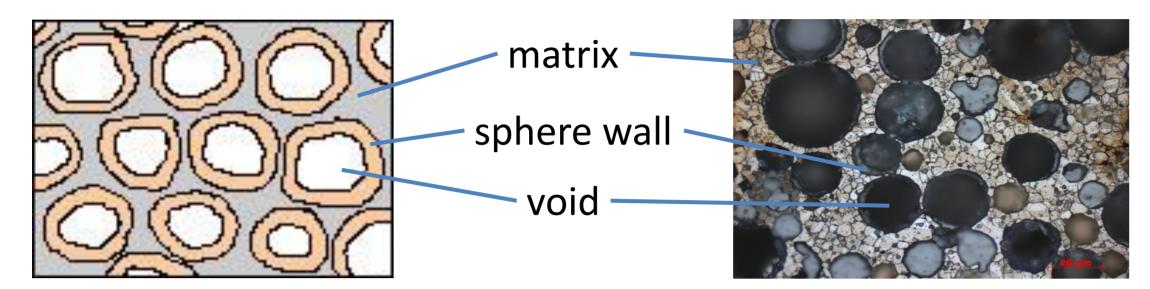
Fatigue behavior of syntactic Fe-36Ni foams under different stress ratios

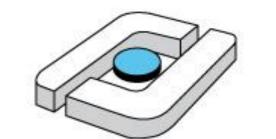
Philipp Poltersdorf, <u>Srecko Nesic</u>, Joachim Baumeister, Jörg Weise, Ulrich Krupp

METFOAM, Raleigh, USA, June 23-26, 2013

Introduction

Syntactic metal foams are a material class between classic closed-celled foams and particle reinforced composites. Porosity is created by hollow particles, integrated in a solid matrix. Different sphere types can be used: metal, ceramics, glass or cenospheres, see e.g. [1].





