 0,5 1,0 1,5 2,0 2,5 3,0 3,5 4,0 4,5 5,0 Depth from Surface [mm]

Results of destructive ring-core-technique; MPA Stuttgart



Situation and Task concerning Stress Analysis in the Track

Assumption

* residual stress averages to zero at any length position / not important

* rail has neutral temperature during final welding

Result

=> there is no stress, except stress induced by temperature change / not true

Request

! Evaluation of temperature induced stress / will not be sufficient to prevent
! Evaluation of neutral temperature / buckling or cracking

Problem

not meaningful

- Measurements covering the cross section are at least time consuming
- Strain or stress states superimpose each other, independent of origin

=> A new approach is needed



Approach

IZFP suggestion

- * Evaluation of total stress state of tread (σ_{Width} and σ_{Length}) caused by
 - manufacturing (residual stress; cross section, different along length), by
 - bedding (elastic and anelastic local deformations, cross section), by
 - welding (very local, cross section), by
 - traffic (long ranged stress influence, similar in a range of a few meters, tread area only), by
 - temperature changes (long ranged, tens of meters, cross section)
- * Measurement of rail temperature
 - Evaluation of temperature induce stress using thermal expansion coefficient and temperature base of 20℃;
 - Evaluation of Stress state of treat caused by manufacturing, bedding, welding and traffic
- * Model buckling safety based on stored energy (stress state), rail size, tie type, track curvature, etc. as suggested by e.g. A. Kish, G. Samavedam, D. Read



Ultrasonic Approach

IZFP suggestion



- * Measurement of SHo time-of-flight (TOF) in treat area (influence of σ_{Width} and σ_{Length} plus microstructure)
- * Measurement of SHo TOF on outer side of head
- (influence of microstructure)
- * Measurement of rail temperature
- * Evaluation of stress state of tread (influence of σ_{Width} and σ_{Length})
- * Model buckling safety based on stored energy (stress state) and tie type track curvature
 - etc as suggested by e.g. A. Kish,
 - G. Samavedam, D. Read



Time-of-flight (TOF) of a SHo wave propagating between transmitter and receiver probe with fixed distance vs load tons applied in a over-rolling-test stand



Relative change of TOF of SHo wave [o/oo]

SHo wave propagates the tread in a surface layer of about 6 mm of thickness



Time-of-flight (TOF) of a SHo wave propagating between transmitter and receiver probe with fixed distance vs load tons applied in a over-rolling-test stand

Relative change of TOF of SHo wave [o/oo]



SHo wave propagates the outer side of the rail head in a surface layer of about 4 mm of thickness



Time-of-flight (TOF) of a SHo wave propagating between transmitter and receiver probe with fixed distance vs load tons applied in a over-rolling-test stand

Relative change of TOF of SHo wave [o/oo]



SHo wave propagates the tread of the rail head in a surface layer of about 6 mm of thickness



Time-of-flight (TOF) of a SHo wave propagating between transmitter and receiver probe with fixed distance vs load tons applied in a over-rolling-test stand

Relative change of TOF of SHo wave [o/oo]



SHo wave propagates the outer side of the rail head in a surface layer of about 4 mm of thickness



Comparison of ultrasonic and ring-core results of samples of new and used rails



In order to avoid errors caused by local inhomogeneities of the material, the stress results should be averaged along a certain part of rail length



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MicroMagnetic Evaluation of Stress State of Used Rails

3MA system was calibrated using the ring-core result of -248 MPa and taking reference values in the vicinity of the ring-core measuring point (pink).



After calibration, the 3MA system was used to evaluate the stress σ_{Length} in the tread at other measuring positions (blue).



MicroMagnetic Evaluation of Stress State of Used Rails

3MA system was calibrated using the ring-core results of -168 MPa (left), -105 MPa (right) and taking reference values in the vicinities, respectively (pink).



After calibration, the 3MA system was used to evaluate the stress σ_{Length} in the tread at other measuring positions (blue).