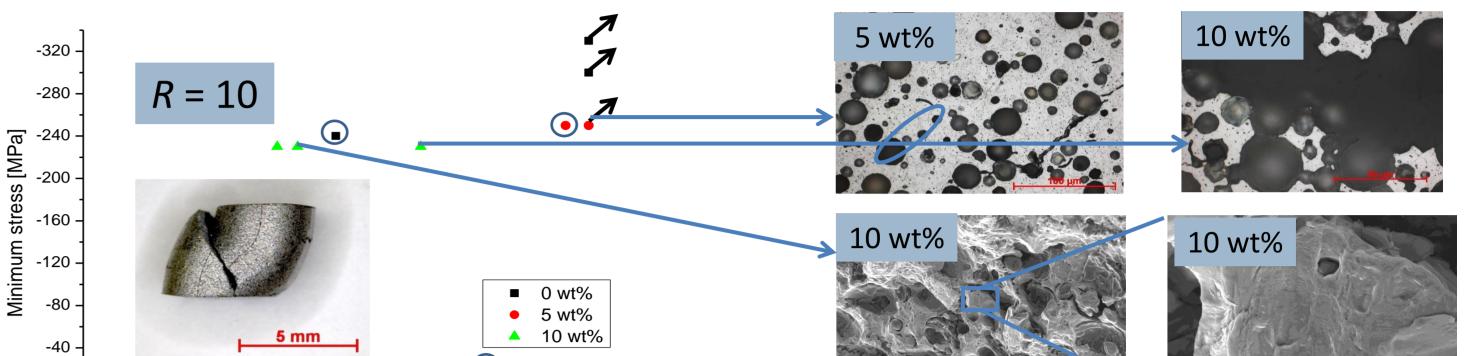
Hochschule Osnabrück

University of Applied Sciences









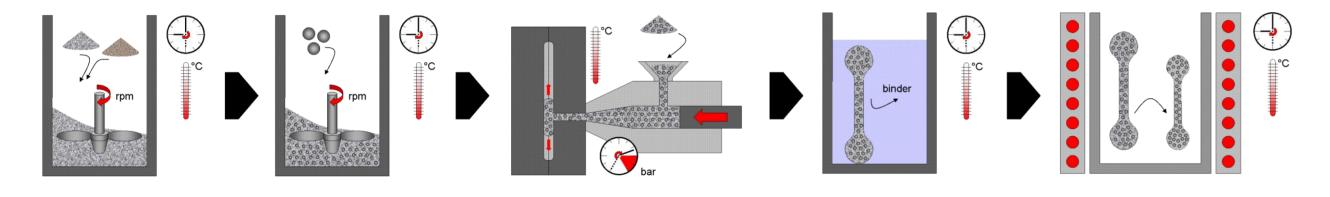
excellent vibration damping high compression strength high specific energy absorption

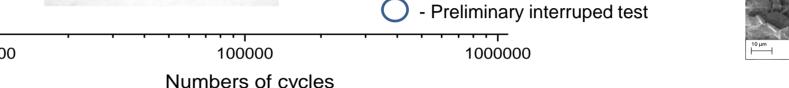
properties

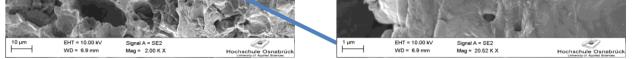
Objective of the project: Crash-relevant and vibration damping components are also subjected to cyclic loads. Therefore, the behaviour of syntactic foams under such loads are investigated for the example of FeNi36 foam.

Experimental approach

Dog-bone-shaped Fe-36Ni foam samples with different weight fractions (0/5/10wt%) of S60HS hollow particles were produced by means of metal injection moulding using a similar approach as described in [2].

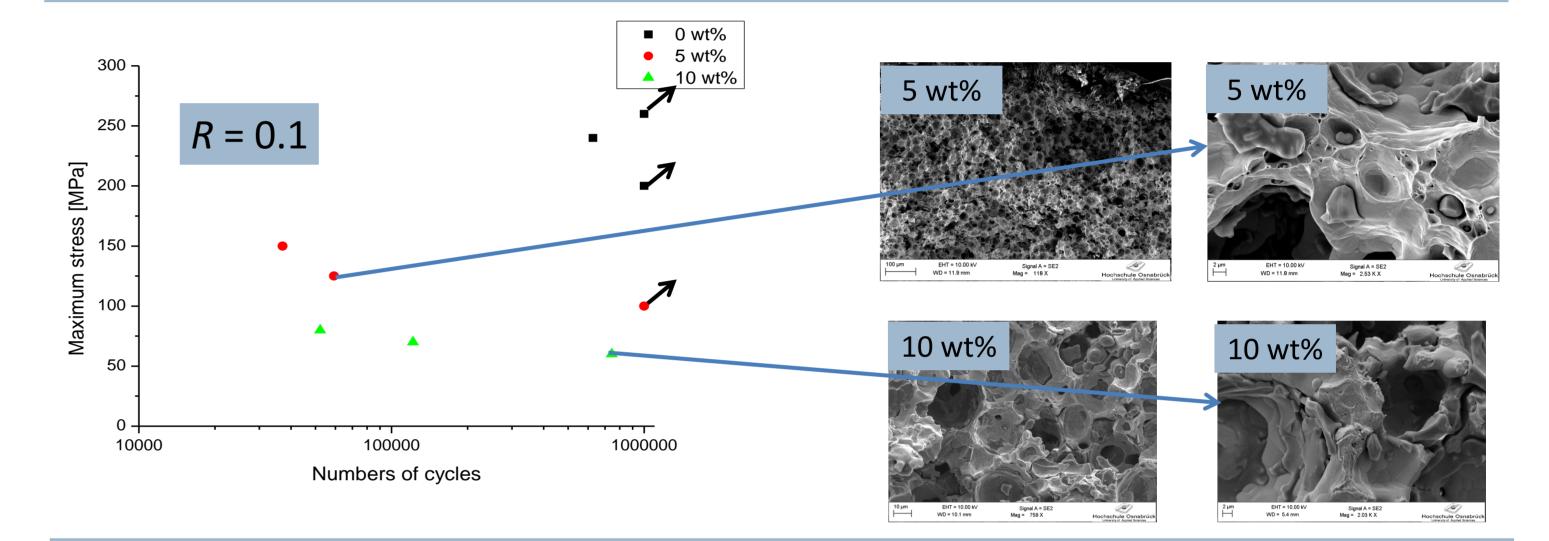




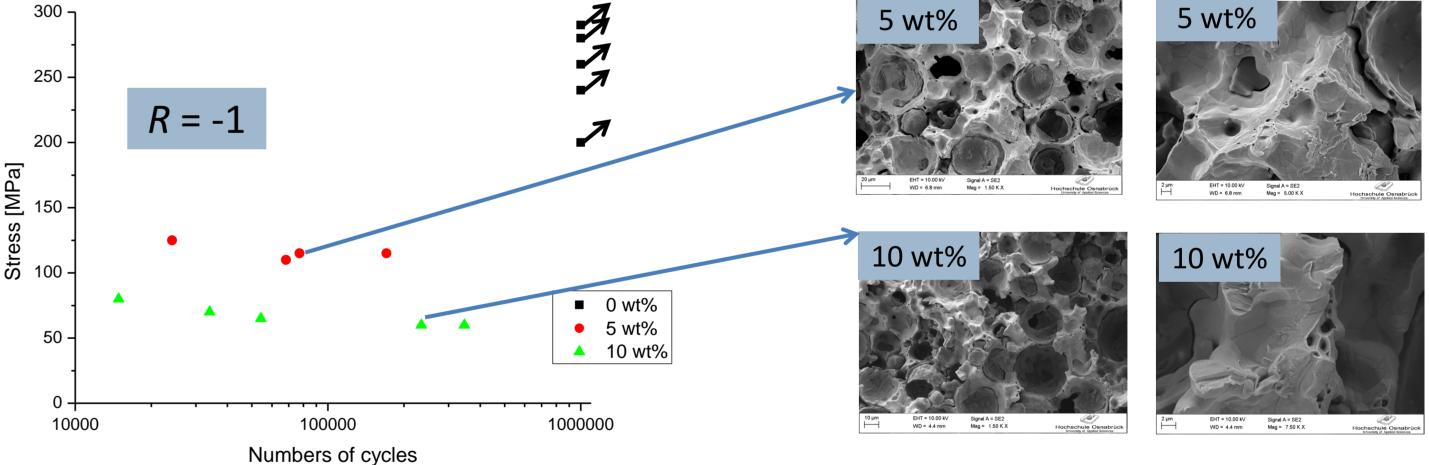


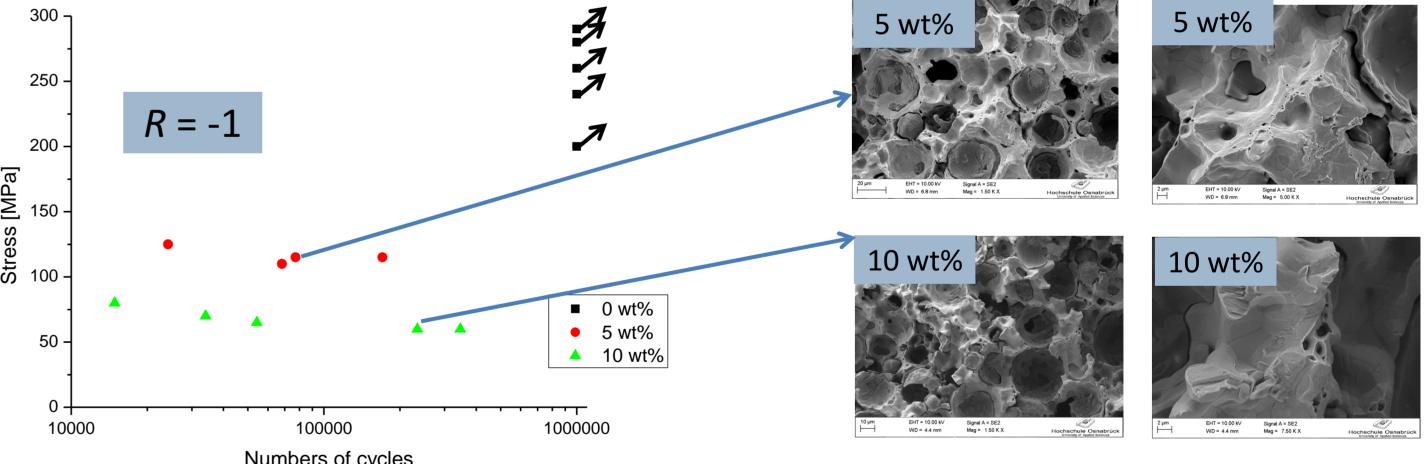
- foams with 5wt%S60HS can be subjected to cyclic compression loads of 240MPa (close to the quasi-static 1% compression yield strength) - for foams with 10wt%S60HS the stress limit is much lower

- ductile failure with increased crack propagation along the sphere-matrix interface



- foams with 5wt%S60HS can be subjected to cyclic tensile loads of 100MPa (close to the quasi-static 0.2% compression yield strength) - for foams with 10wt%S60HS the stress limit is about 50MPa increased crack propagation along the sphere-matrix interface - matrix fracture more of brittle type





	1. Feedstock	2. Filler	3. Injection moulding —	4. Chem. Debinding	5. Thermal Debinding, Sintering
	fatigue testing	g stress ratio = -1,	0.1, 10	tension/fully reverse	compression
	σ		•	R = -1, 0.1	<i>R</i> = 10
σ	m		σ_{max}		
R	Termination criteria				
10	>10 ⁶ cycles compression displacement exceeding 3mm				5 kN servo-pneumatic testing system
0.1	>10 ⁶ cycles				
-1	specimen failure				
	1			25 kN servo-hydraulic	
R	$\sigma_a/[MPa]$		$\varepsilon_{ hol}/[\%]$	testing system	<u>5 mm</u>
10	0 wt%: -240	330	0 wt%:1.12.9		
	5 wt%: -250	D	5 wt%:1.41.7		