MicroMagnetic Evaluation of Stress State of Used Rails

3MA system was calibrated using the ring-core results of all the individual rails and taking reference values in the vicinities, respectively.



Using the one calibration function, the stress values σ_{Length} in the tread of the 5 samples of used rails are evaluated.



Approach to Evaluate Stress States of Rails in the Track

IZFP suggestion

* Measurement of rail temperature

Influence of temperature

 1) Linear expansion coefficient α _{Fe}= 12,1 x 10 ⁻⁶ / K and Youngs-Modulus of 210 GPa
=> Temp Change of 10℃ causes a change of stress σ _{Length} of about 25 MPa

- 2) Ultrasonic velocities decrease linearly with increasing material temperature
 - => Temp Change of 10℃ causes a relative velocity change of about 1.2 ‰

and also the acousto-elastic effect causes a change of the shear wave velocity: => about 150 MPa cause a change of 1.2 ‰

=> rail temperature has to be measured with an accuracy of at least $\pm 1^{\circ}$ C



Approach

Influence of rail temperature on TOF of SHo wave, due to thermally induced stress (blue) and due to temperature dependence of sound velocity (red)





Ultrasonic System for Stress Analysis on Rails

IZFP Version UES; 1997; mounted on cart by DB





Ultrasonic System for Stress Analysis

IZFP system, 2008





Ultrasonic System for Stress Analysis

IZFP system, 2008

A-Scan (bottom), measured signal (yellow) and reference signal (blue), curve of correlation function (center) and max value of correlation function (top)





Ultrasonic Transducer for Stress Analysis

IZFP EMAT's for SHo wave



EMAT SHo Transducer

Sketch of coil and current (red) Resulting forces on metallic lattice

Arrangement of permanent magnets

View towards the food of transducer



MicroMagnetic 3MA and MicroMach System

Electromagnetic, micromagnetic, magneto-elastic material properties are measured and correlated to e.g. with Stress, Rp0,2, Rm, Hardness, Depth





State

- 1) The concept:
 - measuring the total stress state of the tread,
 - separate the thermally induced stress by measurements of the rail temperature,
 - use the mean value of stress results, measured at different tread positions along at least two tie spaces in order to minimize the influence of structural inhomogeneities

needs to be discussed in detail and accepted.

 2) Ultrasonic systems are developed. The EMAT sensors need to be built for the stress analysis according to the mentioned concept.
It is recommended to perform measurements at individual fixed positions rather than continuously along the length.





State

- 3) It will be possible to monitor
 - the stress state and its changes with the traffic load;
 - the stress state and change in the entrance/exit area of tunnels and bridges
 - the stress state of switches and its change
 - the stress state of the track in the vicinity of underpasses
 - It will be possible to
 - measure and monitor the temperature of the bulk of the rail, using a EMAT shear wave sensor as shown.





State

- 4) It seems to be feasible
 - to integrate the EMAT Transmitter Receiver SHo sensors into the head of rail, similarly to the AUROPA sensors as shown in the figure,
 - to monitor the dynamic change of stress state, taking advantage of the measuring rate of the ultrasonic TOF measurement of 50 Hz
 - to improve existing models for track buckling and uplift using the knowledge of the stress state of the track section
 - to develop a model for the characterization of the roadbed condition based on measurements of rail strain/stress state and dynamic changes