	10 wt%: -23	0 10	wt%: 39.142.2	$\bigcirc R = -1$	R = 0.1
0.1	0 wt%: 1321	L43 0	wt%: 1.714.43		
(Middle	5 wt%: 5582	2.5 5	wt%: 0.040.46		

- foams with 5wt%S60HS can be subjected to alternate loads of less than 100MPa for foams with 10wt%S60HS the stress limit is about 50MPa increased crack propagation along the sphere-matrix interface

Conclusions

- using the example of FeNi36 and S60SH micro hollow glass spheres the behaviour of syntactic foams under cyclic loads was investigated
- the foams show reduced allowable stress levels for all tested load modes (compression, tensile, alternating)
- maximum cyclic stresses are close to the quasi-static yield strengths ($R_{p0.2}$ and R_{p1})
- material fails in a ductile manner but with increasing sphere content the matrix fracture changes more to the brittle type
- these first results indicate sufficient fatigue behaviour for many of technical

-1	0 wt%: 200290	0 wt%: 0.00300.0295
	5 wt%: 110150	5 wt%: 0.00200.0235
	10 wt%: 6080	10 wt%: 0.00100.0065

10 wt%: 33...44

evaluation of fracture surface using SEM

applications though more detailed investigations are still needed

Contact:

values)

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10 wt%: -0.05...0.08

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