Source: A. Kish 1996



Literature

- Fritz Fastenrath, Die Eisenbahnschiene Theoretische und praktische Hinweise zur Beanspruchung, Werkstoffbeschaffenheit, Profilwahl, Verschweißung und Behandlung in Gleis und Werkstatt, Verlag von Wilhelm Ernst & Sohn, 1977
- Magnetic Measurement of Lonitudinal Forces in C.W.R. Track PKP, ORE, DT 225 (D 150), Utrecht, September 1990
- Bericht Nr. 4, Untersuchungen zur Messung und Verbesserung der Höhe der Eigenspannungen, ORE, Frage D 156, Utrecht, September 1987
- Bericht Nr. 5, Erweiterung des Verfahrens der magnetischen Parameter zur Einführung der Magnetisierung der gesamten Schiene, ORE, Frage D 150, Utrecht, September 1983
- Bericht. Nr. 3, Bewertung der Messverfahren; Methode der Reaktion der schwingenden Schiene, ORE, Frage D 150, Utrecht, April 1982
- Bericht Nr. 2, Ausführliche Bewertung der technischen Verfahren die Methode der magnetischen Parameter, ORE, Frage D 150, Utrecht, April 1981
- Bewertung eines Biegereaktionsverfahrens auf der Grundlage von Phasenmessungen, zur Ermittlung der Schienenlängskräfte, G.S. Lane, ORE, DT 128 (D 150), Utrecht, Oktober 1981
- Bericht Nr. 1, Vorauswahl der technischen Verfahren zur Bestimmung der Schienen-Längskräfte, ORE, D 150/RP 1/D, Utrecht, September 1980
- Bericht Nr. 6, Eigenspannungen in der Schiene (Fortsetzung) Untersuchung der kaltverfestigten Zone, ORE, C 53/ RP 6/D, Utrecht, Oktober 1970



Literature

- G. Posgay, P. Molnar, Investigations Using Magnetic Barkhausen Noise Measurement, Metalelektro Ltd., 28.03.1997
- Manfred Heyder, Herbert Schmedders, Georg Uhlig, Klaus Wick, Stand der Entwicklung kontinuierlich arbeitender Prüfverfahren für Schienen, Schienentagung, Nürnberg, 1985
- Wilhelm Guericke, Jürgen Weiser, Herbert Schmedders, Robert Dannenberg, Ursachen von Schienen-Eigenspannungen infolge Rollenrichtens und Beitrag zur Verringerung, ETR 46 (1997), H. 10, Oktober, S. 655 – 662
- Erwin Jericho, Schienen mit geringeren Eigenspannungen, ETR 46 (1997), H. 10, Oktober, S. 663 666
- Andrew Kish, Gopal Samavedam, David Wormley, Recent Investigations on Track Lateral Shift Limits for High-Speed Rail Applications, WCRR 1997, Firenze, 16-19 November 1997, p. 41 – 49
- F. D. Fischer, E. Hinteregger, F. G. Rammerstorfer, A Study on the Residual Stresses in Railroad Rails after Cooling Down from the Rolling Temperature, ASME, AMD Vol. 96, RTD Vol. 2, p. 37 – 43
- Andrew Kish, Gopal Samavedam, David Read, Track Buckling Models and Verification Testing, Colorado Springs World Conference, 1996
- M. K. Devine, Detection of Stress in Railroad Steels via Magnetic Property Measurements, Non-Destructive Testing Evaluation, 1994, Vol. 11, p. 215 – 234
- J. Deputat, Ultrasonic Measurement of Residual Stresses Under Industrial Conditions, Acustica, Vol. 79, 1993, p. 161 – 169



Literature

- Allan M. Zarembski, The Influence of Residual Stresses on Crack Propagation, Railway Track & Structures, April, 1993, p. 9, 10
- F. D. Fischer, E. Hinteregger, F. G. Rammerstorfer, Numerische Simulation einer experimentellen Spannungsanalyse, Materialprüfung 32, 1990, S. 181 185
- Hans-Jörg Höhberger, Johann Werner Spies, Messverfahren zur Erfassung von Längsspannung und spannungsfreier Temperatur im lückenlos verschweißten Gleis, ETR 37, 1988, H. 1/2, S. 61 – 66
- Andrzej Brokowski, Julian Deputat, Ultrasonic Measurements of Residual Stresses in Rails, Proc. 11, World Conference on Non-Destructive Testing, Las Vegas 1985, Vol. 1, p. 592 - 598

